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# NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

TECHNICAL NOTE 4308

TRANSIENT TEMPERATURE DISTRIBUTION IN A

TWO-COMPONENT SEMI-INFINITE COMPOSITE SLAB OF ARBITRARY

MATERIALS SUBJECTED TO AERODYNAMIC HEATING WITH A

DISCONTINUOUS CHANGE IN EQUILIBRIUM TEMPERATURE

OR HEAT-TRANSFER COEFFICIENT

By Robert L. Trimpi and Robert A. Jones

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#### SUMMARY

A solution is obtained to the transient temperature distribution in a semi-infinite two-component composite slab of arbitrary materials subjected to an instantaneous application of aerodynamic heating with constant equilibrium temperature and heat-transfer coefficient. The numerical results are tabulated in a form to permit easy computation of heat-transfer problems typical of aerodynamic testing. The solutions are valid for finite two-component slabs as long as the times considered are small compared with the diffusion time of the backing material.

Analytical results obtained from these solutions can be used to determine (a) the heat-transfer testing time for which the outer skin may be assumed to act as a calorimeter without exceeding a given error or (b) correction curves by which the indicated calorimeter heat-transfer coefficient may be multiplied to obtain the true heat-transfer coefficient. For such a correction curve to be valid, the bond between the two materials must have negligible thermal resistance, a condition difficult to attain if the slab is not composed of two metals.

Since the differential equation for the temperature distribution is linear, the principle of superposition is valid. Consequently, the problem of continuously varying equilibrium temperatures and heat-transfer coefficients may be treated by using the tabulated solutions and considering the continuous variation as a series of superimposed step functions.

#### INTRODUCTION

The increase in flight speeds for both operational and experimental missiles and airplanes has resulted in renewed interest in the problems involved in fluid- and solid-state heat conduction. The two problems of transient behavior of a two-component slab, consisting of an outer skin with a backing material, exposed to aerodynamic heating that have become of prime importance are: (1) the performance of the surface as measured by the ability of the material to withstand extreme heating rates on the full-scale vehicle during the course of its mission and (2) the transient testing techniques presently in wide use wherein the aerodynamic heating is varied and the resultant time-wise variation of the temperature of a skin, either with or without a backing, is then used to obtain heat-transfer rates and coefficients. For example, these transient testing techniques are used for shock tubes, free-flight pilotless rocket-propelled models, the sudden insertion of a model into a wind tunnel, or the rapid variation of the stagnation conditions in wind tunnels.

In the interest of simplicity, these techniques, except that used for the shock tube, customarily assume that the outer skin of the slab acts as a calorimeter and absorbs all the aerodynamic heat with negligible loss to the backing material. However, even when the backing material has very low conductivity, heat is continually being transferred across the interface and this heat transfer may introduce large errors in the answers obtained by the calorimeter assumption.

Two recent papers (refs. 1 and 2) treat the heat transfer to such a semi-infinite composite slab. Reference 1 is applicable to shock-tube testing wherein a very thin metal plating is formed on an insulator and the temperature response of the metal is used to determine the heat transfer. This study is applicable to arbitrary heat flux rates but assumes the plating to have such negligible thickness that the interface-temperature solution may be found as a perturbation to the surface solution in the absence of the plating. The solutions obtained are valid for times much greater than the diffusion time in the plating. Reference 2 considers the case of the heating of a composite slab in which the heat transfer is proportional to the difference between wall and equilibrium

In the discussion of transient heating problems it is convenient to have reference values of time such as "diffusion time" and "relaxation time" for comparison purposes. The diffusion time is the quotient of the square of a typical length (for example, the thickness of a slab) divided by the thermal diffusivity of the material. The relaxation time, applicable in exponential decay behavior, is also called the time constant and is that value of time which makes the absolute value of the exponent of e unity.

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temperatures. The equilibrium temperature is a step function. The outer skin has finite thickness but infinite conductivity; thus, the temperature in the skin is uniform at any given time. A solution is presented for the heat conduction to the backing material, no coupling between this loss of heat to the backing and the temperature distribution in the outer skin being assumed. This solution is valid for times that are small compared with the relaxation time of the outer skin. Reference 2 shows that conduction even to relatively good insulators introduces appreciable error.

The present investigation was initiated to obtain solutions for the heat transfer to the composite slab without these restrictions. The magnitude of the errors arising from the calorimetric assumption and possible correction factors were to be determined. When the thickness of the backing material is such that the diffusion time for the backing material is much larger than any of the testing times, the backing material then acts as if it were of infinite extent during the test. Consequently, solutions to the problem of a semi-infinite composite slab would apply under this condition. The problem considered in this report is the transient temperature distribution in a semi-infinite two-component slab subjected to aerodynamic heating at a rate equal to the product of a constant heattransfer coefficient and the difference between surface and equilibrium temperatures. The equilibrium temperature is assumed to be a step function and the outer skin is assumed to have both finite conductivity and thickness. Solutions are found which are applicable for times varying from much less than to much greater than the skin diffusion time. The superposition principle permits extension of the results to arbitrary timewise variation in heat-transfer coefficient and equilibrium temperature. investigation reported herein was conducted in the Gas Dynamics branch of the Langley Aeronautical Laboratory.

#### SYMBOLS

a,b	constants
A,B,C,D	constants
с	specific heat
$G_n$	functions defined by equation (23)
H = h/k	
h	heat-transfer coefficient
ĥ	indicated heat-transfer coefficient
$\hat{\mathbf{h}}_{0}$	indicated heat-transfer coefficient at $\xi = 0$ ; pcl $\frac{(dT/dt)_0}{T_e - T_0}$

 $\hat{h}_1$ indicated heat-transfer coefficient at | \xi = 1 coefficient of § in expression for P and equal to +1 j or -1k thermal conductivity  $L = \frac{lh}{k_1} = lH_1$ Laguerre polynomials (see appendix A)  $L_n$ distance from surface to interface integers m,n P parameter in inverse LaPlace transform variable of the Laplace transform р Q heat flux to surface per unit area per unit time  $q = \sqrt{p/\alpha}$  $s = p/4a^2$  $\mathbf{T}$ temperature  $T_e$ equilibrium temperature  $\mathbf{T}_{\alpha}$ temperature at  $\xi = 0$ relaxation temperature relaxation time  $t_{relax}$ t,t',u time variables coordinate measured normal to surface exposed to heating х thermal diffusivity, k/pc

$$\beta = \frac{1 - \sigma}{1 + \sigma}$$

$$\epsilon = \emptyset - 2.5$$

$$\Gamma_s$$
 solutions to  $\Gamma_s$  tan  $\Gamma_s = L$ 

$$\lambda = \sqrt{L} \omega$$

$$\xi = x/l$$

ρ density of material

$$\sigma = \frac{k_2 q_2}{k_1 q_1} = \sqrt{\frac{\rho_2 c_2 k_2}{\rho_1 c_1 k_1}}$$

η, X, τ dummy variables

$$\phi = \psi + I\omega$$

$$\psi = \frac{P}{2\omega}$$

$$\Omega = \emptyset^2 - \psi^2$$

$$\omega = \sqrt{\frac{\alpha_1 t}{l^2}}$$

inverse Laplace transform

A bar over a symbol denotes the Laplace transform. Except as designated in the preceding list, the subscripts 1 or 2 refer to evaluation in region 1 or 2.

#### THEORY

#### General Solution

The problem to be solved is the one-dimensional transient temperature distribution in a semi-infinite two-component slab which has one face suddenly exposed to a fluid. This fluid will transfer heat to the exposed face at a rate proportional to the difference between the constant equilibrium temperature of the fluid and the outer surface temperature of the slab. In the interval 0 < x < l, the slab is composed of a material with properties  $\rho_1$ ,  $c_1$ ,  $k_1$ , and  $a_1$ ; and, in the interval  $l < x < \infty$ , it is composed of a material with properties  $\rho_2$ ,  $c_2$ ,  $k_2$ , and  $a_2$ . No

thermal resistance is assumed at the interface in the slab. The mathematical formulation of this problem is given in terms of the following governing differential equations and boundary conditions (see fig. 1):

$$\frac{\partial^2 T_1}{\partial x^2} - \frac{1}{\alpha_1} \frac{\partial T_1}{\partial t} = 0 \qquad (t > 0, \quad 0 < x < 1) \qquad (1)$$

$$\frac{\partial^2 T_2}{\partial x^2} - \frac{1}{\alpha_2} \frac{\partial T_2}{\partial T} = 0 \qquad (t > 0, \quad l < x < \infty) \qquad (2)$$

$$T_1 = T_2 = 0$$
 (t < 0, all x) (3)

$$T_2 \leftrightarrow 0$$
  $(t > 0, x \leftrightarrow \infty)$  (4)

$$k_{\perp} \frac{\partial T_{\perp}}{\partial x} + h(T_{e} - T_{\perp}) = 0$$
 (x = 0, t > 0) (5)

$$T_1 = T_2$$
 (x = 1, t > 0) (6)

$$k_1 \frac{\partial T_1}{\partial x} = k_2 \frac{\partial T_2}{\partial x}$$
 (x = \lambda, t > 0) (7)

The LaPlace transforms  $\bar{T}(p) = \int_0^\infty e^{-pt} T(t) dt$  and the definitions of  $q \equiv \sqrt{p/\alpha}$  are then employed to reduce equations (1) to (7) to the following forms:

$$\frac{d^2 \bar{T}_1}{dx^2} - q_1^2 \bar{T}_1 = 0 (0 < x < 1) (la)$$

$$\frac{d^2\bar{T}_2}{dx^2} - q_2^2\bar{T}_2 = 0 (l < x < \infty) (2a)$$

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$$\Phi_2 \to 0$$
  $(x \to \infty)$  (4a)

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$$k_1 \frac{d\bar{T}_1}{dx} - h\bar{T}_1 + \frac{hT_e}{p} = 0$$
 (x = 0) (5a)

$$\bar{\mathbf{T}}_1 = \bar{\mathbf{T}}_2$$
 (x = 1) (6a)

$$k_1 \frac{d\overline{T}_1}{dx} = k_2 \frac{d\overline{T}_2}{dx} \qquad (x = 1) \qquad (7a)$$

The general solutions to equations 1(a) and 2(a) are:

$$\bar{\mathbf{T}}_{1} = Ae^{-\mathbf{Q}_{\perp}\mathbf{X}} + Be^{\mathbf{Q}_{\perp}\mathbf{X}}$$
 (8)

$$\overline{T}_2 = Ce^{-q}2^x + De^{q}2^x$$
 (9)

The value of D must be identically zero to satisfy equation 4(a). Application of the boundary conditions (eqs. 6(a) and 7(a)) yields

$$B = \beta A e^{-2q_{\perp}^2 l}$$
 (10)

$$C = (1 + \beta)Ae^{-q_1 l + q_2 l}$$
 (11)

The remaining constant A is then found from equation 5(a) to be

$$A = \frac{H_{1}T_{e}}{p} \frac{1}{q_{1} + H_{1}} \left( 1 - \beta \frac{q_{1} - H_{1}}{q_{1} + H_{1}} e^{-2q_{1}t} \right)^{-1}$$
 (12)

The solutions to the differential equations in the transformed plane become

$$\frac{\bar{T}_{\underline{1}}}{T_{e}} = \frac{H_{\underline{1}}}{p} \frac{1}{q_{\underline{1}} + H_{\underline{1}}} \frac{1}{1 - \beta \frac{q_{\underline{1}} - H_{\underline{1}}}{q_{\underline{1}} + H_{\underline{1}}} e^{-2q_{\underline{1}}l}} \left[ e^{-q_{\underline{1}}x} + \beta e^{-q_{\underline{1}}(2l-x)} \right] \qquad (0 < x < l)$$
(13)

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$$\frac{\bar{T}_{2}}{T_{e}} = \frac{H_{1}}{p} \frac{1}{q_{1} + H_{1}} \frac{1 + \beta}{1 - \beta \frac{q_{1} - H_{1}}{q_{1} + H_{1}} e^{-2q_{1}l}} e^{-q_{1} \left[l + \frac{k_{1}}{k_{2}} \frac{1 - \beta}{1 + \beta}(x - l)\right]}$$
(x > l)

(14)

The inverse LaPlace transform  $\int_{-1}^{-1} \left(\frac{\overline{T}_1}{T_e}\right)$  of equation (13) is known

for the special case  $\sigma=0$ ,  $\beta=1$  which corresponds to a perfect insulator as the backing material. If the exponentials of equation (13) are expressed in hyperbolic form, the inversion on page 259 of reference 3 applies.

$$\int_{-1}^{-1} \left(\frac{\overline{T}_1}{\overline{T}_e}\right) = \frac{\overline{T}_1}{\overline{T}_e} = 2L \sum_{s=1}^{\infty} \frac{1}{\Gamma_s^2 + L^2 + L} \frac{\cos \Gamma_s (1-\xi)}{\cos \Gamma_s} \left(1 - e^{-\frac{\Gamma_s^2 \alpha_1 t}{\ell^2}}\right)$$
(15)

where  $\Gamma_{\rm S}$  are the roots of the equation

$$\Gamma_{\rm S} \tan \Gamma_{\rm g} = L$$
 (16)

If the slab is composed entirely of the same material  $(\beta=0; k_1=k_2)$ , equations (13) and (14) become identical and have as their transform

$$\frac{T}{T_e} = \operatorname{erfc} \frac{x}{2\sqrt{\alpha t}} - \operatorname{e}^{H_1 x + \alpha H_1^2 t} \operatorname{erfc} \left( \frac{x}{2\sqrt{\alpha t}} + H_1 \sqrt{\alpha t} \right)$$
 (17)

For the general case of  $\sigma \neq 0$ ,  $\beta \neq 1$ , the inverse transform of  $T/T_e$  as expressed in the form of equations (13) and (14) is neither known nor easily determined. Recourse is then made to expansion of the right-hand side of these equations. (Note that  $|\beta| \leq 1$ .) An expansion of this type generally results in solutions which will converge more rapidly for small values of time.

Since

$$\left(1 - \beta \frac{q_1 - H_1}{q_1 + H_1} e^{-2q_1 l}\right)^{-1} = \sum_{n=0}^{\infty} \left(\beta \frac{q_1 - H_1}{q_1 + H_1} e^{-2q_1 l}\right)^n$$
 (18)

substitution of equation (18) into equations (13) and (14) yields

$$\frac{\bar{T}_{\underline{1}}}{T_{e}} = H_{\underline{1}} \sum_{n=0}^{\infty} \frac{\beta^{n}}{p} \frac{(q_{\underline{1}} - H_{\underline{1}})^{n}}{(q_{\underline{1}} + H_{\underline{1}})^{n+1}} e^{-q_{\underline{1}} l (2n + \frac{1}{5})} + \frac{\beta^{n+1}}{p} \frac{(q_{\underline{1}} - H_{\underline{1}})^{n}}{(q_{\underline{1}} + H_{\underline{1}})^{n+1}} e^{-q_{\underline{1}} l [2(n+1) - \frac{1}{5}]}$$
(19)

$$\frac{\bar{T}_2}{\bar{T}_e} = H_1(1+\beta) \sum_{n=0}^{\infty} \frac{\beta^n}{p} \frac{(q_1 - H_1)^n}{(q_1 + H_1)^{n+1}} e^{-q_1 l} \left[ 2n + l + \frac{k_1}{k_2} \frac{1-\beta}{1+\beta}(\xi-1) \right]$$
(20)

If the orders of summation and integration of the inversion process are assumed to be interchangeable, then

$$\mathcal{L}^{-1}\left(\frac{\overline{T}_{1}}{\overline{T}_{e}}\right) = H_{1} \sum_{n=0}^{\infty} \mathcal{L}^{-1}\left\{\frac{\beta^{n}}{p} \frac{\left(q_{1} - H_{1}\right)^{n}}{\left(q_{1} + H_{1}\right)^{n+1}} e^{-q_{1} l(2n+\xi)} + \frac{\beta^{n+1}}{p} \frac{\left(q_{1} - H_{1}\right)^{n}}{\left(q_{1} + H_{1}\right)^{n+1}} e^{-q_{1} l[2(n+1)-\xi]}\right\} \tag{21}$$

$$\mathcal{L}^{-1}\left(\frac{T_{2}}{T_{e}}\right) = H_{1}(1+\beta) \sum_{n=0}^{\infty} \mathcal{L}^{-1}\left\{\frac{\beta^{n}}{p} \frac{(q_{1}-H_{1})^{n}}{(q_{1}+H_{1})^{n+1}} e^{-q_{1}l\left[2n+1+\frac{k_{1}}{k_{2}}\frac{1-\beta}{1+\beta}(\xi-1)\right]}\right\}$$
(22)

Let the function  $G_n(P,\omega,L)$  be defined as follows:

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$$G_{n}(P,\omega,L) = \frac{2}{\sqrt{\pi}} \int_{P/2\omega}^{\infty} e^{-X^{2}} \int_{Q}^{2\omega L} \left(X - \frac{P}{2\omega}\right) e^{-\eta} L_{n}(2\eta) d\eta dx \qquad (23)$$

In appendix A it is shown that the inversion of the general term of the series has the form

$$\sum_{p}^{-1} \left[ \frac{H_{1}}{p} \frac{(q_{1} - H_{1})^{n}}{(q_{1} + H_{1})^{n+1}} e^{-q_{1}lp} \right] = G_{n}(P,\omega,L)$$
 (24)

Substitution of equation (24) into equations (21) and (22) produces

$$\frac{T_{1}}{T_{e}} = \sum_{n=0}^{\infty} \beta^{n} G_{n}(2n+\xi,\omega,L) + \beta^{n+1} G_{n}[2(n+L)-\xi,\omega,L]$$
 (25)

$$\frac{T_2}{T_e} = (1 + \beta) \sum_{n=0}^{\infty} \beta^n G_n \left[ 2n + 1 + \frac{k_1}{k_2} \frac{1 - \beta}{1 + \beta} (\xi - 1), \omega, L \right]$$
 (26)

The formal integrations required for the evaluation of  $G_n$  for a range of values of n from 0 to 5 are given in appendix B. The associated timewise and spacewise derivatives  $\left(\frac{\partial G_n}{\partial \omega^2}\right)$  and  $\left(\frac{\partial G_n}{\partial \xi}\right)$  are also presented. These derivatives permit the evaluation of both the correction curves to the indicated calorimetric heat-transfer coefficient and the amount of heat crossing a given station, in order that estimate of the flux through the backing material may be obtained.

#### Significance of parameters L, $\lambda$ , and $\beta$

The physical significance of the nondimensional parameters L,  $\lambda$ , and  $\beta$  will be briefly discussed at this point. The parameter  $L=\frac{lh}{k_l}$  is proportional to the ratio of the temperature difference required to transport a given amount of heat per unit area across the slab to the temperature difference required to transport the same amount of heat per

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unit area from the fluid to the slab. This may be illustrated for the steady-flow case as follows:

$$Q = h \left[ T_e - T(0) \right] = k_1 \frac{T(0) - T(1)}{l}$$

Therefore,

$$\frac{T(0) - T(1)}{T_e - T(0)} = \frac{hl}{k_1} = L$$

Now if L is small, a small temperature difference across the outer skin is indicated; thus, the surface temperature and heat transfer when  $T(0) \rightarrow T_p$  will be sensitive to changes in the temperature at the interface. Since the interface temperature is in turn influenced strongly by the backing material, the relative influence of the backing material increases with a decrease in L for times of the order of the relaxation time. (For very large times the backing material must always be the dominating factor.) The significance of L may be realized in an alternate way by considering that, when L is small owing to a thin skin, high thermal conductivity, or a low heat-transfer coefficient, a greater portion of the heat transferred to the surface is available for transfer to the backing material and the backing material can exert a larger influence on the temperature time history of the skin for finite times. A plot of the parameter L obtained for various skin thickness and material combinations with h = 0.1 Btu/sq ft-sec-OF is shown in figure 2. A range of L from 0.001 to 0.5 appears to cover practical outer skins which might be used for high-speed vehicles.

The significance of the parameter  $\lambda = \sqrt{L} \ \omega = \sqrt{\frac{ht}{\rho c \, l}}$  is most easily described from consideration of the aerodynamic heating of a slab of thickness l having infinite conductivity  $(\partial T/\partial x = 0)$ . The slab acts as a calorimeter absorbing all the heat input. This slab is initially at T=0 and is subjected to a step input in equilibrium temperature at t=0. The temperature of the slab at time t may be expressed as

$$\frac{T}{T_e} = 1 - e^{-\frac{\alpha L}{12}t} = 1 - e^{-\lambda^2}$$

Thus, the value  $\lambda = 1$  corresponds to the relaxation time in such a slab calorimeter.

For a perfectly insulated skin having finite conductivity and thickness, the temperature distribution departs from that of the calorimeter

as L increases from zero. However, at the value  $\lambda=1$ , the temperature is approximately the relaxation value given by  $T_{\rm relax}=T_{\rm e}\left(1-\frac{1}{\rm e}\right)$ . Since  $t \propto \lambda^2$ , the ratio of any time t to the relaxation time  $t_{\rm relax}$  is simply  $\lambda^2$ .

The parameter  $\beta$  denotes the relative insulating perfection of the backing material. A value of  $\beta=1$  applies to a perfect insulator;  $\beta=0$  describes the homogenous composite slab constructed of the same material throughout; and  $\beta=-1$  describes a perfect conductor which maintains a constant temperature at the interface at  $\xi=1$ . Values of  $\beta$  appropriate to various combinations of outer skin and backing material are shown in figure 3. The outer skin materials have common abscissas and the intersection of these vertical lines with the curves for the backing materials determine the appropriate value of  $\beta$ . If the materials for skin and backing are interchanged, the sign of  $\beta$  is reversed.

#### Particular Solutions

Since many aerodynamic heat-transfer experiments are performed with a model which has a skin of high conductivity and density compared with that of the backing material, it is desirable to have a form of solution applicable to these circumstances. The solution for a perfect insulator backing material is either the series given in equation (15) or that given in equation (25) when a value of  $\beta = 1$  is used. These alternate solutions converge most rapidly at opposite times. The number of terms required to express the timewise derivative for equation (15) is large as  $t \rightarrow 0$  and decreases rapidly with an increase in time; thus for values of t greater than about one-half the relaxation time, only one or two terms are required to give the value of  $T_1/T_e$  and its timewise and spacewise derivatives with acceptable accuracy. Conversely, although one term is sufficient for equation (25) when  $t \rightarrow 0$ , the number of terms required increases with time. A series that will converge rapidly for the times of interest for aerodynamic testing purposes when  $\beta \approx 1$  may be obtained by applying the solution of equation (25) as a perturbation to the solution of equation (15). If  $T_1/T_e$  for  $\beta = 1.0$  is added and subtracted to the right-hand side of equation (25), the resulting equation is

$$\frac{T_{\underline{1}}}{T_{\underline{e}}} = \left(\frac{T_{\underline{1}}}{T_{\underline{e}}}\right)_{\beta=\underline{1}} - \sum_{n=0}^{\infty} \left\{ (1 - \beta^n)_{G_n} (2n + \xi, \omega, L) + (1 - \beta^{n+1})_{G_n} \left[ 2(n+1) - \xi, \omega, L \right] \right\}$$

(27)

where  $\left(\frac{T_1}{T_e}\right)_{\beta=1}$  is evaluated from equation (15) for the appropriate values of L,  $\omega$ , and  $\xi$ .

Of particular interest is the temperature history on the surface exposed to the transferring fluid ( $\xi = 0$ ) and that on the interface ( $\xi = 1$ ) between the two different materials. Substitution of  $\xi = 0$  into equation (27) produces the following set of equations:

$$\frac{T_{1}}{T_{e}}(\xi=0,\omega,L) = \left(\frac{T_{1}}{T_{e}}\right)_{\beta=1} - \left\{\sum_{n=0}^{\infty} (1-\beta^{n})G_{n}(2n,\omega,L) + \sum_{n=1}^{\infty} (1-\beta^{n})G_{n-1}(2n,\omega,L)\right\}$$
(28)

$$\frac{\partial \frac{\mathbb{T}_{\underline{1}}}{\mathbb{T}_{\underline{e}}}}{\partial \omega^{2}}(\xi=0,\omega,L) = \left(\frac{\partial \frac{\mathbb{T}_{\underline{1}}}{\mathbb{T}_{\underline{e}}}}{\partial \omega^{2}}\right)_{\beta=1} - \left\{\sum_{n=0}^{\infty} \left(1-\beta^{n}\right) \frac{\partial G_{n}}{\partial \omega^{2}}(2n,\omega,L) + \sum_{n=1}^{\infty} \left(1-\beta^{n}\right) \frac{\partial G_{n-1}}{\partial \omega^{2}}(2n,\omega,L)\right\}$$
(29)

$$\frac{\partial \frac{T_{\perp}}{T_{e}}}{\partial \xi} (\xi = 0, \omega, L) = \left( \frac{\partial \frac{T_{\perp}}{T_{e}}}{\partial \xi} \right)_{\beta = L} - \left\{ \sum_{n=0}^{\infty} \left( 1 - \beta^{n} \right) \left[ \frac{\partial G_{n}}{\partial \xi} (2n, \omega, L) \right]_{j=1} - \sum_{n=1}^{\infty} \left( 1 - \beta^{n} \right) \left[ \frac{\partial G_{n-1}}{\partial \xi} (2n, \omega, L) \right]_{j=1} \right\}$$
(30)

A corresponding set of equations may be obtained for the interface by substituting  $\xi = 1$  into equation (27):

$$\frac{T_{\underline{l}}}{T_{\underline{e}}}(\xi=\underline{l},\omega,\underline{L}) = \left(\frac{T_{\underline{l}}}{T_{\underline{e}}}\right)_{\beta=\underline{l}} - \sum_{n=0}^{\infty} \left[2 - \beta^{n}(\underline{l} + \beta)\right] G_{\underline{n}}(2n+\underline{l},\omega,\underline{L})$$
(31)

$$\frac{\partial^{\frac{T_{1}}{T_{e}}}}{\partial \omega^{2}}(\xi=1,\omega,L) = \left(\frac{\partial^{\frac{T_{1}}{T_{e}}}}{\partial \omega^{2}}\right)_{\beta=1} - \sum_{n=0}^{\infty} \left[2 - \beta^{n}(1+\beta)\right] \frac{\partial G_{n}}{\partial \omega^{2}}(2n+1,\omega,L)$$
 (52)

$$\frac{\partial \overline{T_{\underline{0}}}}{\partial \xi}(\xi=1,\omega,L) = (1-\beta) \sum_{n=0}^{\infty} \beta^{n} \left[ \frac{\partial G_{\underline{n}}}{\partial \xi}(2n+1,\omega,L) \right]_{\underline{j}=1}$$
 (53)

The evaluation of the terms of equations (25) and (26) becomes progressively more difficult as n increases. Consequently, if the

temperature at the interface ( $\xi = 1$ ) has to be evaluated for any reason or if the values tabulated in this report are to be used, then the temperature distribution in the backing material can advantageously be obtained by Duhamel's method.

Since the temperature distribution in a semi-infinite slab  $(l < x < \infty)$  when one surface at x = l undergoes a unit-step-function increase in temperature is (ref. 3)

$$T_2(x,t) = \operatorname{erfc} \frac{x - l}{2\sqrt{\alpha_2 t}}$$
 (34)

Duhamel's technique yields

$$\frac{T_{2}}{T_{e}}(x,t) = \frac{(x-1)(1+\beta)}{2\sqrt{\pi\alpha_{2}}} \int_{0}^{t} \frac{e^{-\frac{(x-1)^{2}}{4\alpha_{2}(t-\tau)}}}{(t-\tau)^{3/2}} \left[ \sum_{n=0}^{\infty} \beta^{n} G_{n} \left(2n+1, \frac{\alpha_{1}\tau}{2}, L\right) \right] d\tau$$
 (35)

#### RESULTS AND DISCUSSION

#### General Results

The values of  $G_n$  and its derivatives for n=0 to 5 and  $\xi=0$  and 1 were computed on a card-programed calculator. Details of this procedure are discussed in appendix C. The results of these computations are given in table I for values of L between 0.001 and 0.5 with  $0.02 \le \lambda \le 8$ . Table I is arranged for future computing convenience. Values on the left for  $\xi=0$  are alined so that pairs in G or its derivatives on the same horizontal line are operated on by the same power of  $\beta$  as prescribed by equations (28) to (30).

As discussed in appendix C the computing procedure at times involved the subtraction of two large and nearly equal numbers obtained by approximations. Certain voids appear in table I where an inspection of the machine results indicated insufficient accuracy. There was no rigorous rule for determining which answers to discard, but all answers with less than four significant figures were usually eliminated. Those with less than three significant figures were always eliminated.

Typical values of  $G_n$  and its associated derivatives which are required at  $\xi=0$  are plotted against L for  $\lambda=1.0$ . (See fig. 4.) The values shown are those needed in the evaluation of the first series in the braces of equations (28) to (30). It is immediately obvious that

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the convergence of the series is much more rapid for large values of L than for small values of L. For example, at L = 0.5 the ratio of  $G_{l\mu}$  to  $G_{0}$  is of the order of  $10^{-6}$  whereas at L = 0.00l the ratio is of the order of one.

An indication of the accuracy which results from consideration of a finite number of terms to represent the infinite series of equation (25) may be obtained from figure 5. In this figure are plotted the values of the ratio of  $T_1/T_e$  for  $\beta = 1$  when the upper limit of summation in equation (25) is reduced from infinity to 0, 1, 2, 3, 4, or 5 to that obtained from table II. (Table II contains the values of  $T_1/T_e$  as determined from equation (15) by using a sufficient number of terms to get the desired accuracy.) The ratio for values of L = 0.001, 0.1,and 0.5 is plotted as a function of  $\lambda$ . The number of terms required to reduce the error to a given limit is seen to increase with an increase in  $\lambda$  at a constant L and to increase with a decrease in L at a constant  $\lambda$ . For a constant L, the behavior of  $T_1/T_e$  for any finite number of terms becomes oscillatory as \(\lambda\) increases. The errors for  $0 \le \beta < 1$  at a given  $\lambda$  and L should be less than those indicated in figure 5 for  $\beta = 1$  since the terms neglected contain  $\beta^n$  or  $\beta^{n+1}$ . In other words, the neglected terms for  $0 \le \beta < 1$  have a smaller contribution than those for  $\beta = 1.0$ .

#### Illustrative Example

The effects of the backing material in a composite slab under typical transient test conditions will be illustrated by the following study. The numerical results obtained are found by using the values of table I for  $0 \le n \le 5$  and those of table II. The mathematical assumption of an infinite extent of backing material to represent the finite backing of the test is valid for values of  $\beta$  near unity as long as the times considered are much less than the diffusion time of the backing. The diffusion times, which are equal to the square of the thickness of the backing material divided by the diffusivity of the backing material, for 1/4-inch-thick balsa and mahogany are approximately 120 and 170 seconds, respectively. Consider two stainless-steel outer skins (k = 0.0028 Btu/sec-ft-OF,  $\alpha = 5.2 \times 10^{-5}$  sq ft/sec) with thicknesses of 0.060 inch and 0.030 inch backed by either a perfect insulator ( $\beta = 1.000$ ), balsa ( $\beta \approx 0.975$ ), or mahogany ( $\beta \approx 0.950$ ). These composite slabs are subjected to a step input in equilibrium temperature (for example, by sudden exposure to the airstream of a wind tunnel) and the heat-transfer coefficient h is 0.056 Btu/sq ft-sec-OF. The values of L are then 0.10 and 0.05 for the 0.060- and 0.030-inch thicknesses, respectively.

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The resulting behavior of the outer skin is illustrated in figure 6 which shows the temperature distribution at the outer face ( $\xi = 0$ ) as a function of time. The effect of the heat lost to the backing material is evident in a lower temperature in the outer skin at a given time, a larger effect being observed for the thinner skin.

An indicated heat-transfer coefficient is often obtained from the temperature-time history of such an experiment. This heat-transfer coefficient is determined by assuming that the slab acts as a calorimeter with an infinite value of k; that is,

$$\hat{h} \equiv \rho c l \frac{dT/dt}{T_e - T}$$

Since the value of  $\hat{h}$  depends on the value of  $\xi$  at which T is measured for finite k, the term  $\hat{h_0}$  or  $\hat{h_1}$  will be used to designate the values of  $\hat{h}$  which would be found when T and dT/dt are evaluated at  $\xi = 0$  or 1.

The ratio of the indicated heat-transfer coefficient to the true heat-transfer coefficient  $\hat{h}/h$  is plotted as a function of time in figures 7 and 8. Figure 7 shows the ratio at  $\xi=0$  and 1.0 for the 0.030-inch-thick skin. Except for the initial discrepancy at early times the values of  $\hat{h}_0$  and  $\hat{h}_1$  are nearly equal. At t=0,  $\hat{h}_0$  is infinite while  $\hat{h}_1$  is zero, but after about 0.1 second the difference is minor. Figure 8 shows the ratio  $\hat{h}_0/h$  as a function of time for both the 0.030-inch and 0.060-inch skin. It is evident that  $\hat{h}_0=h$  only at a single discrete point for each combination of skin thickness and backing material. Furthermore, even the perfect insulator does not give a ratio of unity for  $\hat{h}/h$  except at one value of time. It may be shown for the perfect insulator that the asymptotic value of  $\hat{h}/h$  is

$$\lim_{t \to \infty} \frac{\hat{h}}{h} = \frac{\Gamma_1^2}{L}$$

$$= 1 - \frac{1}{3} L \frac{1 + \frac{2}{5} L}{1 + \frac{2}{5} L^2} + \cdots$$

$$\approx 1 - \frac{1}{3} L \qquad (L \ll 1)$$

Thus even the perfect insulator gives errors of 5/3 and 10/3 percent for the cases considered (0.030-inch and 0.060-inch-thick skins). The large increase with time of the deviation of  $\hat{h}/h$  from unity for the imperfect insulators is striking. This error increases with time because, as the heat transferred into the skin at  $\xi=0$  decreases monotonically with time, the heat transferred out at  $\xi=1$  first rises with time to a maximum (at approximately  $\lambda=1.0$ ) and then subsequently decreases but at a rate slower than that at  $\xi=0$ . An approximate method for estimating the amount of heat conducted across the interface for the conditions of  $\lambda \ll 1$  and  $k \to \infty$  was also presented in reference 2.

If an error of 10 percent were set on the deviation of indicated to true heat-transfer coefficient, the time limit for useful data with the respective backings composed of mahogany and balsa would be about 1 second and 2.5 seconds when l=0.030 inch and 2.4 seconds and 5.7 seconds when l=0.060 inch. If, instead of using a time limit, a temperature rise limit for a 10-percent error were desired, it may be obtained from a plot similar to that of figure 9. For l=0.030 inch, temperature rises greater than 30 percent of  $T_{\rm e}$  for a mahogany backing or 65 percent of  $T_{\rm e}$  for a balsa backing would give values of  $\hat{h}/h$  deviating from unity by more than 10 percent. Approximately the same limits also apply for l=0.060 inch.

#### CONCLUDING REMARKS

A solution has been obtained to the transient temperature distribution in a semi-infinite two-component composite slab of arbitrary materials subjected to an instantaneous application of aerodynamic heating with constant equilibrium temperature and heat-transfer coefficient. The numerical results are tabulated in a form to permit easy computation of heat-transfer problems typical of aerodynamic testing. The solutions are valid for finite two-component slabs as long as the times considered are small compared with the diffusion time of the backing material.

Analytical results obtained from these solutions can be used to determine (a) the heat-transfer testing time for which the outer skin may be assumed to act as a calorimeter without exceeding a given error or (b) correction curves by which the indicated calorimeter heat-transfer coefficient may be multiplied to obtain the true heat-transfer coefficient. For such a correction curve to be valid, the bond between the two materials must have negligible thermal resistance, a condition difficult to attain if the slab is not composed of two metals.

Since the differential equation for the temperature distribution is linear, the principle of superposition is valid. Consequently, the problem

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of continuously varying equilibrium temperatures and heat-transfer coefficients may be treated by using the tabulated solutions and considering the continuous variation as a series of superimposed step functions.

Langley Aeronautical Laboratory,
National Advisory Committee for Aeronautics,
Langley Field, Va., June 4, 1958.

#### APPENDIX A

#### INVERSION OF THE LAPLACE TRANSFORM

The steps required to invert the general terms of the series of equations (21) and (22) will be determined in this section. The inversion of the expression

$$= \frac{-1}{2} \left[ \frac{e^{-b\sqrt{p}}}{p} \frac{(\sqrt{p} - a)^n}{(\sqrt{p} + a)^{n+1}} \right] = \frac{-1}{2} \left[ \frac{e^{-2ab\sqrt{\frac{p}{\mu_a^2}}} (2\sqrt{\frac{p}{\mu_a^2}} - 1)^n}{e^{-2ab\sqrt{\frac{p}{\mu_a^2}}} (2\sqrt{\frac{p}{\mu_a^2}} - 1)^{n+1}} \right]$$
(A1)

will first be found and then the constants a and b will be assigned pertinent values.

Let  $s = \frac{p}{4a^2}$ . It is then necessary to find the inversion for

The square-root image relation (see page 123 of ref. 4) can be used to evaluate equation (A2). Thus if

$$f(t') = \int_{-1}^{-1} [g(s)]$$

then

$$\frac{1}{\sqrt{\pi t'}} \int_0^\infty e^{-\frac{u^2}{4t'}} f(u) du = \int_0^{-1} \frac{1}{\sqrt{s}} g(\sqrt{s})$$
 (A3)

and the evaluation of the following expression is required:

$$\int_{0}^{-1} \left[ e^{-2abs} \frac{(2s-1)^n}{(2s+1)^{n+1}} \right]$$

The term

$$\mathcal{L}^{-1}\left(\frac{e^{-2abs}}{s}\right) = 0 \qquad (0 < \tau < 2ab)$$

$$\mathcal{L}^{-1}\left(\frac{e^{-2abs}}{s}\right) = 1 \qquad (2ab < \tau)$$

and

(See page 298 of ref. 5 and page 129 of ref. 4.) The symbol  $L_{\rm n}(\tau)$  designates Laguerre polynomials of the following form:

$$L_{n}(\tau) = \sum_{m=0}^{n} {n \choose n - m} \frac{(-\tau)^{m}}{m!}$$

$$L_{n}(\tau) = \sum_{m=0}^{n} \frac{n!}{(n - m)!} \frac{(-\tau)^{m}}{(m!)^{2}}$$
(A6)

Application of the convolution theorem to equations (A4) and (A5) results in:

$$\frac{1}{e^{-2abs}} \frac{(2s-1)^n}{(2s+1)^{n+1}} = \frac{1}{2} \int_0^{u-2ab} e^{-\tau/2} L_n(\tau) (1) d\tau + \frac{1}{2} \int_{u-2ab}^u e^{-\tau/2} L_n(\tau) (0) d\tau$$

$$= \frac{1}{2} \int_0^{u-2ab} e^{-\tau/2} L_n(\tau) d\tau \qquad (A7)$$

Combination of equation (A7) and the image formula (A3) yields

$$\mathcal{L} \left\{ \frac{1}{\sqrt{s}} \left[ \frac{e^{-2ab\sqrt{s}}}{\sqrt{s}} \frac{(2\sqrt{s} - 1)^{n}}{(2\sqrt{s} + 1)^{n+1}} \right] \right\} = \frac{1}{\sqrt{nt^{\tau}}} \int_{2ab}^{\infty} e^{-\frac{u^{2}}{4t^{\tau}}} \int_{0}^{u-2ab} \frac{1}{2} e^{-\tau/2} L_{n}(\tau) d\tau du \tag{A8}$$

For s = cp, ct' = t, it may be shown that, if

$$\int_{0}^{1} \left[ g(s) \right] = f(t')$$

then

$$\mathcal{L} \left[ g(pc) \right] = \frac{1}{c} f\left(\frac{t}{c}\right) \tag{A9}$$

Consequently, since  $c = \frac{1}{4a^2}$ , equation (A8) may be operated on to yield:

$$\int_{-1}^{-1} \left\{ \frac{1}{\sqrt{\frac{p}{\mu_{a}2}}} \left[ \frac{e^{-2ab\sqrt{\frac{p}{\mu_{a}2}}}}{\sqrt{\frac{p}{\mu_{a}2}}} \frac{\left(2\sqrt{\frac{p}{\mu_{a}2}}-1\right)^{n}}{\left(2\sqrt{\frac{p}{\mu_{a}2}}+1\right)^{n+1}} \right] \right\} = \frac{\mu_{a}2}{2\sqrt{\pi\mu_{a}2t}} \int_{2ab}^{\infty} e^{-\frac{u^{2}}{16a^{2}t}} \int_{0}^{u-2ab} e^{-\frac{\tau}{2}} L_{n}(\tau) d\tau \ du$$

or

$$\int_{a}^{-1} \left[ a \frac{e^{-b\sqrt{p}}}{p} \frac{(\sqrt{p} - a)^{n}}{(\sqrt{p} + a)^{n+1}} \right] = \frac{1}{4a\sqrt{\pi t}} \int_{2ab}^{\infty} e^{-\frac{u^{2}}{16a^{2}t}} \int_{0}^{u-2ab} e^{-\frac{\tau}{2}} I_{n}(\tau) d\tau du$$
(Alo)

If  $a = H \sqrt{\alpha}$  and  $b = \frac{Pl}{\sqrt{\alpha}}$ , equation (AlO) becomes

Ιſ

$$\eta = \tau/2$$

and

$$x = \frac{u}{\frac{1}{4} l H \sqrt{\frac{\alpha t}{l^2}}}$$
$$= \frac{u}{\frac{1}{4} L \omega}$$

are substituted in the right-hand side of equation (All), the following equations result:

$$\frac{-1}{\left[H_{\perp} \frac{e^{-1Pq_{\perp}}}{p} \frac{\left(q_{\perp} - H_{\perp}\right)^{n}}{\left(q_{\perp} + H_{\perp}\right)^{n+1}}\right]} = \frac{2}{\sqrt{\pi}} \int_{P/2\omega}^{\infty} e^{-\chi^{2}} \int_{0}^{2L\omega\left(\chi - \frac{P}{2\omega}\right)} e^{-\eta} L_{n}(2\eta) d\eta d\chi$$

$$\equiv G_{n}(P,\omega,L) \tag{A12}$$

#### APPENDIX B

Expressions for the various 
$$G_n$$
,  $\frac{\partial G_n}{\partial \omega^2}$ , and  $\frac{\partial G_n}{\partial \xi}$ 

#### FOR VALUES OF n FROM 0 TO 5

Formal integration of the equations for the  $G_n$  for values of n from 0 to 5 and subsequent partial differentiation with respect to  $\omega^2$  and  $\xi$  produced the following expressions:

$$\begin{split} &\mathbf{G}_{\mathrm{O}} = \mathrm{erfc} \ \psi - \mathrm{e}^{\Omega} \mathrm{erfc} \ \phi \\ &\frac{\partial \mathbf{G}_{\mathrm{O}}}{\partial \xi} = -\mathrm{j} \mathrm{Le}^{\Omega} \mathrm{erfc} \ \phi \\ &\frac{\partial \mathbf{G}_{\mathrm{O}}}{\partial \omega^{2}} = \frac{1}{\sqrt{\pi}} \frac{\mathrm{L}^{3/2}}{\lambda} \ \mathrm{e}^{-\psi^{2}} - \mathrm{L}^{2} \mathrm{e}^{\Omega} \mathrm{erfc} \ \phi \\ &\mathbf{G}_{\mathrm{I}} = -\mathrm{erfc} \ \psi + \left(1 - \frac{1}{4} \lambda \sqrt{\mathrm{I}} \phi\right) \mathrm{e}^{\Omega} \mathrm{erfc} \ \phi + \frac{1}{4} \frac{1}{\sqrt{\pi}} \lambda \sqrt{\mathrm{I}} \mathrm{e}^{-\psi^{2}} \\ &\frac{\partial \mathbf{G}_{\mathrm{I}}}{\partial \xi} = -\mathrm{Lj} \left(1 + \frac{1}{4} \lambda \sqrt{\mathrm{I}} \phi\right) \mathrm{e}^{\Omega} \mathrm{erfc} \ \phi + \mathrm{j} \frac{1}{\sqrt{\pi}} \lambda \mathrm{L}^{3/2} \mathrm{e}^{-\psi^{2}} \\ &\frac{\partial \mathbf{G}_{\mathrm{I}}}{\partial \omega^{2}} = -\mathrm{L}^{2} \left(3 + \frac{1}{4} \lambda \sqrt{\mathrm{I}} \phi\right) \mathrm{e}^{\Omega} \mathrm{erfc} \ \phi + \frac{13/2}{\sqrt{\pi}} \left(\frac{1}{\lambda} + \frac{1}{4} \lambda \mathrm{L}\right) \mathrm{e}^{-\psi^{2}} \\ &\mathbf{G}_{2} = \mathrm{erfc} \ \psi - \left(1 + 8 \lambda^{2} \mathrm{I} \phi^{2} + \frac{1}{4} \lambda^{2} \mathrm{L}\right) \mathrm{e}^{\Omega} \mathrm{erfc} \ \phi + \left(\frac{8}{\sqrt{\pi}} \lambda^{2} \mathrm{I} \phi\right) \mathrm{e}^{-\psi^{2}} \\ &\frac{\partial \mathbf{G}_{2}}{\partial \xi} = -\mathrm{Lj} \left(1 + 8 \lambda \sqrt{\mathrm{I}} \phi + 8 \lambda^{2} \mathrm{I} \phi^{2} + \frac{1}{4} \lambda^{2} \mathrm{L}\right) \mathrm{e}^{\Omega} \mathrm{erfc} \ \phi + \frac{8 \mathrm{j}}{\sqrt{\pi}} \lambda \mathrm{L}^{3/2} \left(1 + \lambda \sqrt{\mathrm{I}} \phi\right) \mathrm{e}^{-\psi^{2}} \\ &\frac{\partial \mathbf{G}_{2}}{\partial \omega^{2}} = -\mathrm{L}^{2} \left(5 + 16 \lambda \sqrt{\mathrm{I}} \phi + 8 \lambda^{2} \mathrm{L} \phi^{2} + \frac{1}{4} \lambda^{2} \mathrm{L}\right) \mathrm{e}^{\Omega} \mathrm{erfc} \ \phi + \frac{1}{\sqrt{\pi}} \left(\frac{1}{\lambda} + 8 \lambda \mathrm{L}^{3/2} \left(2 + \lambda \sqrt{\mathrm{I}} \phi\right)\right) \mathrm{e}^{-\psi^{2}} \end{split}$$

$$\begin{split} \mathbf{G}_{3} &= -\text{erfc} \ \psi - \mathbf{e}^{\Omega} \text{erfc} \ \phi \left( -\mathbf{1} + 4\lambda \sqrt{\mathbf{L}} \phi + 8\lambda^{2} \mathbf{L} \phi^{2} + 4\lambda^{2} \mathbf{L} + \frac{32}{3} \ \lambda^{3} \mathbf{L}^{3/2} \phi^{3} + \\ & 16\lambda^{3} \mathbf{L}^{3/2} \phi \right) + \frac{1}{\sqrt{\pi}} \left( 4\lambda \sqrt{\mathbf{L}} + 8\lambda^{2} \mathbf{L} \phi + \frac{32}{3} \ \lambda^{3} \mathbf{L}^{3/2} \phi^{2} + \frac{32}{3} \ \lambda^{3} \mathbf{L}^{3/2} \right) \mathbf{e}^{-\psi^{2}} \end{split}$$

$$\begin{split} \frac{\partial G_3}{\partial \xi} &= -\mathrm{e}^\Omega \mathrm{erfc} \ \phi \ \mathrm{j} \left( \mathrm{L} + 12\lambda \mathrm{L}^{3/2} \phi + 2^{\mathrm{j}} \lambda^2 \mathrm{L}^2 \phi^2 + 12\lambda^2 \mathrm{L}^2 + \frac{32}{3} \, \lambda^3 \mathrm{L}^{5/2} \phi^3 + \\ & 16\lambda^3 \mathrm{L}^{5/2} \phi \right) + \mathrm{j} \, \frac{1}{\sqrt{\pi}} \left( 12\lambda \mathrm{L}^{3/2} + 2^{\mathrm{j}} \lambda^2 \mathrm{L}^2 \phi + \frac{32}{3} \, \lambda^3 \mathrm{L}^{5/2} + \frac{32}{3} \, \lambda^3 \mathrm{L}^{5/2} \phi^2 \right) \mathrm{e}^{-\psi^2} \end{split}$$

$$\frac{\partial G_{3}}{\partial \omega^{2}} = e^{-\psi^{2}} \frac{1}{\sqrt{\pi}} \left( \frac{L^{3/2}}{\lambda} + 36\lambda L^{5/2} + 40\lambda^{2}L^{3}\phi + \frac{32}{3} \lambda^{3}L^{7/2}\phi^{2} + \frac{32}{3} \lambda^{3}L^{7/2} \right) - e^{\Omega} \operatorname{erfc} \phi \left( 7L^{2} + 36\lambda L^{5/2}\phi + 40\lambda^{2}L^{3}\phi^{2} + 20\lambda^{2}L^{3} + \frac{32}{3} \lambda^{3}L^{7/2}\phi^{3} + 16\lambda^{3}L^{7/2}\phi \right)$$

$$G_{\downarrow} = \operatorname{erfc} \ \psi - e^{\Omega} \operatorname{erfc} \ \phi \left( 1 + 16\lambda^{2} L \phi^{2} + 8\lambda^{2} L + \frac{64}{3} \lambda^{3} L^{3/2} \phi^{3} + \frac{32}{3} \lambda^{4} L^{2} \phi^{4} + 32\lambda^{4} L^{2} \phi^{2} + 8\lambda^{4} L^{2} + 32\lambda^{3} L^{3/2} \phi \right) + \frac{1}{3\sqrt{\pi}} \left( 48\lambda^{2} L \phi + 64\lambda^{3} L^{3/2} \phi^{2} + 64\lambda^{3} L^{3/2} \phi^{3} + 80\lambda^{4} L^{2} \phi^{3} + 80\lambda^{4} L^{2} \phi^{2} + 80\lambda^{4} L^{2} \phi^{2} + 80\lambda^{4} L^{2} \phi^{3} + 8$$

$$\frac{\partial G_{l_1}}{\partial \omega^2} = e^{-\psi^2} \frac{1}{\sqrt{\pi}} \left( \frac{1}{\lambda} L^{3/2} + 64\lambda L^{5/2} + 112\lambda^2 L^3 \phi + 64\lambda^3 L^{7/2} \phi^2 + 64\lambda^3 L^{7/2} + \frac{32}{3} \lambda^4 L^4 \phi^3 + \frac{80}{3} \lambda^4 L^4 \phi \right) - e^{\Omega} \operatorname{erfc} \phi \left( 9L^2 + 64\lambda L^{5/2} \phi + 112\lambda^2 L^3 \phi^2 + 56\lambda^2 L^3 + 64\lambda^3 L^{7/2} \phi^3 + 96\lambda^3 L^{7/2} \phi + \frac{32}{3} \lambda^4 L^4 \phi^4 + 32\lambda^4 L^4 \phi^2 + 8\lambda^4 L^4 \right)$$

$$\begin{split} \mathbf{G}_5 &= -\mathrm{erfc} \ \psi - \mathrm{e}^\Omega \mathrm{erfc} \ \phi \left( -1 + 4 \lambda \sqrt{\mathbf{I}} \phi + 16 \lambda^2 \mathbf{I} \phi^2 + 8 \lambda^2 \mathbf{L} + \frac{128}{3} \ \lambda^3 \mathbf{L}^{3/2} \phi^3 + \\ & 64 \lambda^3 \mathbf{L}^{3/2} \phi + 32 \lambda^4 \mathbf{L}^2 \phi^4 + 96 \lambda^4 \mathbf{L}^2 \phi^2 + 24 \lambda^4 \mathbf{L}^2 + \frac{128}{15} \ \lambda^5 \mathbf{L}^{5/2} \phi^5 + \\ & \frac{128}{3} \ \lambda^5 \mathbf{L}^{5/2} \phi^3 + 32 \lambda^5 \mathbf{L}^{5/2} \phi \right) + \frac{1}{\sqrt{\pi}} \left( 4 \lambda \sqrt{\mathbf{L}} + 16 \lambda^2 \mathbf{I} \phi + \frac{128}{3} \ \lambda^3 \mathbf{L}^{3/2} \phi^2 + \right. \\ & \frac{128}{3} \ \lambda^3 \mathbf{L}^{3/2} + 32 \lambda^4 \mathbf{L}^2 \phi^3 + 80 \lambda^4 \mathbf{L}^2 \phi + \frac{128}{15} \ \lambda^5 \mathbf{L}^{5/2} \phi^4 + \frac{192}{5} \ \lambda^5 \mathbf{L}^{5/2} \phi^2 + \\ & \frac{256}{15} \ \lambda^5 \mathbf{L}^{5/2} \right) \mathrm{e}^{-\psi^2} \end{split}$$

$$\begin{split} \frac{\partial G_5}{\partial \xi} &= -\mathrm{e}^\Omega \mathrm{erfc} \ \phi \ \frac{1}{3} \bigg( 60 \lambda \mathrm{L}^{3/2} \phi + 240 \lambda^2 \mathrm{L}^2 \phi^2 + 120 \lambda^2 \mathrm{L}^2 + 320 \lambda^3 \mathrm{L}^{5/2} \phi^3 + \\ & 480 \lambda^3 \mathrm{L}^{5/2} \phi + 160 \lambda^4 \mathrm{L}^3 \phi^4 + 480 \lambda^4 \mathrm{L}^3 \phi^2 + 120 \lambda^4 \mathrm{L}^3 + \frac{128}{5} \lambda^5 \mathrm{L}^{7/2} \phi^5 + \\ & 128 \lambda^5 \mathrm{L}^{7/2} \phi^3 + 96 \lambda^5 \mathrm{L}^{7/2} \phi + 3 \mathrm{L} \bigg) + \frac{1}{3 \sqrt{\pi}} \bigg( 60 \lambda \mathrm{L}^{3/2} + 240 \lambda^2 \mathrm{L}^2 \phi + 320 \lambda^3 \mathrm{L}^{5/2} + \\ & 320 \lambda^3 \mathrm{L}^{5/2} \phi^2 + 160 \lambda^4 \mathrm{L}^3 \phi^3 + 400 \lambda^4 \mathrm{L}^3 \phi + \frac{128}{5} \lambda^5 \mathrm{L}^{7/2} \phi^4 + \frac{576}{5} \lambda^5 \mathrm{L}^{7/2} \phi^2 + \\ & \frac{256}{5} \lambda^5 \mathrm{L}^{7/2} \bigg) \mathrm{e}^{-\psi^2} \end{split}$$

$$\frac{\partial G_5}{\partial \omega^2} = -e^{\Omega} \operatorname{erfc} \, \phi \left( 11L^2 + 100\lambda L^{5/2} \phi + 240\lambda^2 L^3 \phi^2 + 120\lambda^2 L^3 + \frac{640}{3} \lambda^3 L^{7/2} \phi^3 + 320\lambda^3 L^{7/2} \phi + \frac{224}{3} \lambda^4 L^4 \phi^4 + 224\lambda^4 L^4 \phi^2 + 56\lambda^4 L^4 + \frac{128}{15} \lambda^5 L^{9/2} \phi^5 + \frac{128}{3} \lambda^5 L^{9/2} \phi^3 + 32\lambda^5 L^{9/2} \phi \right) + \frac{1}{3\sqrt{\pi}} \left( 300\lambda L^{5/2} + 720\lambda^2 L^3 \phi + 640\lambda^3 L^{7/2} \phi^2 + 640\lambda^3 L^{7/2} \phi^2 + 224\lambda^4 L^4 \phi^3 + 560\lambda^4 L^4 \phi + \frac{128}{5} \lambda^5 L^{9/2} \phi^4 + \frac{576}{5} \lambda^5 L^{9/2} \phi^2 + \frac{256}{5} \lambda^5 L^{9/2} + 3L^{3/2} \frac{1}{\lambda} \right) e^{-\psi^2}$$

#### APPENDIX C

NUMERICAL COMPUTATIONS FOR THE VARIOUS 
$$G_n$$
,  $\frac{\partial G_n}{\partial \omega^2}$ , AND  $j \frac{\partial G_n}{\partial \xi}$ 

The computations necessary to evaluate the equations of appendix B were carried out on a card-programed calculator. On this machine, the number of significant figures in any computational step was limited to eight, a limitation which resulted in a progressive diminishing of the significant figures in the answers as the value of n increased at a given  $\lambda$  and L. The reason for the loss of significant figures is the fact that each answer (except for  $\frac{\partial G_O}{\partial \xi}$ ) is the difference between two numbers; thus, when these numbers become large and nearly equal, the resultant difference has few significant figures.

It was also found that the complimentary error functions had to be computed to within a very small fraction of a percent of the correct value in order to obtain usable accuracy. The above-mentioned subtraction of two large but nearly equal numbers, one of which contains the complimentary error function as a multiplier, is the reason for the particular accuracy required. The following expressions were used to compute the complimentary error function of  $\phi$  and  $\psi$  in the ranges of the arguments listed ( $\phi$  is taken as the illustrative argument):

erfc 
$$\phi = \frac{2}{\sqrt{\pi}} e^{-\phi^2 \left( a_1 \eta + a_2 \eta^2 + a_3 \eta^3 + a_4 \eta^4 + a_5 \eta^5 \right)}$$
  $(0 \le \phi < 2)$  (C1)

where

$$\eta = \frac{1}{1 + 0.32759110}$$

 $a_1 = 0.22583685$ 

 $a_2 = -0.25212867$ 

 $a_3 = 1.2596951$ 

 $a_h = -1.2878225$ 

 $a_5 = 0.94064607$ 

erfc  $\phi = 0.00040695202 - 0.0021782842\epsilon \left(1 - 2.5\epsilon + 3.8333333\epsilon^2 - 3.9583333\epsilon^3 + 2.80833333\epsilon^4 - 1.2847222\epsilon^5 + 0.24900794\epsilon^6 + 0.11966766\epsilon^7 - 0.11490024\epsilon^8 + 0.036175871\epsilon^9\right)$   $(2 \le \phi \le 2.8)$  (C2)

where  $\epsilon = 0 - 2.5$  and

erfc 
$$\phi = \frac{1}{\sqrt{\pi}} \frac{e^{-\phi^2}}{\phi} \left[ 1 - \frac{1}{\chi} + \frac{1 \cdot 3}{\chi^2} - \frac{1 \cdot 3 \cdot 5}{\chi^3} + \frac{1 \cdot 3 \cdot 5 \cdot 7}{\chi^4} - \frac{1 \cdot 3 \cdot 5 \cdot 7 \cdot 9}{\chi^5} + \frac{1 \cdot 3 \cdot 5 \cdot 7 \cdot 9 \cdot 11}{\chi^6} - \frac{1 \cdot 3 \cdot 5 \cdot 7 \cdot 9 \cdot 11 \cdot 13}{\chi^7} \right] \left[ 1 + e^{-\phi^2} \left( 14 \cdot 695 - \frac{76 \cdot 331}{\phi} + \frac{104 \cdot 18}{\phi^2} \right) \right]$$
 (2.8 <  $\phi$  <  $\infty$ ) (C3)

where  $x = 20^2$ .

Equation (C1) is the approximation found on page 169 of reference 6. The errors introduced by this approximation became unacceptable in this application above a value of the argument of 2. Equation (C3) was originally thought to be useful in the range of arguments from 2 to  $\infty$  since the product of the first bracketed expression and  $\frac{1}{\sqrt{\pi}} \frac{e^{-\sqrt{2}}}{\phi}$  represent the first eight terms of the semiconvergent series for erfc  $\phi$  valid for large  $\phi$  and the constants of the second bracketed expression are chosen to give true answers at  $\phi = 2$ , 2.5, and 3. However, it was discovered that this equation was also unacceptable in the range  $2 < \phi < 2.8$ . A usable equation (eq. (C2)) for this range was found by employing the first 10 terms of the Taylor expansion of erfc  $\phi$  about the point  $\phi = 2.5$ .

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# THE IN I. := COMPUSED VALUES OF $G_{n_1}$ , $1\frac{\partial G_{n_2}}{\partial g}$ , And $\frac{\partial G_{n_1}}{\partial g^2}$ for n=0 to 5 and integers.

#### VALUES OF P FOR VARIOUS VALUES OF L AND A

(a) L = 0.001,

Pn	O <sub>n</sub> (P)	) gr <sup>j</sup>	9. 5 90"	Pn	G <sub>n</sub> (P)	1 <u>96</u> f	90°5	P n	G <sub>n</sub> (P)	1 <u>9f</u>	30 30 30°2	
L	λ = 0.02											
0 0 2 1 4 2 6 3	0.71330000 × 10 <sup>-3</sup> .78778800 × 10 <sup>-3</sup> .14221489 × 10 <sup>-8</sup>	-0.99968667 × 10 <sup>-5</sup> 25323594 × 10 <sup>-8</sup> 27570915 × 10 <sup>-8</sup> o(10 <sup>-13</sup> )	0.89106275 x 10 <sup>-3</sup> .73148921 x 10 <sup>-4</sup> .40460842 x 10 <sup>-7</sup> o(10 <sup>-12</sup> )	2 0 4 1 6 2	0.78840000 × 10 <sup>-5</sup> .14225740 × 10 <sup>-8</sup> .0(10 <sup>-1/4</sup> )	-0.25339356 × 10 <sup>-8</sup> 77399352 × 10 <sup>-8</sup> 0(10 <sup>-13</sup> )	0.73199582 × 10 <sup>-1</sup> .40476921 × 10-7 o(10 <sup>-12</sup> )	3 2	0.11842000 × 10 <sup>-3</sup> .18702 <b>4</b> 80 × 10 <sup>-6</sup> 0(10 <sup>-11</sup> )	-0.26545419 x 10 <sup>-3</sup> 79567516 x 10 <sup>-6</sup> o(10 <sup>-10</sup> )	0.47782504 × 10 <sup>-5</sup> .32148902 × 10 <sup>-5</sup> 0(10 <sup>-9</sup> )	
						λ = 0.06						
0 0 2 1 4 2 6 5 8 4 10 5	0.2276000 x 10 <sup>-2</sup> .7083960 x 10 <sup>-3</sup> .12981845 x 10 <sup>-3</sup> .23913870 x 10 <sup>-4</sup> .21725620 x 10 <sup>-5</sup> .12376640 x 10 <sup>-6</sup>	-0.99786298 x 10 <sup>-3</sup> 37992972798263927182172 x 10 <sup>-4</sup> 28394702 x 10 <sup>-6</sup>	0.29675615 × 10 <sup>-5</sup> .22367069 .97206756 × 10 <sup>-5</sup> .24231467 .5466884 × 10 <sup>-5</sup> .26451641 × 10 <sup>-6</sup>	2 0 4 1 6 2 8 3 10 4	0.70860000 × 10 <sup>-3</sup> .1601080 .2753408 × 10 <sup>-1</sup> .21788900 × 10 <sup>-5</sup> .12773466 × 10 <sup>-6</sup>	-0.45554779 × 10 <sup>-5</sup> 1555561225229222 × 10 <sup>-4</sup> 6555846 × 10 <sup>-5</sup> 19282515 × 10 <sup>-6</sup> 76975870 × 10 <sup>-8</sup>	.97479558 × 10 <sup>-1</sup> .84851678 .34719858 × 10 <sup>-5</sup> .86490151 × 10 <sup>-6</sup>	5 1 5 2 7 5 9 4	0.12860700 × 10 <sup>-2</sup> .55402510 × 10 <sup>-3</sup> .64909676 × 10 <sup>-4</sup> .75987500 × 10 <sup>-5</sup> .7522765 × 10 <sup>-6</sup> .24412690 × 10 <sup>-7</sup>	-0.70810226 × 10 <sup>-5</sup> 2664887262082072 × 10 <sup>-5</sup> 90342175 × 10 <sup>-5</sup> 79124666 × 10 <sup>-6</sup> 41142490 × 10 <sup>-7</sup>	.15857527 .52085864 × 10 <sup>-5</sup> .98527275 × 10 <sup>-5</sup> .10652666	
					<del></del>	λ = 0.10	L—	لسلسالا			<u> </u>	
0 0 2 1 4 2 6 3 8 4 30 5	0.75782000 × 10 <sup>-2</sup> .19054886 .89805062 × 10 <sup>-3</sup> .36773850 .12942502 .38815500 × 10 <sup>-1</sup>	-0.9964x183 x 10 <sup>-3</sup> 64898630 56698052 1712254 72464999 x 10 <sup>-3</sup> 84916962	0.17741597 × 10 <sup>-5</sup> .15947568 .11774972 .71268376 × 10 <sup>-1</sup> .77367461 .114568576	2 0 4 1 6 2 8 3 10 4 12 5	0.191k9800 × 10 <sup>-Q</sup> .90189750 × 10 <sup>-3</sup> .96906695 .1298k870 .98920878 × 10 <sup>-1</sup> .98730000 × 10 <sup>-5</sup>	-0.65280635 × 10 <sup>-5</sup> 569380411778591672724865 × 10 <sup>-4</sup> 2499469871810940 × 10 <sup>-5</sup>	0.160781k1 × 10 <sup>-5</sup> .11848469 .71643356 × 10 <sup>-4</sup> .35508651 .14418469 .47553030 × 10 <sup>-5</sup>	11   1	0.86501400 × 10 <sup>-8</sup> .13353592 .58642586 × 10 <sup>-3</sup> .22260210 .72448140 × 10 <sup>-1</sup> .19990280	-0.82041324 × 10 <sup>-5</sup> 49634395250606671159957843514728 × 10 <sup>-4</sup> 13694710	0.17518700 × 10-3 .13056495 .94187200 × 10-4 .51592956 .83154795 .85115798 × 10-5	
<u> </u>						λ = 0.20						
0 0 8 1 4 2 6 5 8 4	0.70968000 × 10 <sup>-2</sup> .52518250 .57469821 .26015410 .17478965 .11345101	-0.99890918 × 10-3 80725792 65576711 8558-071 35505771 85080271	0.88213301 × 10 <sup>-1</sup> .84560692 .77492948 .67782656 .56530327 .14920757	2 0 4 1 6 2 8 3 10 4 12 5	0.52868200 × 10 <sup>-2</sup> .37834780 .2625001 .17625774 .11434377 .715577010 × 10 <sup>-3</sup>	-0.81.777676 × 10-7 64369737 48906724 35857626 2500067 17168225	0.86187985 × 10-4 .10772011 .60777744 .97243967 .4548464 .94376987	10 31 32 73 94 115	0.61475600 × 10 <sup>-2</sup> .44668500 .51492684 .21507130 .14201454 .90550270 × 10-3	0.90882350 × 10 <sup>-3</sup> 7228860856022628418566773012905620859186	0.87747983 × 10 <sup>-1</sup> .82137441 .73462898 .68591755 .51000073 .395727900	
L.,			· · · · · · · · · · · · · · · · · · ·			λ = 0.40						
0 0 0 2 1 4 2 6 3 8 4 10 5	0.001124500 .011968211 .010088664 .84524140 x 10 <sup>-2</sup> .70353471 .35164440	-0.98 <del>780</del> 751 × 10 <sup>-5</sup> 874751A17713531867607754588787A3588781A8	0.k3617816 x 10 <sup>-k</sup> .k1633138 .39521381 .37823319 .3k771k67 .32135337	2 0 4 1 6 2 8 3 10 4 12 5	0.012289780 .000902064 .86843287 × 20 <sup>-2</sup> .71739480 .73867762 .48660860	-0.89874994 × 10 <sup>-3</sup> 79178386 69913430 60879478 - <del>.5007846</del> 5 44618547	0.45486458 × 10 <sup>-41</sup> .4105040 .38598510 .3956847 .3386844	10 31 38 73 94	0.03150930 .01114098 .95371168 × 10 <sup>-2</sup> .77545770 .64641891 .53803930	-0.94286965 x 10 <sup>-3</sup> 85299550752001086550110549581675147700652	0.49591368 × 10 <sup>-4</sup> .41436346 .59120359 .36690388 .34046996 .31341379	

# There is, converse values of $q_{\rm pl}$ , $1\frac{3\Omega_{\rm pl}}{3\xi}$ , and $\frac{3\Omega_{\rm pl}}{3\xi}$ for n=0 to 5 and determine

(a) L = 0.002 - Continued

P 2	O <sub>12</sub> (2)	1 94 207	<b>₩</b>	7 2	G <sub>a</sub> (P)	3 <u>90</u> "	- 2	A	G <sub>n</sub> (T)	1 <u>2</u> 4	2
						), = 0.60				•	
99	0.020.054700	-0.91094750 × 10 <sup>-3</sup>	0.88779976 x 30 <sup>-3</sup>	П				10	0.080090090	-0.9500M187 × 10 <sup>-3</sup>	0.8 <b>076-778</b> x 10
치기	.0167337506	007/1400	,96996390	20	0.01907-180	-0.981×2986 × 10" <sup>3</sup>	0.28731491 × 10 <sup>-1</sup>	3 1	.017663480	006801.00	.86907055
A B	-036603660	796B3A8A	.2520186k	4 2	.036829986	82094050	,468480a	9 2	-meemakke	77155551	. 2517438Y
63	-01/16/4006	-,71747500	.036933.00	6 2	.02/r/As/e9	74619950	.45064036	7 3	-013 <del>3710</del> 336	-,69586547	-275 <b>-</b> 0333
하	-018505559	61199056	.02113665	4 3	.01.00000056	-,67039514	,43%4907K	94	.011869500	620954B6	.20005309
ud 3	.010981905	-,57861800	-a0680366	70/#	.01.1857 <b>A58</b>	60099759	,23,860e05	11 5	.0103733318	- 55000564	.a05\ra085
Ш		<u>.  </u>		29 5	•98053580 × 10 <sup>-8</sup>	5577 <del>45</del> 07	,20369119				
						) = 0-80					
9	0.027998200	-0,9780Å171× 10 <sup>-3</sup>	0.21365 <b>4</b> 69 x 30 <sup>-4</sup>					10	0.085956540	-0.95074468 × 10 <sup>-3</sup>	0.413/4097 x 10
의기	.03088800.	57049767	.1978 <b>9</b> 439		0.00600.65%	-0.98940968 x 30 <sup>-3</sup>	0.61227320 × 10 <sup>-1</sup>	3 1	.004000989	85895749	.19740177
비의	*089179977	19405556	,1906)96	1 4 2	.0651.T1866	65940926	.19749539	5 2	.001397325	77619685	.17937908
터커	.019756766	72780045	.16460079	6 2	.080680046	~-T281078*	-319 <del>40</del> 63-	1 7 3	,0190 <del>175</del> 11	70130137	,36400TO3
어서	.017900900	<del>(7-880)/-6</del>	.15160945	N 013	.010554147	66+64006	.36 <del>19100</del> 0	∥⋬⋡	.00.694.769.L	- 65572,548	.15180760
여기	.015650357	586557786	*73616100	ᄱ	.016300383	61858964	72724200	ᆘ屮᠈	.00.5070725	5725 <b>60</b> 83	.1399673R
Ш		<u> </u>	<u>                                       </u>	28 5	-coarcockers	25656559	-1999TQ19	Ш			
						λ = 1.0					
ماما	0.034705900	-0.95589909 × 30 <sup>-3</sup>	0.16873947 × 30 <sup>-3</sup>					10	0.055†i68en	-0.9480125 × 1075	0.16 <b>7003</b> 71 × 10°
취	.031039 <del>100</del>	8676787A	.15090589	20	0.098809070	-0.95150001 × 10 <sup>-3</sup>	0.16201269 × 10-1	ᄩᆀ	.050179185	- काराजा	.353145318
시험	-027190390	19056543	.13519867	1 1 2	·005587559	- 83744336	.150,51017	5 2	.005975702	~,76689679	.13336676
43	994F18400	,700000006	-121300H5	6 8	.006026974	103/07/03	*7 <del>2061,1</del> 78	7/2	,00A191751	-,69006644	.12176097
하	.0221505	-,63425788	.10905809	63	·065457568	6(16(105)k	1385126210	∥ 91∙	,001,5689T7	-,69130616	.10951-905
(1)	,aragentan	-,56g5e635	.981254260 x 10 <sup>-7</sup>	ᄱ	.000550005 -	6103 <del>3099</del>	,10998081.	щ⁵	.019 <b>665999</b>	77967919	.98741540 × 10
Ш		<u> </u>		123	ermeyam.	<del></del>	,9 <b>92059</b> 40 x 16 <sup>-5</sup>	Ш		<u></u>	
						λ = 1.8	_				
	0.641/129900	-0,99998094 × 10 <sup>-3</sup>		П		_		10	0.010467700	-0.94466990 x 10 <sup>-3</sup>	0.15580\5\ × 10
획사	.0969 <b>(</b> 4613	854e4705	-ranyagelo		0.0995@9890			∥ ≱ı	-00611160ED	84909149	O\$7584EL,
비비	-098997393	-, 76165336	70398888	H1	.090 <b>00</b> 0690	8299135	.19190775	∦ × ∗	-0599A30TA	transp	.10658958
44	.029 <del>16</del> 7766	67959804	.92556390 × 20 <sup>-5</sup>	6 2		<b>1</b> -033698	.30673094	∥ार्थः	.000700700	<b>67011901</b>	.950541No x 345°
하	.0963242290	60635767	.80808peo	8 3		6601933.9	.95*60#10 × 10 <sup>-5</sup>	94	.007711972	590av511	.813800m0
여기	CETTOTEL	24142711	.poptope	10 4	.0E3117704	290003126	.81,908/80	14  2	-0 <del>22</del> 9697 <del>3</del> 5	534360HS	, OLEMENT,
Ш				197	.000435900		.71794500				
						λ - 1,4					
dol	0.046079800	-0.90194064 × 30 <sup>-3</sup>	0.13779000 × 10 <sup>-3</sup>					10	0,047213646	-0.5400\h395 × 10 <sup>-5</sup>	0.11001974 × 10
회사	.oks6897110	85646955	-300k3.05T		o.#61 <del>,075</del> 0	-0.98833801 × XI <sup>-3</sup>	0.11 <b>00090</b> 4 x 10-4	31	,0 <del>13212610</del> 70 <del>0032</del> 140,	889A15A8	.10006675
뉙히	.07 <del>1980</del> \12	T+057775	,0000000 × 10-5	4 1	,0A1051497	41937 <del>138</del>	,20000998	52	-057290706	-,7518e9e1	.87670610 x 10
이기	.033706320	673017332	.TM53640	6 2	.0964653.06	7236420	.060026070 × 10 <sup>-5</sup>	5 ± 17 3	·033036990	64:50@Ag6	· 12786970
예시	.0099602TI	57635448	.63000730	8 7	.076A1A570	-,63038985	.73169570	إداوا	.00555F1.9T	770 <b>08</b> 41	. <b>617687</b> 90
예키	.086677090	50658\30	.513 <b>998</b> 110	10 4	BOACHECKED.	-,5655158	,620 <del>0,70</del> 60	11/5	.006333400	50521760	.53,963000
11			l	12 5	,025650960	~,49799860	.5257-550			1	

## Should I.- congruence values of $a_n$ , $a \frac{\partial a_n}{\partial \xi}$ , and $\frac{\partial a_n}{\partial z^2}$ for n=0 to 5. And integrates

#### VALUES OF P FOR VARIOUS VALUES OF L AND $\lambda$ - Continued

(a) L = 0.001 - Continued

PD	G <sub>g</sub> (P)	1 ge	9 <b>2</b> 5	Pa	o <sub>n</sub> (P)	1 <u>90</u>	8 8	₽	n	<b>4</b> (P)	1 <u>9f</u>	2 <b>3</b> 5
						λ = 1.6			_	· · · · · · · · · · · · · · · · · · ·		
00	0.05%626200	-0.94557583. x 10 <sup>-3</sup>	0.10205401 x 10 <sup>-1</sup>	١ ١				1	ļ۵	0.055685850	-0.93316365 x 115 <sup>-5</sup>	0.10214525 × 10
2 1	.045212350	82397723	.84725540 x 20 <sup>-15</sup>	200	0.052 <del>7550</del> 00	-0.92494596 x 10 <sup>-5</sup>			치	.04759263.0	81549873	.64960450 x 10
4 2	.042555562	71785096	.69925770	¥ 1	.046581450	-,80698599	.85273940 × 20 <sup>-5</sup>	1	Яa	,0418 <del>99</del> 144	7308k079	.10272980
6 3	.0 <del>3 (3</del> 61920	62510547	.57751.0470	6 2	.041331780	10719745	10599470	H.	d 커	,0 <del>36</del> 959680	61955045	.57744270
8 4	.053157146	5N407N90	.16580500	l 워크	.056325220	- 61355593	-58357830	1	회사	.099615767	59959170	.kγση9890
ᄢᆌ	.029271620	47550910	57479100	10	.032078734	- 53465940	,4 <del>75,788</del> 00	ľ	식키	.02880053.0	46955400	.36023940
Ш			<u> </u>	12 5	.0283332500	16570500	.38550200	L	LJ	<u> </u>	_ <del></del>	L. <u></u> .
						λ = 1.8	,		т 1			<del></del>
이이	0.061122700		0.89729898 x 30 <sup>-5</sup>			_	l	10		0.060087620	-0.92990053 x 10 <sup>-3</sup>	
ᆁᅬ	.07575763320	80611754	-795879 <b>4</b> 0		0.059262250	-0.92090590 × 10-3		18 1	키긕		80064777	.72802220
4 2	.046982708	69474085	.580.28750	4 1		- 1798557750	75001540	PM .	현		68891250	.58434260
6 3	OY08401.40.	59650111	.A9939890	6 8		68505390	,58755140	1	7 3	.040455820	59188731	.46550540
하니	053901350	-,51143940	.35728510	B 3		58725551	467 <b>0</b> 9260	1	위식	.055421.971:	90784460	.96169110
띠키	.031146590	~.457 <del>84</del> 540	.277.61.990	10	1	50420610	.366021-90	1.	비키	.051009980	4853.0080	.27666330
Ш			<u> </u>	12 5	.050576550	43831080	.261,78200	L	Ш	L		<u> </u>
						λ = 2.0						
이	0.067547800	-0.55845880 x 10 <sup>-3</sup>	0.79881682 × 10 <sup>-5</sup>	П		- [		1	ųο	0.06661,9290	-0.92446044 x 10 <sup>-3</sup>	0.79976034 × 10
립기	.058666690	-, 19809630	.62955723	20	0.065698740	-0.91616133 x 10-5	0.80019998 x 10 <sup>-7</sup>	1	5 2	.007977400	78579330	.63128981
부호	.05092621.7	673/6002	.A880A169	4 2	.057094870	? <del>79</del> 47209	.65513580	1	5 2	-0508577298	-,666 <del>5555</del> 08	.49090076
6 3	.044185080	5678561.0	. <del>77</del> 07050	6 2	.049595158	66165256	.49565526	M ·	73	.043617320	56413157	.574422570
하니	.05853.0043.	479006 <del>8</del> 0	.arp310460	8 3		56037197	-37T64250	111	9 4	.0518522704	476ak990	.27767880
비키	0.055309853.0	~.40899680	19592520	10 4	-05779577430	-6 M29/2210	.251,560\to	1112	ᄬ	:.098796300	-140095720	19819570
Ш			<u>                                     </u>	18 5	-052596080	59895440	.20257550		L	<u> </u>		<u> </u>
						λ = 2.5			_			
90	0.085509600		0.62198007 × 10 <sup>-5</sup>	1.1					40	0.082595580	-0.910\6798 × 10 <sup>-3</sup>	1
격기	.07067 <del>31</del> 470	75007846	.45747980	2 0	0.081488470	1 -	0.6g33156 × 10 <sup>-5</sup>	HI I	71	.069922730	14749569	15901209
취임	.059854181	61,586582	.32187536	רול ו	.069277980	TA289791.	.16051976	ш	32		61060571	.30711360
92	.0506090.90	19808800	·12376169	6 8		6075E547	.38950279	Ш	73		49588720	.2013/1969
하시	.012697162	- 40135160	.13459000	8 5		-,49565940	.2540911A	111.	9*	,042396651,	39999080	.1575\600
岣키	.055951570	36075850	.6879#700 × 10 <sup>-6</sup>	10	1	39860090	.74655800 x 20 <sup>-6</sup>	淵	<b>ካ</b> ን	.055650750	32005350	.71608400 x 10
Ш				18/2	.055511240	31952010	1 -140) X UU -	14	_	<u> </u>		<del> </del>
_				1		λ = 5.0	1	Т	_	r	т .	
	0.098653500	1 7 7 7	0.50\ <del>5</del> 7515 × 10 <sup>-2</sup>			a demokrati a - I			40	0.097752470	-0.89630029 x 10 <sup>-3</sup>	
21	.050,560,590	71989694	.34510985		0.096858500		0.50551719 x 10 <sup>-5</sup>		ᆉ		90956870	.54658452
12	.067920695	558559-30	.24118482	1		70589880	.54762634	Ш	월		55651359	.22296762
6 3	.05520690.0	45275960	.12605935	6 2		-,55407474	.29172279	ı	7?	.054774900	A51A8880	,12811858
8 4	.045362092	55069110	.54084460 x 30-6	8 2		4501,9730	.13017535	d.	9*	.044851648	55013960 c48c6770	.56500540 x 14
20 5	.076762750	248281AO	7-01 × 00007±17.	30		3E9965N0	.58496£10 x 10 <sup>-6</sup>	-18	┦?	.056533990	24896550	.29475000 × 10
13		1		122/2	.03695740	24822240	.51671000 x 10-7	1				

#### TABLES I.- CONFUSSION VALUES OF $G_{n}$ , $3\frac{\delta G}{\delta \epsilon}$ , AND $\frac{\delta G_{n}}{\delta \sigma^{2}}$ FOR n=0.50 ) AND INTERIORS.

#### VALUES OF P FOR VARIOUS VARIES OF L AND $\lambda$ = Continued

(a) L = 0.001 - Concluded

P n	G <sub>n</sub> (P)	1 <u>98 </u>	8 8	P	G <sub>n</sub> (P)	1 <u>90"</u>	92 <sup>2</sup>	P	n G <sub>n</sub> (P)	1 2d gar	90 <sub>7</sub>		
_	λ = 3.5												
00	0.115588%	-0,8 <b>86</b> +116 <b>2</b> × 10 <sup>-3</sup>	0.4E110658 x 10 <sup>-5</sup>				_	.:	0 0.33270408	-0.88219846 x 10 <sup>-3</sup>	0.40051949 x 10-2		
2 1	.091100110	67475740	.a6663613	20	0.11182505	-0.87798339 x 10 <sup>-5</sup>	0.4E393000 x 10 <sup>-5</sup>	:	2 .090726820	-,67206575	<b>.2676954</b> 8		
4 2	.075172778	50617490	.15117795	*1	.090036040	- ,66940366	.96875580	:	2 .07956740.5	50467580	15069057		
6 3	.058e\ee50	<del>7727</del> 1680	.6646£130 x 10 <sup>-5</sup>	6 2	.072165526	50312260	,15404606	111	5 .057870030	~.57204400	.68093060 x 10=0		
8	.046049 <b>16</b> 6	86780730	.51940100 × 10-1	8 3	.057498190	57135510	.69710970 x 20 <sup>-6</sup> .91440100 x 20 <sup>-7</sup>		045761781	-,26774080	.74745000 x 10 <sup>-7</sup> 34569700 x 10 <sup>-6</sup>		
끡?	.036128550	18601580	96225400 x 10 <sup>-6</sup>	30 t	.045513899	26765770 18670650	-,5296A000 x 10-6	∭~	055942040	18636890	1.74709100 X M-1		
Щ.	l		L	18 5	.035755780		-,,x,D+X X X0 -	111	<del></del>	J	<u> </u>		
_	λ = 4.0 0 0.1272560 -0.87236699 × 10 <sup>-3</sup> 0.776984436 × 10 <sup>-3</sup> 0.57519644 × 10 <sup>-3</sup> 0.5751964 × 10 <sup>-3</sup> 0.575196 × 10 <sup>-3</sup> 0.57519 × 10 <sup>-3</sup> 0.575196 × 10												
	0,10035560			l .l.		A not court sand	0.35955492 × 10 <sup>-5</sup>	111	1 1	1			
E 3	10024654	63803905	.20986277	R O	0,12639707	-0,86468866 x 10 <sup>-3</sup> 63363613	.e1107665	ın '	099609890 8 .077590850	6759A195 40598980	.21015700 .10515781		
		45701450	.10153577	6 2	.098975180 .076954905	0505015 45195150	.10\51027	1111	0.00103000	51781090	.a6501/50 x 10-6		
6 3		51808750	.27006790 x 10 <sup>-6</sup>	8 3	.059295440	51752150	.29586570 × 10-6	111	44.0454461.44	- 21279480	- 283,54850		
8 4	,045661021 art-record	-,91296700	25420400 95496400	30 4	.0\9255860	21500980	20853770			15596450	5A296500		
20 5	.0545759010	1,5541,560	33490400		.091090920	-,13450140	53100500	肵	11 //		*****		
	12 5 .09409092013450000  53100900												
7.	0.18295190	-0.81754813 × 10 <sup>-3</sup>	0 31561000 × 10-2	ГΤ				T :	1 0 0.18185553.	-0.61519086 × 10 <sup>-3</sup>	0.21505267 × 10-2		
<b>a</b> ;	.19689796	5051860.6	.84e21480 x 10 <sup>-6</sup>	90	0,18109138	-0.81305UA × 10-7	0.2160\a65 × 10 <sup>-5</sup>	Ш,	3 1.18656876	50433752	.54727750 × 10-6		
1,		29152560	.57296A00.x 10 <sup>-7</sup>	1 1		50348748	.85630970 × 10 <sup>-6</sup>	IN :	2 .085851050	29036570	.63210600 × 10-7		
٦,	.056940880	-,1/899900	77129400 × 10-6	6 2	1	291,39950	.69104300 x 10*?		056690420	1A536760	96571800 x 10-6		
ali	.036038040	57255600 × 10-1	56705800	8 5	.056541960	=.1A9750N0	56015540 × 10 <sup>-6</sup>	Ш	94 .055975340	57790500 x 10 <sup>-1</sup>	96240000		
10		85000000 x 10-6		10	.055917340	58680700 × 10 <sup>-1</sup>	-,55777600	II	1 5 .020,5120,40	1M656000 × 1.0 <sup>-5</sup>	61344500		
I.				18 5	.021510020	201712000 × 10-5	60997700		<u>                                     </u>	<u> </u>			
						λ = 8.0			· · · · · · · · · · · · · · · · · · ·		,		
a	0.25186150	-0.76815550 × 10 <sup>-3</sup>				_			1 0 0.85109701		0.13654758 × 10-7		
9	.14162532	393253.95	.50645340 x 10 <sup>-6</sup>	20	0.25055184		0.14649118 x 10 <sup>-5</sup>	1111	1 .1k185848	- 59294596	.50964700 x 10 <sup>-6</sup>		
4	.082454311	16953690	£491,3940	+ 1	.14085986	-,39063049	.31263200 x 10-6	Ш	2 .052254754	-,16958680	#1590090		
6	,0 <del>116113670</del>	1310+300 × 10 <sup>-1</sup>	-,1/5560090	6 2	li .	- 169853.00	24266570	Ш	7 5 .044568510	43059800 × 10 <sup>-1</sup>	li .		
a i	.000189650	.23,705400	k†26\100	8 3	.044524590	-,W010800 × 10-		111	o⊊⊔23120.  4¢	.#1831000	471.22700		
~	,75k12000 × 10 <sup>-12</sup>	ACCOM.	39950900	120 5		,20761000 ,48556600	46960700 59799900	ll <sup>p</sup>	1 5 .T3900.000 × 10 °	.48995700	39875500		
_				<u>                                     </u>	1,1,2,2,4	λ = 12.0		Ш			· · · · · · · · · · · · · · · · · · ·		
7	0.53699030	_0_68#110 <b>6</b> 8 v 10 <sup>-2</sup>	0.80565050 × 10 <sup>-6</sup>	ТТ	T	I	1	W	1 0 0.31619769	-0.68231575 x 10 <sup>-3</sup>	0.80445180 × 10-4		
2	.1/199818e	-,2301340 X 20 ·	96675000 x 10-7	وأع اا	0.51551565	-0.68153076 × 30°	0.80024890 x 10-6		3 1 .14536115	-,22050950	95179600 × 10		
- 71	.056646480	1881.6400 × 10 <sup>-14</sup>			.16514101	22060990	99678400 x 10 <sup>-7</sup>		9 .056627600	19149000 x 10 <sup>-4</sup>			
a	.ш.уулуюю	.51105100	29932300	6 8	,056608450	-,19480400 × 10 <sup>-1</sup>	-,53094660 x 10 <sup>-6</sup>		7 3 .00/1008500	.50806700	29 <b>00760</b> 0		
a	38652000 × 10 <sup>-2</sup>	.607213.00	18720200	8 2	.00/1078700	.50507900	298453.00		9 458050000 × 10 <sup>-4</sup>	,605528000	187#100		
10	T	A7362000	<del>793</del> 68000 × 10 <sup>-7</sup>		1	,60546600	18727300	ᆒ,	1 590,958000	,4 <b>726500</b> 0	79869000 x 10		
			j	12	,9245 <b>7900</b> 0	.17201000	80160000 x 10 <sup>-7</sup>		<u></u>		L		

# There i. - computes values of $\sigma_n$ , $4\frac{\delta\sigma_n}{\delta\epsilon}$ , and $\frac{\delta\sigma_n}{\delta\sigma^2}$ for n=0 to 5. And different

#### VALUES OF P FOR VARIOUS VALUES OF L AND $\lambda$ - Continued

(b) L = 0.005

P n	G <sub>n</sub> (P)	ગ <u>છુક</u> જુવ્ય	95. 97.	P n	G <sup>B</sup> (3-)	2 <u>98</u> 900°	38 <u>1</u> 3m <sup>2</sup>	]	n	Ū <sub>n</sub> (₽)	1 <u>97</u>	94 <sub>5</sub>
	λ = 0.02											
0 0 2 1 4 2	0:15959000 × 10 <sup>-2</sup> .21362600 × 10 <sup>-9</sup> 0(10 <sup>-26</sup> )	-0.49920708 × 10 <sup>-8</sup> 28633011 × 10 <sup>-8</sup> 0(10 <sup>-85</sup> )	0.99485970 × 10 <sup>-2</sup> .57125006 × 10 <sup>-7</sup>	20	0.21379000 × 10 <sup>-9</sup> 0(10 <sup>-26</sup> )	-0.29654382 × 10 <sup>-8</sup> 0(10 <sup>-25</sup> )	0.37153660 × 10 <sup>-7</sup> 0(10-25)		1 0 3 1	0.80110000 × 10 <sup>-5</sup> 0(10 <sup>-16</sup> )	-0.62056725 × 10 <sup>-1</sup> 0(10 <sup>-1,5</sup> )	0.43789710 × 10 <sup>-5</sup> 0(10 <sup>-14</sup> )
			•	I								
00 21 42 65	0.47696000 × 10 <sup>-2</sup> .23632080 × 10 <sup>-3</sup> .13370168 × 10 <sup>-3</sup> .63676200 × 10 <sup>-9</sup> 0 (10 <sup>-13</sup> )	-0.49761522 × 10 <sup>-9</sup> 47434759 × 10 <sup>-3</sup> 42571094 × 10 <sup>-5</sup> 28441385 × 10 <sup>-8</sup> 0 (10 <sup>-12</sup> )	0.32996382 × 10 <sup>-2</sup> .82183707 × 10 <sup>-5</sup> .12745502 × 10 <sup>-1</sup> .12289401 × 10 <sup>-7</sup> 0 (10 <sup>-12</sup> )	20 41 62 83	0.23740100 × 10 <sup>-3</sup> .13589540 × 10-3 .63812230 × 10-9 o(10-33)	-0.47671619 x 10-5 48704791 x 10-5 28505125 x 10-8 0 (10-12)	0.82659258 × 10 <sup>-5</sup> .12768140 × 10 <sup>-4</sup> .12517874 × 10 <sup>-7</sup> o(10 <sup>-12</sup> )	1	1 0 5 1 5 2 7 3	0.13558500 × 10 <sup>-2</sup> .23922080 × 10 <sup>-3</sup> .40185541 × 10-7 o(10 <sup>-11</sup> )	-0.20165040 × 10 <sup>-2</sup> 6175750 × 10 <sup>-4</sup> 15555516 × 10 <sup>-6</sup> 0(10 <sup>-10</sup> )	0.23391829 × 10 <sup>-2</sup> .14514067 × 10 <sup>-3</sup> .56064111 × 10 <sup>-6</sup> .13478731 × 10 <sup>-9</sup>
19.	1 0 tan -7 .	J(W /	<u> </u>		- V	λ = 0.10		4	ш			
2 1 4 2 6 3 8 4 10 5	0.75891000 × 10 <sup>-2</sup> .16438811 .16695475 × 10 <sup>-3</sup> .75017800 × 10 <sup>-5</sup> .14012802 × 10 <sup>-6</sup> .10483080 × 10 <sup>-8</sup> 0.015759900 .76640470 × 10 <sup>-2</sup>	15617475 22528242 × 10 <sup>-5</sup> 13624000 × 10 <sup>-4</sup> 31054302 × 10 <sup>-6</sup> 28062806 × 10 <sup>-8</sup>	.21691526 x 10-4	8 3 10 4 12 5	0.16587800 × 10 <sup>-2</sup> .16809710 × 10 <sup>-3</sup> .75425461 × 10 <sup>-5</sup> .14080570 × 10 <sup>-6</sup> .10720225 × 10 <sup>-8</sup> 0(10 <sup>-11</sup> )	-0.15782589 × 10 <sup>-2</sup> 28496768 × 10 <sup>-3</sup> 15309220 × 10 <sup>-4</sup> 31174766 × 10 <sup>-6</sup> 28187622 × 10 <sup>-8</sup> 0(10 <sup>-11</sup> ) λ = 0.20	0.12019626 × 10 <sup>-2</sup> .26656538 × 10 <sup>-3</sup> .21824242 × 10 <sup>-4</sup> .65815500 × 10 <sup>-6</sup> .75056941 × 10 <sup>-8</sup> 0(10 <sup>-10</sup> )	]       	5 1 7 3 9 4 1 5	0.79572800 x 10 <sup>-2</sup> .57989430 x 10 <sup>-3</sup> .5989340 x 10 <sup>-3</sup> .11508610 x 10 <sup>-3</sup> .12581615 x 10 <sup>-3</sup> o(10 <sup>-10</sup> )	-0.30556994 × 10 <sup>-2</sup> 65953777 × 10 <sup>-2</sup> 61102502 × 10 <sup>-2</sup> 22637023 × 10 <sup>-2</sup> 53557428 × 10 <sup>-2</sup> 18634761 × 10 <sup>-9</sup> -0.35563812 × 10 <sup>-2</sup> 22885594	.67(5)982 × 10 <sup>-3</sup> .86102008 × 10 <sup>-3</sup> .82827205 × 10 <sup>-5</sup> .78403905 × 10 <sup>-7</sup> .528134257 × 10 <sup>-9</sup>
6 5 8 4 10 5		15051664 66816499 × 10 <sup>-3</sup> 21269085 57631094 × 10 <sup>-4</sup>	.76632765 .7012998 .12708065 .40524958 × 10 <sup>-4</sup>	41 62 83 104 125	.32543630 .3254360 x 10 <sup>-3</sup> .7596180 x 10 <sup>-4</sup> .34415640	15373088 639351h9 × 10 <sup>-3</sup> 21589730 58586097 × 10 <sup>-k</sup> 12688595 h = 0.40	.760,74001 .70746756 .12722756 .41107027 × 10 <sup>-14</sup> .10760026		2 7 3 9 4 1 5	.19402750 .61481880 × 10 <sup>-5</sup> .15992952 .33798080 × 10 <sup>-1</sup>	10069986 37872279 × 10 <sup>-5</sup> 11883938 27880972 × 10 <sup>-4</sup>	. 153657714 . 16866960 . 74018382 × 10 <sup>-1</sup> . 21148694
0 0 2 1 4 2 6 3 8 4 10 5	.0114224616 .911421920 × 10-8 .56565966	-0.1845783 × 10 <sup>-8</sup> 36821742271082971859714213301172857547660 × 10 <sup>-5</sup>	0.47445616 x 10 <sup>-3</sup> .467591450 .56788655 .56786561 .2772668 .17600531	2 0 4 1 6 2 8 3 10 4 12 5	0.022590210 .018847700 .95120407 x 10-2 .5665750 .54764569 .19725380	-0.59009859 × 10 <sup>-2</sup> 201684921367742188765840 × 10 <sup>-3</sup>	.595782169 .52505061 .25050617		1 1 2 2 3 3 4 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0.026525050 .017905009 .011694785 .73662880 × 10 <sup>-2</sup> .44609264 .25905150	-0.43699983 × 10 <sup>-2</sup> 326198882352777163649901095640068968880 × 10 <sup>-3</sup>	0.47894715 x 10 <sup>-5</sup> .A106599 .54775469 .2955645 .21186721 .15170860

### There i... conform values of $G_{a}$ , if $\frac{\partial G_{a}}{\partial t}$ , and $\frac{\partial G_{b}}{\partial x^{2}}$ for a=0.20.5 and increase

#### VALUES OF P FOR VARIOUS WALKER OF L AND $\lambda$ - Continued

(b) L = 0.005 - Continued

P B	G <sub>k</sub> (P)	1 9t gaff	<u>a</u>	7 0	a <sub>n</sub> (P)	1 <u>9f</u>	9P5 92 <sup>3</sup>	1	n	G <sub>p</sub> (P)	<del>اری</del> د چوته	80 <u>m</u> 8m²	
	λ = 0.60												
00	0.0\6129200 .05\650121	-0.47693545 x 10 <sup>-2</sup> 57989381	0,30860513 × 10 <sup>-5</sup> .86738057	2 0	0.057207580	-0.41561961 × 10 <sup>-2</sup>	0.30710305 × 10 <sup>-3</sup>		1 0 5 1	0.041515970 .050970665	-0.44603680 x 10 <sup>-8</sup>	0.50099775 × 10 <sup>-5</sup> ,26619450	
4 2	.02575#A19	899AT548	.931 <b>he97</b> 2	41	.0275771148	38614027	.65071051		512	.021872942	27546562	268+5406	
6 3	.018944486	25425572	.19911036	6 2	.090921065	25385267	.22551647	Ш	캠케	.006700741	21457308	.19453415	
8 4	013768954	16180618	.16950153	8 3	.014651440	19541630	,18835265	Ш	외식	.019040653	26453570	.16370149	
10 5	,98746090 x 10 <sup>-2</sup>	138333.96	.1\ase578	1001	.010476080	11850751	.15665774	1	니키	•926732340 × 10−5	12442955	.13566910	
		•		12년 5	.75877610 × 10 <sup>-8</sup>	11122740	,19816895		Ш				
	λ = 0.60												
90	0.060762400	-0.46961688 × 10 <sup>-2</sup>	0. <b>20585798</b> × 10 <sup>-5</sup>	П						0.056178840	-0.44699883 × 10 <sup>-8</sup>	0.22650277 × 10 <sup>-5</sup>	
8 7	.047008480	- · 5T4-970754	,186e16†s		0.051502150	-0.42435067 x 30-2		Ш	커시	.045550660	-, 7,696659	.18700E14	
4 2	.056261512	29948 <b>367</b>	.15 <del>199667</del>	4 2	.059883360	35756650	.18684918	Ш	커의	.055564875	96 <del>594434</del>	15565879	
6 3	.027980890	25912555	.13001977	92	.050605599	90836535	,157)59522	111	기기	.027591000	~. <b>296</b> 09/ <u>(32</u>	.15055179	
8 4	.021/109525	19067643	.10968254	0 3	.025398360	21308025	.12987016		이네	015557269	17970166	-10962674	
ᄱᄝ	.016347 <b>58</b> 0	15169 <del>1</del> 05	-92620270 × 10 <sup>-1</sup>	10 4	.01781A990	16917550	.10684575	╢╸	식기	.018876970	142A£9£9	.92965240 × 10 <sup>-4</sup>	
			<u> </u>	145	.013498750	15504810	,91278030 × 10 <sup>-1</sup>	Ш	Ш			L	
	λ = 1.0												
00	0.075048600	-0.46247669 × 20 <sup>-2</sup>	0.17654781 × 10 <sup>-5</sup>	1		_				0.070505650	-0.14180616 x 10 <sup>-6</sup>		
2 1	058466890	36-75242	.13752676	1 1	0.066146220	-0.42709898 x 10 <sup>-2</sup>			키긔	.054887560	509件方	.15875091	
+ 2		26654960	.10821193	4 2	.051847590	35705835	.1391-9050	116	기의	.0\e73866\	STIO-90.3	10971946	
6 3	.077525970	- #2085047	.87991820 × 10 <sup>-4</sup>	6 2	.0\001.7556	-,26662133	.11076740		기키	.055278650	22016847	87575790 × 10-4	
8 *	.027690427	18194450	.69076640	8 3	.051121050	21175025	.86721370 × 10 <sup>-3</sup>		엠	.025905628	17495948	OFECTOR.	
씨키	·0#1576550	11499896	.56059040	10 4	.094191880	16764273 15748613	.71698090 .58427070	┉	비기	.0000,5200	15926167	·57 <del>12301</del> 0	
Ш	i			19 5	.018791.980		->01013400.	Ш.	Ш				
_						እ = 1-2	····	ш	_			<del></del>	
00	0.088983300	-0.45550945 × 10 <sup>-6</sup>	0.3A5A5OA8 × 30~3	1 1	0					0.084497860	-0.441133330 × 10 <sup>-0</sup>		
뷥	.069002900	57412536	.107771221 .77421040 × 10 <sup>-4</sup>	1 H 1	0.080358540 ,062398940	-0.48671401 x 10 <sup>-8</sup> 37080703	0.14451408 x 30 <sup>-5</sup> ,10760690		뷞	.065775\760 .05091.9579	5415909†	.10562679 .79074470 x 10 <sup>-1</sup>	
6 5	.053609157 .0k1690980	27290600 21210\17	.56963470	6 8	.048308381	2571.056R	.804e2870 x 10-4		43	.059598760	26507998 20651581	.50764630	
93	.039468795	16554950	.48055770	🏋	.0575653300	- 20055948	.60519050	Ш.	1.1	.030830578	-,1610A88A	.45862500	
י פוסנ	.085507850	14950575	.11268790	20 4	089248518	-,15658058	.N5\63110	,	];	.024030170	19609887	.39594000	
7			·3	125	.022785760	12279589	31190500	$\   \ $	71	roa ngomp		.,.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
	······································	· · · · · · · · · · · · · · · · · · ·	<del> </del>	<u></u>		λ = 1.4							
olo	0.10058850	-0.44870576 x 10 <sup>-8</sup>	0.1200410 x 10-3	П		l	î I	1	ᅵ이	0.098161590	-0.43667438 × 10 <sup>-9</sup>	0.12075484 × 10 <sup>-3</sup>	
21	.00000000	55853,802	.82740430 × 10 <sup>-4</sup>	P O	0.099654840	-0.42460090 x 10 <sup>-2</sup>	0.190 <b>666</b> 56 x 10 <sup>-3</sup>		ᅰ	.075369590	5899839R	.8551A450 × 10 <sup>-4</sup>	
4 2		25505551	.56076150	4 2	.072111510	- 32151086	.64915970 × 10 <sup>-1</sup>		9 2	.057955008	24956958	.57615970	
6 3	,o46496560	19275554	,57169860	6 2	.055460550	2577777	.589945330		ᅰᆀ	.044580000	18895189	56874790	
BA	.075805577	- 1k5725k9	25896480	8 3	.04271 <b>7</b> 980	16498519	,40A329000	1		.034360478	11524588	.256 <del>5</del> 4470	
10 2	.0848310020	11032537	.11698320	10 4	.058941089	14060116	.a7236630	1		.086705050	10877069	.16579570	
				18 5	.085455670	10705365	.17946970		П				

### THE E I.- COMPUTED VALUES OF $G_n$ , $3\frac{\partial G_n}{\partial t}$ , AND $\frac{\partial G_n}{\partial z^2}$ FOR n=0 10 5 AND INSTRUME

#### VALUES OF P FOR VARIOUS VALUES OF L AND $\lambda$ - Continued

(b)  $L = 0.005 \sim Costinued$ 

	G <sub>22</sub> (P)	i ge <sup>t</sup>	98,	Pa	G <sub>n</sub> (P)	1 22	<u>90</u> -	P	h	a <sub>n</sub> (P)	1 92 F	30,
	· · · <u>-</u> · ·					λ = 1.6			۰		<u></u>	
aol	0.11587430	-0.44206286 × 10 <sup>-2</sup>						בו		0.22250 <b>48</b> 5	-0.45178961 × 10 <sup>-2</sup>	0.10501948 × 10 <sup>-2</sup>
리시	.087570010	- 59ko5871	.660769710 x 10 <sup>-1</sup>		0.10725852		0.10335505 × 30-3	]] 2	14	084362690	31739594	.67141360 × 10-1
비외	.066197915	25692436	-4071427C	Ì <b>⊁</b> Þ	.063.262440	53065455	.68092190 x 10 <sup>-1</sup>		11	065819557	- 25278258	42100730
613 814	050059980	17270600	-25522900	6 2	.061542792	-,22850756	.45585770	]	13	.048344670	170R9697	-24842A70
	<b>05787195</b> 6	- 12547765	.11606960	8 3	.046654960	16774068	.26267870	II.'	11	.056625111	12425979	13036560
엑기	.028665610	908e6580 × 10 <sup>-3</sup>	139019100 × 10-5	10 4	055557657 095858850	329 <del>33</del> 300 89734970 × 10 <sup>-5</sup>	.67663600 x 10 <sup>-2</sup>	"	넴	.027759550	90562330 × 10 <sup>-5</sup>	•55685500 × 10*
	L	<del></del>	L			λ = 1.8		ш_	ш		-l	<del></del>
o o	0.12551650	-0.47577578 × 10-2	0.89058510 × 10 <sup>-1</sup>	ГΤ				<b>]</b> 1	ļ	0.18455710	-0.42665111 × 10 <sup>-0</sup>	a.89449000 × 10
2 1	099640090	30973268	-55590.770	20	0.12051520	-0.41769025 × 10-9	0.89761910 x 10 <sup>-1</sup>		Ы	.092569670	~- 30432501	.54546780
4 2		21861406	-25550720	4]1	.089753860	29884792	.55983780	ء اا	Ы	.068758590	21561713	-303110HO
6 3	.052511190	15894639	.13461770	6 2	.066597981	20250092	.31754150	1	dal.	.050988680	15155575	.JA780610
إباه	0588534505	10583468	.30494000 × 20-7	واھ ا	.04 <i>9</i> 480770	<u>11000011</u>	.16okoyko	و اا	1	-03177760h	- 10544410	.47518200 × 10-
اوام	.02667 <b>68</b> 00	72225590 × 10 <sup>-5</sup>	30723000	10/4	.056725948	10 <del>1925</del> TY	.58051600 × 10"5	Ju	45	.0279773260	72467040 x 10 <sup>-3</sup>	- 18294900
				12 5	.027229750	72590500 x 10 <sup>-5</sup>	64648000 × 10 <sup>-6</sup>	L	Ш			
						λ = 2.0						
90	0.1/152010	-0.42927981 × 10 <sup>-2</sup>	0.78275581 × 10 <sup>-1</sup>					נ	40	0-13726695	-0.42139595 × 10 <sup>-2</sup>	0-78654107 × 10*
21	.10295986	25548964	-45485050		0.15509250	-0.41551495 x 10 <sup>-8</sup>	0.76955036 x 10 <sup>-6</sup>	3	키긔	.10002676	29109719	.44359T3.0
¥٤	.07467875¥	20071449	.20773940	⊧ ı	.09713 <b>801</b> 0	28662270	.45138610	]]] •	기억	079581850	- 19858311	·21849030
6 3	.055979010	~- 15400524	.63612800 × 10⁻⁵	6 2	· OPOTOTOS	19694626	.2987 <del>მე</del> ნი		73	.052612270	13333025	-74940500 × 10
8 4	-058862529	- 87417950 × 10−5	~540 <b>8</b> 03.00	8 3	.051513010	15250572	.85881900 × 10-5		14	.057987597	87604050 x 10 <sup>-5</sup>	~*727.55800
o s	.027651350	55201,000	74006600	10 <del> </del> 4	.077111091	87682220 x 10 <sup>-5</sup>	[25650000 × 10 <sup>-6</sup> ]	լլիո	네티	027295910	55890A00	64043900
يا	<u> </u>	J	<u>[</u>	38 5	.026774110	56480600	-,54508500 x 10°5	W.	Ц	<u> </u>	<u> </u>	l
					<del>,</del>	λ = 2.5						
d٥	0.737352200	-0.43405834 × 10 <sup>-2</sup>		1		_		ш		0.16782489	-0.408109#1 × 10 <sup>-6</sup>	
21	_118ee368	~.26116136	-26450605		0.16377397		0.59616667 x 10°4	3	바	.11562525	~.258485k1	-27109106
뉙a		- 15897287	.6991/1000 × 10-5	1 4 2		25574.285	.27727083.	!!! 2	뵈	.078899965	- 15825361	.T7666300 × 10
43	054196690	- 91695970 × 10 <sup>-5</sup>	5 I	6 2		15741620	.85214800 x 10-2	1	13	075210120	~92019510 × 10 <sup>-3</sup>	30754600
8 4	055845850	~.¥826e500	94561100	8 3	.092257980	-,98588990 x 10 <sup>-3</sup>	aha69300	9	14	050557560	- 491,14500	57796000
405	-02 <del>3265</del> 670	20954600	11659720 x 10 <sup>-1</sup>	ᄤ		50078700	81130500	llþu	닉키	027070430	~-28092600	~,11099690 x 10=
1	<u>L</u>	<u></u>	<u>L</u>	12 5	.0886e4130	23174300	- 10554870 x 10-4	Ш	Ц			<u> </u>
_	,	<del></del>	····			λ = 3.0		III .	1			1
٩º	0.20051910		0.7620001E × 30-4	<u> </u>			la Mardade		• •	0.19567588	-0.39501352 × 10 <sup>-2</sup>	
<b>9</b> 1	.12958396	29916540	.1596@02	20	0.19274897	1	0.46956965 x 10 <sup>-1</sup>	III '	91	.32750058	2275k170	.16467787
为®		12254450	- 45198000 x 10 <sup>-6</sup>	1	.12705325	- 22567050	.1695 <b>017</b> 7		12	.08079490A	,182561A5	-01 × 000+000 E
93	-cetol-com	~-57266760 x 10 <sup>-5</sup>		6 a		12032279	.65072000 × 10-6	111	13	.049964010	~.56072960 x 10-3	78099500 x 10-
여누	.029995580	191A1A00	-'n502100 × 70_#	8 3			75066000 × 10-5		카	-029798750	- 202 1300	- 10797640 × 10
岣5	.016817740	.19036000 x 10-4	31560980	10 4	1	21500800	10590060 × 10 <sup>-1</sup>	llþa	႞키	.016851150	78080000 × 10−7	21069690
- 1	1	I	ı i	1245	.0268335880	50950000 × 30 <sup>-5</sup>	10000000		1 i		1	

### SANCE I.— COMPOSED VALUES OF $c_{n}$ , j $\frac{\partial u_{n}}{\partial t}$ , And $\frac{\partial u_{n}}{\partial m^{2}}$ FOR n=0 30 5 And DESSONS

#### VALUES OF P FOR VARIOUS VALUES OF L AND $\lambda$ - Continued

(b) L = 0.005 - Compluded

P	-	G <sub>n</sub> (P)	۲ <u>ورت</u>	ge <sup>2</sup>	,	G <sub>R</sub> (P)	1 <u>91</u> 90°	80 <sub>1</sub> ∂a <sup>2</sup>		G <sub>n</sub> (P)	1 <u>क्</u> र	8,12
_							λ = 5-5			<u> </u>		
٥	00	2.227789A0	-0.38610861 × 10 <sup>-2</sup>			0.000175/75	-0.37833333 × 10 <sup>-8</sup>	0 E801350 × 10-1	1 C	0.22595975	-0.58033101 × 10 <sup>-2</sup> 19876856	0.37669388 x 10 <sup>-1</sup> .95687130 x 10 <sup>-5</sup>
2	2	.13755161	19970157 90899870 × 10 <sup>-5</sup>	.91298880 x 10 <sup>-5</sup> -,75153300		0.29015575	19779613	.99194780 x 10 <sup>-5</sup>	M - I		91530730 × 10" <sup>3</sup>	
1	٦.	,080855695 ,0445555560	~,30959100	97949900	زار ا	.078409368	91720670 × 10-5		73		-,31211600	94516900
6	1	,0888114350	.12911000 x 10 <sup>-4</sup>	10667860 × 10 <sup>-1</sup>	l ăl	.043909500	32140600	,91£1B900	باو اا		.16620000 × 10 <sup>-5</sup>	
20	-	.010025000		94571100 × 10 <sup>-5</sup>	10	1 1 1	86470000 × 10 <sup>-5</sup>	10191750 x 10-4	ولنط			-,95145100 × 10-5
	1	<u>-</u>		, , , ,	19	.010517500	.13694200 x 10 <sup>-3</sup>	91686500 x 10 <sup>-5</sup>				
_					•		λ = 4.0	•		<del>4 </del>		
a	90	.25344570	-0.7727717 × 10 <sup>-2</sup>	0.31203986 × 10-4	П			1	10	0,94979855	-0.3703A900 × 10 <sup>-8</sup>	0.31356435 × 10 <sup>-4</sup>
•	1	.11250141	17875416	.453/48800 × 30 <sup>-5</sup>	2	0.24604256	-0.56700615 x 10 <sup>-8</sup>	0.31301894 × 10 <sup>-1</sup>	∥ 3 2	.14077659	17926667	.48544990 x 10 <sup>-5</sup>
, k	٤	.075955550	64269360 x 10 <sup>-3</sup>	66525900	• :	.13905624	17176728	.51495040 x 10*2	<b>∦</b> 5∣9	.075885440	6490.9560 × 1 <i>0</i> -3	65486700
5	3	.057115590	96586000 x 10 <sup>-lq</sup>	-,98066600	6 1	.0746 <del>4</del> 1170	-,65539550 × 10 <sup>-3</sup>		1 3		10628700	95 <del>84</del> 7600
8	4	.015359 <b>42</b> 0	.14547500 x 10 <sup>-5</sup>	-,98158400	8	1	11575800	936a4300	∥ የነኝ	I _	.13632800	908331100
10	5	.57991000 × 10 <sup>-2</sup>	.22457000	71921300	10		.12751500	89505500	14   2	*100000000 × 10 <sup>-22</sup>	.21720200	-,11370900
Ц	$\perp$			,	16	,46555000 × 10 <sup>-2</sup>	.21008800	70810600	L. L.			l
_	_						λ = 6.0			·	<del>,</del>	<del></del>
0		0.34331890	-0.3685\055 x 10 <sup>-2</sup>		H					0.34004120		0.16911360 x 10 <sup>-1</sup>
2		.13960442	86765270 × 10 <sup>-5</sup>	95954240 × 10 <sup>-5</sup>		0.53676576	-0.32493837 x 10-8	0.10999000 × 10-5	3 4	.13875495		34464560 × 10 <sup>-3</sup>
*	2	,045206720 ,58220000 x 10 <sup>-2</sup>	- 01 x 00019004. ኛ- 01 x 000445188.	74688500 57468800	6		87452600 x 10 <sup>-3</sup>	33003050 × 10 <sup>-5</sup> 72842800	2 5	.045844250 .61007000 x 10 <sup>-2</sup>	.35598000 × 10 <sup>-3</sup>	75767000 57382500
9	1	- 7495e000	,26451000	50169000	8	1	.27010900 × 10 <sup>-5</sup>		بَاوُ ا		.26149500	30300100
מג		95771000	.17570800	-;87210000 × 10 <sup>-6</sup>	10	1	.25845100	304£6500	وانتاا	1 '. '	.3.7484200	- 90540000 × 10-6
_	1	2/1	()/(******	1		,9997\$4000	.17590300	95440000 x 10 <sup>-6</sup>		'	1	
				· · · · · · · · · · · · · · · · · · ·			λ = 8.0	<del>/</del>	W		·	·
0	0 0	0.43649650	-0.29173167 × 10 <sup>-2</sup>	0.10 <del>71</del> 6298 × 10 <sup>-3</sup> 1					7 0	0.41358382	-0.29071465 x 10 <sup>-2</sup>	0.10597674 x 10 <sup>-1</sup>
2	a.	.112665550	27988630 x 10 <sup>-5</sup>	54547200 × 10-5	2	0.41066200	-0.25967236 × 10 <sup>-2</sup>		3 1	11240500	28558550 x 10 <sup>-5</sup>	,5359-070 x 10-5
١.	•	.99595900 x 30 <sup>-8</sup>	51976900	51363700	*		~,29060410 × 10 <sup>-3</sup>		E *  ~	1	.33363900	51151700
6		002f584to	,26626900	E1084300	6		, 20953700	50915400	7 7		.88617500	- 811/4/500
8		0073154700	3)4216800		8		.26105100	21260000	9 4		.1/41/7100	16400000 × 10 <sup>-7</sup>
10	[기	80190000 × 10−8	.52900000 x 10 <sup>-1</sup>	,89690000 × 10 <sup>-6</sup>	10		.18212900 .58550000 × 10 <sup>-3</sup>	58300000 x 10 <sup>-7</sup> -80650000 x 10 <sup>-6</sup>	h)	75050000 x 20 <sup>-2</sup>	.35740000 x 10 <sup>-4</sup>	.81960000 x 10-6
	щ			ļi	1.42	7-190000 X 1D -	λ = 12.0	1.000,000 % 2	<b>F</b>	<u> </u>		[
	٦.	o sotroro	-0.25640307 x 10 <sup>-2</sup>	a tenathan v and	7	Τ -	<u> </u>	r	1/0	0.52405809	-0.23592167 × 10 <sup>-8</sup>	0.48863680 x 10 <sup>-5</sup>
2	9	0,52719590 ,026 <b>8</b> 41700	.59220 <del>15</del> 0 x 10 <sup>-5</sup>		ا ا	0.58947553	-0. P75k378e x 10-2	0.48500.870 × 10-5			.36785850 × 10 <sup>-7</sup>	
ľ	١.	~.056457400	,338118900	15120300			.38235390 x 10-5		m - 1	096120900	.55680500	13199200
٦	١٦.	01 <b>079400</b> 0	.66590000 x 10 <sup>-1</sup>	.66284000 x 10-6	ß	1 .	-55548600	13277700	7 3		.63250000 × 10 <sup>-1</sup>	.65189000 × 10-6
ď		-,89510000 × 10-8	-, N-250000	.79950000	B		.63900000 x 20-4	.64112000 x 10-6			4353.0000	73490000
10	ш	.24950000	-, N5660000	.28960000	10	1	-,42740000	.75170000	ولد		N5590000	.00000000
_1	ľ	J#	-	1 <sup>-</sup>	امدا	27760000	45050000	.29220000	11 1	i	I	l '

## THE CRIPTIES VALUES OF $a_n$ , $a_n$ ,

#### VALUES OF P FOR VARIOUS VALUES OF L AND \(\lambda\) - Continued

### (c) L = 0.01

P n	G <sub>n</sub> (P)	7 <u>90°</u>	òo <sub>n</sub> òo²	Pn	G <sub>n</sub> (P)	3 <u>91</u> 90 <sup>2</sup>	98. 98 <sup>3</sup>	P	п	G <sub>n</sub> (P)	1 <u>91</u>	9 <u>4</u>
		-				λ = 0.02			_			
0 0 2 1	0.22589000 × 10 <sup>-2</sup> 0(10 <sup>-15</sup> )	-0.99774711 x 10 <sup>-2</sup> 0(10 <sup>-15</sup> )	0.028009704 0(10 <sup>-12</sup> )	\$ 0	0(10-15)	0(10-15)	o(10- <sub>75</sub> )	•	91	0.28686000 × 10 <sup>-6</sup> 0(10 <sup>-29</sup> )	-0.40666516 × 10 <sup>-5</sup> o(10 <sup>-2</sup> 7)	0.5441 <i>0</i> 437 × 10 <sup>-4</sup> 0(10 <sup>-25</sup> )
						λ = 0.06						
0 0 2 1 4 2 6 3	0.67343000 × 10 <sup>-2</sup> .52103410 × 10 <sup>-4</sup> .40130948 × 10 <sup>-8</sup> 0 (10 <sup>-14</sup> )	-0.99326574 × 10 <sup>-2</sup> 18265256 × 10 <sup>-3</sup> 24083166 × 10 <sup>-7</sup> 0(10 <sup>-15</sup> )	0.95058333 × 10 <sup>-2</sup> .51915537 × 10 <sup>-5</sup> .1395844e × 10 <sup>-6</sup> o(10 <sup>-12</sup> )	20. 11.	0.52567000 × 10 <sup>-1</sup> .40264100 × 10 <sup>-8</sup> 0(10-14)	-0.18369726 × 10 <sup>-5</sup> 2 <b>h</b> 163560 × 10 <sup>-7</sup> 0(10 <sup>-13</sup> )	0.58281888 × 10 <sup>-5</sup> .15980689 × 10 <sup>-6</sup> 0(10 <sup>-12</sup> )	<u> </u>   •	0	0.99117000 x 10 <sup>-3</sup> .85596000 x 10 <sup>-6</sup> 0(10-11)	-0.25760172 × 10 <sup>-2</sup> 40437722 × 10 <sup>-5</sup> 0(10 <sup>-10</sup> )	0.46717257 × 10 <sup>-2</sup> .180 <b>5</b> 0712 × 10 <sup>-4</sup> 0(10 <sup>-9</sup> )
		·				λ = 0.30						
0 0 2 1 4 2 6 3 8 4	0.011184600 .98818120 × 10 <sup>-3</sup> .19186800 × 10 <sup>-4</sup> .65745900 × 10 <sup>-7</sup> o(10 <sup>-10</sup> )	-0.98881539 × 10 <sup>-2</sup> 15431225 45809149 × 10 <sup>-4</sup> 21665655 × 10 <sup>-6</sup> 0(10-9)	0.55450145 × 10 <sup>-2</sup> .20288466 .10108128 × 10 <sup>-5</sup> .68096857 × 10 <sup>-6</sup> o(10 <sup>-9</sup> )	20 41 62 83	0.99945000 × 10 <sup>-3</sup> .19951800 × 10 <sup>-4</sup> .66124650 × 10 <sup>-7</sup> o(10 <sup>-1</sup> 0)	-0.15629988 × 10 <sup>-8</sup> 46154886 × 10 <sup>-4</sup> 21752600 × 10 <sup>-6</sup> 0(10 <sup>-9</sup> )	ام ا	3 5 7	0 1 2 5	0.39650100 x 10 <sup>-2</sup> .17007130 x 10 <sup>-5</sup> .1313274 x 10 <sup>-5</sup> .19463000 x 10 <sup>-8</sup> 0(10 <sup>-12</sup> )	-0.47575498 × 10 <sup>-5</sup> 55381554 × 10 <sup>-5</sup> 599858070 × 10 <sup>-6</sup> 78958070 × 10 <sup>-8</sup> 0(10 <sup>-11</sup> )	0.1;34635555 x 10 <sup>-2</sup> .58456862 x 10 <sup>-3</sup> .10689759 x 10 <sup>-1</sup> .26481881 x 10 <sup>-7</sup> 0(10 <sup>-11</sup> )
						λ = 0.20						
0 0 2 1 1 2 6 3 8 4	0.022175500 .7656330 × 10 <sup>-2</sup> .18957755 .52513650 × 10 <sup>-3</sup> .36460200 × 10 <sup>-3</sup> .26660500 × 10 <sup>-3</sup>	-0.97762647 × 10 <sup>-9</sup> 4569512147536031578680 × 10 <sup>-3</sup> 45575086 × 10 <sup>-3</sup> 77658352 × 10 <sup>-5</sup>	0.27251677 × 10 <sup>-2</sup> .20770222 .96167670 × 10 <sup>-3</sup> .2744120 .47614012 × 10 <sup>-4</sup> .90151366 × 10 <sup>-5</sup>	2 0 4 1 6 2 8 5 10 4 12 5	0.78751000 × 10 <sup>-8</sup> .19451780 .32521845 × 10 <sup>-3</sup> .37025900 × 10 <sup>-4</sup> .87021250 × 10 <sup>-2</sup> .12584050 × 10 <sup>-6</sup>	-0.4716#85 × 10 <sup>-2</sup> 1513807632211176 × 10 <sup>-3</sup> 44113978 × 10 <sup>-4</sup> 38189154 × 10 <sup>-5</sup> 20661097 × 10 <sup>-6</sup>		5 7 9 11	1 2 3	0.03746840 -0.0374684 × 10 <sup>-2</sup> -8517488 × 10 <sup>-3</sup> -11542820 × 10 <sup>-3</sup> -10495457 × 10 <sup>-4</sup> -61542600 × 10 <sup>-6</sup>	-0.70998678 × 10 <sup>-2</sup> 6765296072856914 × 10 <sup>-3</sup> 1249652213651500 × 10 <sup>-3</sup> 95638290 × 10 <sup>-6</sup>	.15027546
L,-	·	<u> </u>				λ = 0.40				<del></del> _		
00 21 42 65 84 105	0.043788200 .023405974 .013870233 .70251970 x 10 <sup>-2</sup> .32747170 .13953730	-0.996\176\ × 10 <sup>-8</sup> 64\1289405\9772295\16\51246\18559677060 × 10 <sup>-3</sup>	0.15148582 × 10 <sup>-2</sup> .11218849 .87841540 × 10 <sup>-3</sup> .62117155 .39868555 .22075852	20 41 62 83 104 125	0.027071890 ,0114681668 .75969595 × 10 <sup>-2</sup> .34267650 .11447069 .56136100 × 10 <sup>-5</sup>	-0.69660179 × 10 <sup>-2</sup> -,437/4904 -,24955430 -,13131592 -,62727130 × 10 <sup>-2</sup> -,2704085	0.12773774 × 10 <sup>-2</sup> .966 <u>31020</u> × 10 <sup>-5</sup> .66963677 .41827667	5	2 3 4	0.034673490 .015217059 .016241973 .45675380 × 10 <sup>-8</sup> .22164840 .85676300 × 10 <sup>-5</sup>	-0.82500894 × 10 <sup>-2</sup> 59498516582107771761142185685030 × 10 <sup>-3</sup> 40829510	0.17061079 × 10 <sup>-2</sup> .10769060 .78046072 × 10 <sup>-3</sup> .51862768 .30769457 .16825112

### THE I. - CONFUSED VALUES OF $\alpha_n$ , $J \frac{\partial \alpha_n}{\partial t}$ , and $\frac{\partial \alpha_n}{\partial a^2}$ for a=0 to 5 and inference

#### VALUES OF P FOR VARCOUS VALUES OF L AND \(\lambda = \text{Continued}\)

(a) L = 0.01 - Continued

P .	a <sub>n</sub> (P)	91 902	গুনি	P a	G <sub>n</sub> (P)	श्रीत:	রীয়	P	n	a <sub>n</sub> (P)	) <u>p</u> e 98 <sup>7</sup>	30, 20,
						λ = 0.60		•				
0 0 R 2		-0.93574070 x 10 <sup>-2</sup> 6564208348312464	0.84674192 × 10 <sup>-3</sup> .69366878 .56463498	20	0.047240440 .030610610	-0.76642540 × 10 <sup>-2</sup> 53962667	0.05791522 x 10 <sup>-5</sup> .66671009	3	0 1 2	0.055325510 .036344070 .035359305	-0.85085988 × 10 <sup>-2</sup> 60754619 42545721	0.846739964 × 10 <sup>-3</sup> .68567404 .54748965
6 3 8 4	01.7754050	35478587 89670833	,45066885 34898641	6 a 8 3	.01957907 .01957707	572.92806 24965485	.58153995 .59660076	1 9	3	.01\657760 .89119\+50 × 10 <sup>-2</sup>	19513710	.46668585 .56176504
10 ;	3 x 365070630 x 10 <sup>-8</sup>	1A871051.	,2601.77 <del>87</del>	10 ¥	.11.364800 x 1.0 <sup>-4</sup>	-,16646586 -,10809464 \(\lambda\) = 0.80	.29129531 .205557759	111	2	50995870	12402585	.25525091
<u> </u>		I				X = 0.50	<del></del> 1	m .	اما	A ACT   ACT	a Beladent zerő	a (2006027 140 <sup>3</sup>
2 3	1	-0.91576305 x 10 <sup>-10</sup> 66677900 48366845	0.61366060 x 10 <sup>-5</sup> ,46911908 ,36522700	20 41	0.0673,524,50 ,046606270	-0.79253140 × 10 <sup>-2</sup>	0.61505080 × 10 <sup>-3</sup>	)	1	0.075385890 .058068560 .055880279	-0.85418414 × 10 <sup>-2</sup> 61964854 44900595	0.61/06935 x 10** .4/963978 .36711594
6 3	.083673800	35294656 25519956	.68789506 .6681/s069	6 g 8 5	.0515 <b>75526</b> .021388330	-,41259176 -,2957760	.96449686 .96592609	7 9		.00A486490 .006951A95	38\1\355 858\9009	.2074905\ .2254963L
10 2	.01.00.000000	18506390	.18044305	10 ¥ 12 5	.014558454 .949646 <b>0</b> 0 × 10 <sup>-2</sup>	21020506 14793412	,21,976976 ,16950138	"	2	.011061710	-16)2177	71406250
						λ = 1.0						
6 : 8 : 6 : 8 :	053196967	-0.85675656 × 10 <sup>-8</sup> 6416170646183668354132402467574017688380	0,47454368 × 10 <sup>-3</sup> .55438011 .83999190 .17610985 .13818611 .10116975	80 41 68 85 104 185	0.085567#A0 ,060625580 ,042450A44 ,082690740 ,082727355 ,014485590	-0.50095979 x 10 <sup>-8</sup> 5756535541255777297757762255765015593970	0.47847880 x 10 <sup>-3</sup> .34374191 .20078406 .18517741 .14039564 .20785675	2 2 7	3	0.094816150 .066957410 .046700167 .094760880 .086950981 .016048180	-0.84861160 x 10 <sup>-8</sup> 6019736437148333516196642898783016656690	0.47789970 x 10 <sup>-5</sup> .94080825 .94660950 .18229738 .13780998 .10508050
	•					እ = 1.2						
0 2 1 6 8	1	-0.67779131 × 10 <sup>-Q</sup> 6099617348660500299616602190849015108610	0.3847(85) × 10 <sup>-3</sup> .847(7)328 .150(3804 .10808)67 .666(387)0 × 10 <sup>-4</sup> .44334800	8 0 4 1, 6 8 6 3 10 4 18 5	0.1094s135 .073660600 .051581270 .05195900 .065443613 .017814360	-0.80076404 × 10 <sup>-8</sup> 5596431859517089871761801973694014106890	0.38682750 × 10-5 .25661669 .17136855 .11365187 .75079660 × 10 <sup>-1</sup> .55670000	7 9	1 2 3	0.113646977 .075984990 .097597919 .099028470 .097456368 .018751710	-0.85558072 × 10 <sup>-62</sup> 585084ss410020115859287602050108011654770	0.38546557 × 10 <sup>-3</sup> .25194516 .16575587 .10546189 .75461840 × 10 <sup>-3</sup> .50275100
L,						λ = 1.4	,					
2: 4: 6: 8:	0 0.34086090 1096408790 20964084860 3049885890 405378890890 5088098890	-0.85975969 x 10 <sup>-2</sup> 5757040958606900859451801746515011852850	0.91703878 × 10 <sup>-5</sup> .1840865 .10239945 .55081600 × 10 <sup>-4</sup> .84038660 .77090000 × 10 <sup>-5</sup>	8 0 1 1 6 2 8 5 10 4 12 5	0.12570264 .085269940 .058917056 .040812740 .068349650	-0.79787748 × 10 <sup>-8</sup> 97776718364274702474724101687648011764690	0.760,7581.7 × 10 <sup>-5</sup> .19478665 .11758818 .66668840 × 10 <sup>-1</sup> .76417810 .18905000	3 3 7	1 8 5	0.131882/k8 .090744190 .06881/5182 .045319540 .050054750 .08091/k300	-0.62769630 x 10 <sup>-2</sup> 5570681555747690853774101721275011725890	0.51\$66594 × 10 <sup>-3</sup> .189\$6047 .109510¶5 .60006580 × 10 <sup>-3</sup> .50535940 .13945800

## TABLE I.- CONFUSED VALUES OF $a_n$ , $1\frac{\partial a_n}{\partial t}$ , and $\frac{\partial a_n}{\partial a_n}$ for n=0.205 and describe

#### VALUES OF P FOR VARIOUS VALUES OF L AND $\lambda$ - Continued

#### (a) L = 0.00. - Continued

<b>P</b>	G <sub>n</sub> (P)	1 30n	96 <sup>n</sup>	Pn	a <sub>n</sub> (P)	1 <u>96</u>	94 <sub>5</sub>	P	D	φ <sub>k</sub> (‡)	1 <u>90</u> a	98
						λ = 1.6				· 		
0 0 2 1 4 2 6 3 8 4 10 5	0.15772920 .10602960 .071510779 .048000000 .091820570	-0.84627683 × 10 <sup>-2</sup> 7407097174498100218707801372029089278400 × 10 <sup>-3</sup>	0.86835081 × 10 <sup>-3</sup> .13934666 .59599340 × 10 <sup>-4</sup> .2038261086997300 × 10 <sup>-5</sup> 14296800 × 10 <sup>-4</sup>	2 0 4 1 6 2 8 3 10 4 12 5	0.1k1k1736 .055k55660 .05k3k570k .0k3676720 .085600170 .080095kk0	-0.76815067 × 10 <sup>-2</sup> 5117670555107660215226101566795087152900 × 10 <sup>-5</sup>	0.27248870 × 10 <sup>-3</sup> .14927655 .75358660 × 10 <sup>-4</sup> .38243940 .75068600 × 10 <sup>-5</sup> 48374000		1 0 7 1 7 3 9 4 1 5	.045896540 .050970050	-0.81531482 × 10 <sup>-2</sup> 52649180 52831030 21615550 13721136 86448400 × 10 <sup>-3</sup>	0.87074895 × 10 <sup>-5</sup> .11471347 .69729020 × 10 <sup>-4</sup> .26477060 .26756900 × 10 <sup>-5</sup> ~.94267000
<u></u>						λ = 1.8						
0 0 2 1 4 2 6 3 8 4 10 5	0.17468210 .11450174 .074627510 .046984840 .051526536 .020584550	-0.82537790 × 10 <sup>-2</sup> 5059171050478030179507301060098055125700 × 10 <sup>-5</sup>	0.23090067 × 10 <sup>-3</sup> .30612132 .36066040 × 10 <sup>-3</sup> -312646900 × 10 <sup>-3</sup> 19503800 × 10 <sup>-3</sup> 26598500	2 0 4 1 6 2 6 5 10 4	0.15557567 .104-0150 .068611595 .045002950 .0294557700 .019254820	-0.77879771 × 10 <sup>-R</sup> 4877892829650570176541201049660059659400 × 10 <sup>-5</sup>	0.25455500 × 10 <sup>-5</sup> .11488099 .46516370 × 10 <sup>-4</sup> .87518400 × 10 <sup>-5</sup> 10380100 × 10 <sup>-4</sup> 18838900		10	.070,598869 .046752050 .030499480	-0.80217995 × 10 <sup>-2</sup> 495072013058592017517460105711000 × 10 <sup>-5</sup>	0.29897691 × 10 <sup>-5</sup> .11070697 .11578100 × 10 <sup>-1</sup> .96706000 × 10 <sup>-5</sup> .114748600 × 10 <sup>-1</sup>
<u>,                                     </u>						λ = 2.0						
0 0 2 1 4 2 6 5 8 4 10 5	0.1909050 .12137545 .076971916 .047502120 .08565000 .018128760	-0.80501570 × 10 <sup>-2</sup> 14712857082665771101450413070605700 × 10 <sup>-5</sup> 26886600	0.2011/9882 × 10 <sup>-3</sup> .8053/7500 × 10 <sup>-3</sup> .1619898015 <sup>3</sup> 5315902866970072015500	2 0 4 1 6 2 8 3 10 4 12 5	.077.269480 .04501598 .028198670	-0.76842513 × 10 <sup>-16</sup> 45497902262213001452825075616100 × 10-355110000	0.20\5\812 × 10 <sup>-3</sup> .88551990 × 10 <sup>-4</sup> .2505855070800000 × 10 <sup>-5</sup> 2152\800 × 10 <sup>-4</sup>		10 51 75 94 15	.046464400 .028943550	-0.9880758 x 10 <sup>-2</sup> 46568638864307701443706073888500 x 10 <sup>-3</sup> 32544000	0.2030301 x 10 <sup>-5</sup> .04360460 x 10 <sup>-4</sup> .207394001112069023098500
Г.					<u> </u>	እ = 2.5						
0 0 # 1 # 2 6 5 8 4 10 5	0.88565540 .13404855 .076417425 .042468030 .022155830 .010738500	-0.77054661 x 10 <sup>-2</sup> 59175261806453067799000 x 10 <sup>-5</sup> 10696500 .15309400	0.14864117 × 10 <sup>-2</sup> .59070560 × 10 <sup>-4</sup> 12555820 51542190 51548000	2 0 4 1 6 2 8 3 10 4	.072779670 .040746500 .040780120	-0.74095331 × 10 <sup>-2</sup> 959956791827400079598400 × 10 <sup>-3</sup> 1790600092951000 × 10 <sup>-3</sup>	0.15128071 × 10 <sup>-3</sup> .5505550 × 10 <sup>-5</sup> 64881500 × 10 <sup>-5</sup> 26481590 × 10 <sup>-5</sup> 5114560060750800		1031777	.0\3\69090 .022091160	-0.75%1096 x 10 <sup>-2</sup> 387798001819834070823400 x 10 <sup>-3</sup> 14055900 .18257000	0.1500A448 × 10 <sup>-5</sup> .41058580 × 10 <sup>-8</sup> 94715000 × 10 <sup>-5</sup> 88950A40 × 10 <sup>-8</sup> 50088400
$\bot$						λ = 3.0				,	, <del> </del>	
0028	0.26740060 .12075277 .070978759 .032075900 .032077990 .22750000 × 10 <sup>-2</sup>	-0.13455944 × 10 <sup>-2</sup> 319771171112455034304500 × 10 <sup>-3</sup> .23160700 .56028000	0.11160525 × 10 <sup>-5</sup> .13584880 × 10 <sup>-1</sup> 14805700577159405058250025058500	2 0 4 1 6 2 8 1 10 4	.0926706960 .092677600 .013562120	-0.71146202 × 10 <sup>-2</sup> 316610431197959029777000 × 10 <sup>-3</sup> .19271700 .51305100	0.11670815 × 10 <sup>-5</sup> .17979900 × 10 <sup>-1</sup> -20763170 -20763020 -20763020 -2076600		3 1 3 8 7 3 9 4	0.89811186 .13776180 .069878180 .038827800 .03718960 .37896000 x 10 <sup>-2</sup>	-0.7290527 × 10 <sup>-2</sup> 318900491196227017402700 × 10 <sup>-5</sup> 82172000 .53744700	0.11570265 × 10 <sup>-5</sup> .15614640 × 10 <sup>-5</sup> 22754020322525503545840022654700

## TABLE 1.— COMPOSED VALUES OF $a_{\rm D}$ , $a_{\rm D}$ $a_{\rm C}$ $a_{\rm C}$ for a=0.205 and dependent

### VALUES OF P FOR VARIOUS VALUES OF L AND $\lambda$ - Continued

(a) I = 0.01 = Concluded

Pþ	о <sub>л</sub> (Р)	<u> </u>	90 <sup>2</sup>	P	G <sub>n</sub> (P)	1 <u>90</u> 7	85	P	]	G <sub>n</sub> (P)	1 <u>90</u>	94 <sup>2</sup>
						λ = 3.5			_			
2 1 4 2 6 3 8 4	0.85650570 .14511443 .062064780 .022506600 .44473000 x 10 <sup>-2</sup>	-0.70149626 x 10 <sup>-2</sup> - 27594100 - 56372700 x 10 <sup>-3</sup> .21486900 .48909000	0.91047600 x 10 <sup>-3</sup> 11511000 x 10 <sup>-5</sup> 29014310 x 10 <sup>-3</sup> 505156002254540014259200	2 0 4 1 6 2 8 3 10 4	.022677100 .52604000 x 10 <sup>-2</sup>	-0.68311237 × 10 <sup>-2</sup> 2558331061901200 × 10 <sup>-3</sup> .15583500 .38404900 .38458000	0.92794250 × 10 <sup>-1</sup> , .22062400 × 10 <sup>-5</sup> .26275700 × 10 <sup>-1</sup> .28655100 .22190400 .114846700	))) 1	1 2 3 4	0.89153465 .13995469 .061486810 .088706700 .48646000 × 10 <sup>-2</sup> 23547000	-0.69294696 x 10 <sup>-2</sup> 259709059805100 x 10 <sup>-3</sup> .18496800 .40540800 .39488000	0.91929450 × 10" -54453000 × 10" -27640710 × 10" -29511000 -2252640014264400
						λ = 4.0						
2 1 4 2 6 5 8 4	0.38981250 .12081548 .051071170 .012131800 ~.26955000 × 10 <sup>-2</sup> ~.66952000	-0.67078714 × 10 <sup>-2</sup> 1996902018190600 × 10 <sup>-3</sup> .83602500 .88360100	0.7396850 × 10 <sup>-1</sup> 1017990 29146390 24955800 17533400 72459000 × 10 <sup>-5</sup>	6 2 8 3 30 4	1 7	-0.62587091 × 10 <sup>-2</sup> 2014648019836800 × 10 <sup>-3</sup> .58106900 .45820600	0.75574180 × 10 <sup>-1</sup> 75808300 × 10 <sup>-5</sup> 27514680 × 10 <sup>-1</sup> 24180100 13453000 75567000 × 10 <sup>-5</sup>	3 5 7 9	2 3 4	0.5825\130 .13821382 .050915000 .0125\9700 22157000 x 10 <sup>-2</sup> 65288000	-0.66333435 × 10 <sup>-8</sup> -,20064860 -,17099700 × 10 <sup>-5</sup> ,4054200 ,46807200 ,36075000	88712100 × 16 <sup>-7</sup>
						λ = 6.0						
2 1 4 2 6 5 8 4	0.43219790 .10974690 .79746000 × 10 <sup>-2</sup> ~.016120500 ~.018955500 ~.64980000 × 10 <sup>-2</sup>	-0.36760450 × 10 <sup>-2</sup> 3581600 × 10 <sup>-2</sup> .66525000 .51456700 .22187000 .35840000 × 10 <sup>-4</sup>	0.37831149 × 10 <sup>-1</sup> 21592601797820068776000 × 10 <sup>-5</sup> -77410000 × 10 <sup>-6</sup> -90490000 × 10 <sup>-5</sup>	8 0 4 1 6 9 8 5	0153.02900	-0.56038115 × 10-8 40041400 × 10-5 .62754300 .50284300 .22510000 .59130000 × 10-4	20600190 17703050 64672000 × 10 <sup>-5</sup> .48640000 × 10 <sup>-6</sup>	3 5 7 9	1 2 3 -	0.4a695615 .10317990 .4za86000 x 10 <sup>-2</sup> .015608900 .012712100 .64600000 x 10 <sup>-2</sup>	.64534000	0.37618974 × 10 <sup>-4</sup> 21.155901.784007065753000 × 10 <sup>-5</sup> -62870000 × 10 <sup>-5</sup> -29480000 × 10 <sup>-5</sup>
П			·		<del></del>	λ = 8.0			_			<del></del>
2 1	0.51089950 .045652400 ~.050075100 ~.060051700 ~.56540000 × 10 <sup>-2</sup> .84800000 × 10 <sup>-3</sup>	85200000 × 10 <sup>-2</sup> -0.7575000 × 10 <sup>-2</sup> -0.45750000 × 10 <sup>-2</sup>	0.21613694 × 10 <sup>-4</sup> 2042661072925000 × 10 <sup>-5</sup> .16135000 .30710000	2 0 4 1 6 2 8 3 10 4 12 5	019618800 57550000 × 10 <sup>-2</sup>	-0.48473527 × 10 <sup>-2</sup> .56057500 × 10 <sup>-5</sup> .69309100 .2090100057720000 × 10 <sup>-4</sup>	0.22039135 × 10 <sup>-1</sup> 19975820 79779000 × 10 <sup>-5</sup> .1 <sup>1</sup> 4192000 .29700000	3 5	2 - 3 - 4 -	.50501909 .044646800 .069571000 .019865400 .56960000 x 10 <sup>-2</sup> .76800000 x 10 <sup>-3</sup>		0-218a9076 × 10 <sup>-5</sup> 2020058075366000 × 10 <sup>-5</sup> 1515900030250000

# TABLE 1.— COMPOSED VALUES OF $G_{ns}$ , 4 $\frac{\partial G_{ns}}{\partial t}$ , AND $\frac{\partial G_{ns}}{\partial m^2}$ FOR n=0 10 5 AND INTEREST. VALUES OF P FOR VARIOUS VALUES OF L AND $\lambda$ — Continued.

(4) L = 0.05

P n	G <sub>n</sub> (P)	1 9t gr <sup>27</sup>	<u>3a²</u> 3a₁	P n	G <sub>p</sub> (P)	ì <u>94</u> 9a <sup>tr</sup>	<u>36,</u> 36 <sup>2</sup>	,		a <sub>n</sub> (P)	1 <u>98</u> 7	<u>8</u> 42_
						λ = 0.02						
51	0.50265000 × 10 <sup>-2</sup>	-0.049748683	0.31290\1\	20					1 0 5 1	o (10-17)	0(10-15)	o(xo-z+)
J	<u>.                                    </u>					λ = 0.06	·			<del>!</del>		
0 0 2 1 4 2	0.014960800 .45525200 × 10 <sup>-9</sup> 0(10- <sup>28</sup> )	-0.049251961 67354238 × 10 <sup>-8</sup> 0(10 <sup>-26</sup> )	0.10266792 .96677662 × 10 <sup>-7</sup> 0(10 <sup>-25</sup> )	20	0.45817000 × 10-9 0 (10-28)	-0.67810950 × 10 <sup>-8</sup> 0(10-26)	0.97 <del>3534</del> 90.×10 <sup>-7</sup> 0(10 <sup>-85</sup> )		1 0 3 1	0.49546200 × 10 <sup>-4</sup> 0(10 <sup>-17</sup> )	-0.41799690 × 10 <sup>-5</sup> 0(10 <sup>-15</sup> )	0.52*51921 × 10 <sup>-1</sup> 0(10 <sup>-1</sup> *)
						λ = 0.10		٠				
00 21 42	0.024739800 .13143250 × 10 <sup>-1</sup> 0(10 <sup>-11</sup> )	-0.048753008 76277119 × 10 <sup>-1</sup> 0(10 <sup>-10</sup> )	0.060640165 .41344459 x 10 <sup>-3</sup> 0(10 <sup>-9</sup> )	20 41 62	0(10 <sup>-11</sup> )	-0.77602210 × 10 <sup>-1</sup> 0(10 <sup>-10</sup> )	0.42213835 × 10 <sup>-3</sup> .12612455 × 10 <sup>-9</sup> 0(10 <sup>-20</sup> )	Н	1 0 3 1 5 2	0.15185000 × 10 <sup>-2</sup> .12747550 × 10-7 o(10 <sup>-16</sup> )	-0.56165595 × 10 <sup>-2</sup> 10514420 × 10 <sup>-6</sup> o(10 <sup>-15</sup> )	0.017791418 .80487849 × 10 <sup>-6</sup> 0 (10 <sup>-14</sup> )
_						λ = 0.20	•					
0 0 2 1 4 2 6 5 8 4	.25874000 × 10 <sup>-7</sup>	-0.047575594 52452536 × 20 <sup>-2</sup> 71812640 × 20 <sup>-1</sup> 96564050 × 20 <sup>-7</sup> 0 (20 <sup>-2</sup> 0)	0.029160477 .82194266 × 10 <sup>-2</sup> .19379040 × 10 <sup>-3</sup> .37303836 × 10 <sup>-6</sup> o(10 <sup>-10</sup> )	2 0 14 1. 6 2 8 3	0.30007500 × 10 <sup>-2</sup> .85655020 × 10 <sup>-4</sup> .8448540 × 10 <sup>-7</sup> 0 (10 <sup>-11</sup> )	-0.55482770 × 10 <sup>-2</sup> 74357020 × 10 <sup>-4</sup> 96780350 × 10 <sup>-7</sup> 0(10 <sup>-10</sup> )	0.87590071 × 10 <sup>-2</sup> .20109788 × 10 <sup>-5</sup> .38 <sup>2</sup> 79576 × 10 <sup>-6</sup> 0(10 <sup>-10</sup> )		10 31 52 75	0.03500050 .5555560 × 10 <sup>-3</sup> .10588520 × 10 <sup>-3</sup> .51560600 × 10 <sup>-9</sup> o(10 <sup>-14</sup> )	-0.020709759 83089560 × 10 <sup>-3</sup> 35928558 × 10 <sup>-3</sup> 14513620 × 10 <sup>-8</sup> o(10 <sup>-13</sup> )	0.022059054 .17658556 × 10 <sup>-8</sup> .11852066 × 10 <sup>-8</sup> .65512996 × 10 <sup>-8</sup> o(10 <sup>-12</sup> )
						አ = 0.40						
0 0 2 1 4 2 6 3 8 4 10 5	.48226890 × 10 <sup>-2</sup>	-0.045328545 017250255 45729350 × 10 <sup>-2</sup> 65652420 × 10 <sup>-3</sup> 57291540 × 10 <sup>-4</sup> 28070770 × 10 <sup>-5</sup>	.67972050 × 10 <sup>-5</sup> .76051130 × 10 <sup>-1</sup>	20 41 62 85 304	0.029126720 .53194970 × 10 <sup>-2</sup> .61585700 × 10 <sup>-3</sup> .42877400 × 10 <sup>-3</sup> .17347400 × 10 <sup>-7</sup> .39904300 × 10 <sup>-7</sup>	-0.080005335 -,48400606 × 10 <sup>-2</sup> -,72776860 × 10 <sup>-3</sup> -,61442680 × 10 <sup>-3</sup> -,29776440 × 10 <sup>-3</sup> -,79990500 × 10 <sup>-7</sup>			5 1 5 2 7 5 9 4	0.074868420 .012421268 .18409766 × 10 <sup>-2</sup> .16797900 × 10 <sup>-3</sup> .89691300 × 10 <sup>-5</sup> .27727800 × 10 <sup>-6</sup>	-0.031868226 97772690 × 10 <sup>-2</sup> 18930717 × 10 <sup>-2</sup> 216\1630 × 10 <sup>-3</sup> 1\087260 × 10 <sup>-4</sup> 31159800 × 10 <sup>-6</sup>	0.012990066 .62085268 × 10 <sup>-2</sup> .17038167 .8562930 × 10 <sup>-3</sup> .80831384 × 10 <sup>-4</sup> .91013680 × 10 <sup>-6</sup>

### THESE I.- COMPUSED VALUES OF $a_n$ , $\frac{1}{3}\frac{\partial G_n}{\partial x^2}$ , AND $\frac{\partial G_n}{\partial x^2}$ FOR n=0 30 5 AND INCOMP

#### VALUES OF P FOR VARIOUS VALUES OF L AND \(\lambda\) - Continued

### (d) L = 0.05 - Continued

Pn	G <sub>n</sub> (P)	7 <u>95</u>	90°	P	G <sub>n</sub> (₽)	1 ga <sup>u</sup>	2 de 1	P	n G <sub>R</sub> (P)	1 <u>9</u> 4	925 90 <sup>7</sup>
						እ = 0.60					
8 1 4 R 6 3	0.13505490 ,053239040 ,018548625 ,55057100 x 10 <sup>-2</sup>	020711169 88282780 x 10 <sup>-2</sup> 51754990	0.83306890 × 10 <sup>-6</sup> .54501592 .31764638 .15037754	4 1 6 ₽		-0.096640596 010961094 37(706130 × 15 <sup>-2</sup>	0.76177401 × 10 <sup>-2</sup> ,41609509 ,185106 <b>82</b>	3 5 7	9 .001807439 5 .89997100 × 10 <sup>-8</sup>	-0.034806865 015454888 59618040 x 10 <sup>-8</sup> 19109530	.20559050
105	.13708040 .26763900 × 10 <sup>-3</sup>	£25660760 £2660760	.15722750 .15722750	8 5 10 4 12 5	.15589130 .50014800 × 10 <sup>-5</sup> .46971300 × 10 <sup>-1</sup>	10740506 24499610 × 10 <sup>-5</sup> 43977200 × 10 <sup>-4</sup> \(\lambda = 0.80\)	.65558440 x 10 <sup>-3</sup> .10050780 .38116500 x 10 <sup>-1</sup>	17 9	1 ' ' '	10104630 × 10 <sup>-5</sup>	.98998580 × 10 <sup>-5</sup> .80517950 × 10 <sup>-5</sup>
	0.17369490	-0.041515255	A 500 000 11 2008			1	1	П.,			
6 3 8 4 10 5	.077054060 .07805450 .03320450 .49904500 x 10 <sup>-8</sup>	-0.0450580 00450585 46918130 × 10 <sup>-8</sup> 80555790 79845100 × 10 <sup>-5</sup>	.64654890 x 10 <sup>-5</sup>	80 4 1 6 8 5 10 4 5 10 5	0.10289424 .042764990 .018813799 .61460300 x 10 <sup>-2</sup> .20337000 .61613000 x 10 <sup>-3</sup>	-0.029466555 015810525 61581720 × 10 <sup>-2</sup> 25908010 56659600 × 10 <sup>-3</sup> 35682500	0.76176918 × 10 <sup>-2</sup> .76068666 .17578148 .87778190 × 10 <sup>-5</sup> .39911450 .15967030	] 3	,32605800	-0.037599985 -0.07128443 -80458540 × 10 <sup>-2</sup> 57605170 14471630 58568100 × 10 <sup>-5</sup>	0.596am249 x 10-2 .557a6960 .1957ge0e .10560e00 .543617a0 x 10 <sup>-5</sup> .2x595560
Н				I		λ = 1.0		1	<u> </u>	<u> </u>	
0 0 2 1 4 2 6 5 8 4 10 5	0.20562580 .095619560 .045613310 .019726220 .87246700 × 20 <sup>-2</sup> .57502000	-0.09951864a 00866595 98674940 × 10 <sup>-6</sup> 46158690 22661760 -,11019100	0.49318598 × 10 <sup>-2</sup> .19949177 .10450680 .6189990 × 10 <sup>-5</sup> .97501500 .28260000	20 41 62 83 104 125	0.13943997 .062180290 .027397370 .011784980 .49117800 × 10 <sup>-2</sup> .139597100	-0.030619514 014953975 69700690 × 10 <sup>-2</sup> 55116570 15340160 68153800 × 10 <sup>-3</sup>	0.44698201 × 10 <sup>-2</sup> ,82360254 ,1130.6975 -69540600 × 10 <sup>-5</sup> ,35739600 ,18686000	1 5 7 9 11	.0154e7200	-0.077107338 016765867 81578870 × 10 <sup>-2</sup> 39735740 19054140 881168900 × 10 <sup>-3</sup>	0.44743075 × 10 <sup>-2</sup> ,21770672 ,11524348 ,66119600 × 10 <sup>-3</sup> ,3005100 ,21222200
L					•	እ = 1.2					
0 0 2 1 4 2 6 3 8 4 10 5	0.84508100 .10908406 .049675670 .088907730 .000842570 .49488000 x 10 <sup>-2</sup>	-0.057645951 -0.06784544 -76586710 × 10 <sup>-2</sup> -36454600 -,18035600 -,91602000 × 10 <sup>-3</sup>	0.3364am06 × 10 <sup>-8</sup> .11516072 .359634000 × 10 <sup>-3</sup> .13586600 .80361000 × 10 <sup>-1</sup> .56628000	20 41 62 53 104 125	0.17468623 .078605880 .075757550 .0160651140 .78804800 × 10 <sup>-2</sup> .38718000	-0.070852079 014086649 67794230 × 10 <sup>-2</sup> 51288490 15474400 78676000 × 10 <sup>-5</sup>	0.35544875 × 10 <sup>-2</sup> .14795070 .55407070 × 10 <sup>-5</sup> .5608300 .17679500 .10504600	1 5 7 9 11	2 .01221-9010	-0.054311754 015467459 71753740 × 10 <sup>-8</sup> 34357650 1696500 84284000 × 10 <sup>-5</sup>	0.34907168 × 10 <sup>-2</sup> .13507577 .57578870 × 10 <sup>-3</sup> .25953600 .14187100 .86365000 × 10 <sup>-1</sup>
<b>_</b>	<del></del>					λ = 1.4					
0 0 2 1 4 2 6 3 8 4 10 5	0.27482450 .11798062 .051445980 .022670500 .010556400 .47958000 × 10 <sup>-2</sup>	-0.056607777 01444/44 57970860 x 10 <sup>-2</sup> 83797700 165959000 x 10 <sup>-3</sup>	0.9693/070 × 10 <sup>-6</sup> .59959060 × 10 <sup>-3</sup> 10017000 × 10 <sup>-6</sup> 13031000 × 10 <sup>-5</sup> 11262900 71254000 × 10 <sup>-3</sup>	20 41 62 83 104 125	0.20739077 .090474580 .040031640 .017973470 .81826000 × 10 <sup>-8</sup> .37759000	-0.090708810 012899985 95928790 x 10-2 96596600 11185900 55128000 x 10 <sup>-5</sup>	0.98569682 × 10 <sup>-6</sup> .98542810 × 10 <sup>-3</sup> .8857500 × 10 <sup>-5</sup> .7750000 × 10 <sup>-5</sup> -,10900000 × 10 <sup>-6</sup>	3	0 0.2995645 110380761 2. obj668060 3. osobsk900 4. 98979000 × 10 <sup>-2</sup> 525019000	-0.03335784 015750096 57886960 × 10 <sup>-6</sup> 84549100 10971100 71654000 × 10 <sup>-5</sup>	0.28001646 x 10-8 .78686590 x 10-3 .13199000 25166000 x 10-4 45836000 51378000

THERE I.- CORPUTED VALUES OF  $G_{n}$ ,  $J = \frac{iG_{n}}{\partial \xi}$ , And  $\frac{iG_{n}}{\partial \xi^{2}}$  For n = 0 to 5 And Definition

VALUES OF F FOR VARIOUS VALUES OF L And h — Continued.

(4) L = 0.05 ~ Continued

Pn	G <sub>n</sub> (P)	ا <u>م</u> م	e l'a	P	а <sub>л</sub> (Р)	۶ <u>چو</u> د	90.j	2	_ 0 <sub>α</sub> (₽)	1 <u>95</u>	30 <sub>0</sub>
						λ = 1,6					
0	0.30542770	-0.054888515	0.22009678 × 10 <sup>-2</sup>					1	0.46971648-	-0.098578189	0.229N28E4 x 30 <sup>-6</sup>
2 2	,19270 <b>0</b> 54	010001110	.29094950 x 10 <sup>-5</sup>	20	0.85889692	-0.0502533405	0.85737717 × 10 <sup>-2</sup>	3	11069091	011886484	.59023040 × 10 <sup>-5</sup>
1 2	,0 <del>19777569</del> 0	79952970 x 10 <sup>-2</sup>	2469A900	1 1/2	.0989809ap	~.011429125	.58417180 × 10 <sup>-5</sup>	3	2 .045640620	41778490 × 10 <sup>-2</sup>	11940600
6 3	-020274100	11704400	-,27698200	6 2	.041494700	~.425755No x 10 <sup>-8</sup>	74910000 × 10 <sup>-5</sup>	7	.018997100	13860600	19159700
0 4	.85765000 × 30 <sup>-Q</sup>	~.24445000 × 10 <sup>-3</sup>	20445700	8 3	.03.7520000	1 <del>536700</del> 0	11528200 x 10-3	9	-80197000 x 10 <sup>-6</sup>	Jan B2000 × 30-3	15129700
1005	סטננועלי		~,1506 <b>54:00</b>	10+	•175315000 € 10-6	5463000 x 10-5	10541000	Ьυ.	,34977000	-41106500Q	98741000 x 10 <sup>-1</sup>
			l	128 5	.53085000	-19459000	699*3000 × 10**	1	i i	1	·
		<u> </u>			<u> </u>	λ = L.8	<del></del>		<del></del>	L. <del></del>	<del></del> -
٥٥	o. <del>13068</del> 40	-0.053465779	0.1 <b>0</b> 510618 × 10 <sup>-8</sup>	Π				<b>F</b> 1	0.00814813	-0.051592728	0.1911990\ × 10 <sup>-4</sup>
2 1	.12401592	010074326	18139000 × 10 <sup>-3</sup>	elo	0.26174194	-0.089653.097	0,19681320 x 10-9	<b>i</b> ,i	1 .31395555	02.0005757	.11715260 × 10°
1 2	.04559 <b>561</b> 0	~,2 <del>7/7</del> 0700 x 10 <sup>-8</sup>	~.97427900 × 10 <sup>-3</sup>	4 2	.10400888	9645£730 × 10-6	1		2 .042870650	26962000 x 10 <sup>-2</sup>	l.
6 3	.016044700	,19017000 x 10 <sup>-3</sup>	59000900	69	.0400931290	29239800	17980500	7	.025768700	42067000 × 10 <sup>-3</sup>	-, g696650o
8	.5571.0000 x 10 <sup>-9</sup>	.56916000	-,29955800	6 5	.005995000	66079000 x 10 <sup>-5</sup>	21056700	i 9	1	.16209000	-,189 <u>41800</u>
10 5	.16407000	.95765000	137756000	10 4	.77083000 × 1.0 <sup>-2</sup>	~96400000 × 10-5	15474600	11/2	.195\3000	.25050000	11778000
				12 5	. £1119000	.18965000 × 10 <sup>-5</sup>	98290000 x 10		L	<b>.</b>	]
						λ = 2.0					
00	0.55621190	-0.05e189hoh	0.15HH495 x 10 <sup>-8</sup>	П				1	0 0.32480681	-0.0506090E4	0.16156945 × 10*
21	,1205k895	80994990 × 10 <sup>-6</sup>	<u>.</u>	a o	0.89501k11	-0.0289676Nk	0,16669349 x 10-4	3	1 .11417516	82255190 × 10 <sup>-6</sup>	~,751£5000`× 10-
4 2	.05619551-0	~.99501000 × 10 <sup>-5</sup>	~431 <b>32</b> 100	41	.10790748	82491690 × 10-8	.507 <b>66</b> 100 × 10 <sup>-1</sup>	<b>.</b>	.091999690	-,13894000	<del>5556</del> 5100 × 100
6 3	.010970100	.66813000	~,33139900	6 8	.059449580	-,1 <b>7018700</b>	27970700 x 10-7	7	5 .0111-59600	.95765000 × 10 <sup>-3</sup>	-, a09Na200
84.	.00776000 × 20 <sup>-2</sup>	.7 <del>7706</del> 000	-,20 <b>\106</b> 00	a s	.003679500	.89190000 x 10 <sup>-1</sup>		γİ	.2756e000 x 10-R	.58e <del>01</del> 000	18406200
10 5	29440000 × 10 <sup>-3</sup>	.5 <del>775</del> 0000	11 <b>A42</b> 000	10 4	.52513000 × 10 <sup>-8</sup>	,40949000 x 10 <sup>-3</sup>	-,16 <del>177</del> 600	и	.20960000 × 10 <sup>-5</sup>	.447 <b>73000</b> 00	107(4000
	i '		11 11 1	15 5	.507€0000 × 20°3°.	. 34690000	~996+1000 × 30-4		<u> </u>		· ·
						λ = 2.5					
٥٥	0.41359980	-0.029558082	0.10565519 x 10 <sup>-2</sup>					4	0.58456459	-0.028250527	0.110 <del>7717</del> 1 × 10 <sup>-4</sup>
2 1	.10009960	58767730 x 30 <sup>-2</sup>	4053,5630 x 10 <sup>-5</sup>	20	0.3968/Neo	-01 <b>08712</b> 3459	0.11460000 × 10-4	13	1 .109999560	42431240 × 10 <sup>-9</sup>	32996050 x 10 <sup>-3</sup>
4 2	-01.9 <del>76</del> 2900	.11215000	43,5621,00	4 2	.0997977000	-,45377840 × 10 <sup>-9</sup>	25980010 × 10 <sup>-3</sup>	1	009205050. 2	.10250500	580£1700
6 3	18430000 x 10 <sup>-8</sup>	.16900900	2251,000	6 2	,02164,0900	.663.080.00 × 10 <sup>-3</sup>	54400500	7	30530000 x 10~3	.1/4258700	~*************************************
84	46604000	.10505600	~.95820000 x 10 <sup>-3</sup>	83	·100,580000 × 10-4	.12130000 × 10-2		9	436760000 × 10 €	.95392000 × 10 <sup>-5</sup>	~-97T70000 × 10~
10 5	54360000	.98480000 x 10 <sup>-3</sup>	-,29 <b>7000</b> 00	ᄱ	27900000	.89603000 × 10 <sup>-7</sup>	977 <b>9000</b> 0 x 10	11	99e\0000	49500000	5A20000
┙	<u></u>		l	45	-24440000	.¥5750000	37720000	Ш		<u> </u>	L
_					,	λ - 5.0	<del>,</del>				
olo	Q.46m1130	-0.026879A35	0.75865850 x 10 <sup>-5</sup>	Н			!	149	0.43791720	-0.086108701	0.19456750 x 10~
8 1	.085608000	60042000 x 10 <sup>-5</sup>	M68ee770	20	p.41021755	-0.025251.681	0.88657760 x 10-7	1	002161200	- 10449270 x 10 <sup>-9</sup>	ſ
4 2	-,605#0000 x 10 <sup>-3</sup>	.26040 <b>90</b> 0 × 10 <sup>-9</sup> 2	31616000	4 1		1446/190 × 10-5	~374 <u>0</u> 1690	1	2 .16445000 × 10 <sup>-2</sup>	.229A0800	30565800
6 3	010866100	J6333600	<u>16704500</u>	62		.199 <b>726</b> 000	28958000	1	3 98665000	.1541100	20 <del>0223</del> 111, م
84	72570000 x 10 <sup>-2</sup>	.68120000 × 10 <sup>-3</sup>	<del></del>	83	-,77786000	.3A517600	-31378900	9	4 695k0000	.66970000 x 10-7	i
70 2	~3 <b>/360</b> 000 .	.1 <i>5</i> 450000	*E0860000 × 70_m	1.7	78930000	ľ	21.750000 × 30 <sup>-1</sup>	P	5 5220-00000	.20580000	,1k900000
LL	Ļ		L	122 5	30010000	.g1.660000	.96700000 × 10 <sup>-5</sup>		<u> </u>	<u> </u>	<u> </u>

### TABLE I. - COMPUTED VALUES OF $G_{n}$ , $J = \frac{\partial G_{n}}{\partial q}$ , AND $\frac{\partial G_{n}}{\partial x^{2}}$ FOR n=0 TO 5 AND INTRODUCE

#### 'VALUES OF P FOR VARIOUS VALUES OF L AND $\lambda$ - Continued

(d) L = 0.05 - Concluded

Pb	O <sub>n</sub> (P)	j da <u>n</u>	gan gan	Pn	a <sub>n</sub> (P)	1 <u>90 <sup>n</sup></u>	92. 90. <sup>3</sup>	P	n	a <sub>n</sub> (P)	<u>ئو</u> د <u>مو</u> ق	<u>∂u,</u> ∂a²
						λ = 3.5						
00	0.50482550	-0.024758725	0.56430130 x 10 <sup>-3</sup>			,		1	0 0.4	18055555	-0.024180701	0.59156440 × 10 <sup>-2</sup>
2 1	.052956000	.18946320 × 10 <sup>-8</sup>	46805110	₽ 0	0.45647255	-0.025576752	0.6160 <b>7</b> 680 x 10 <sup>-5</sup>	3	u .	054621600	.14420490 × 10 <sup>-2</sup>	- 43707660
1 2	017506700	,29377000	2081.2000	41	.055850500	.10204980 x 10 <sup>-2</sup>	-,40602830	5	20	114672200	.27300400	20708400
6 3	~ <b>.01467890</b> 0	.11878100	19133000 × 10 <sup>-lq</sup>	6 2	012045400	.25240500	20470600	7	5	11,5500500	.11649000	26786000 x 10 <sup>1</sup>
8	61340000 × 10 <sup>-2</sup>	.21050000 x 10 <sup>-5</sup>	.55780000	8 3	0123k9200	.11547800	35504000 × 10 <sup>-1</sup>	9	4 5	9010000 x 10 <sup>-2</sup>	.9\190000 × 10 <sup>−3</sup>	27740000
رد ما	15950000	.94500000 x 10 <sup>-3</sup>	.30720000	10	56+50000 x 10 <sup>-2</sup>	.26740000 × 10-5	.22070000	ונו	5 1	15270000	~.63700000 × 10 <sup>-1</sup>	.28010000
Ш				12 5	16890000	55800000 × 10 <sup>-1</sup>	.25540000					
						λ = 4.0	4					<b></b>
00	0.54175570	-0.022912316	0.43154200 × 10 <sup>-5</sup>				[	1	00.5	1906060	-0.022470426	0.45220510 × 10 <sup>-3</sup>
g 1	.018818500	.37735000 x 10 <sup>-2</sup>	44012700	20	0.49681.948	-0,022006590	0.47161820 x 10-3	l 3	1 .0	P2574800	.55¥35700 × 10 <sup>−2</sup>	k1968260
ų s	029432200	.27382800	11527700	4 1	.02551.2500	.295\2670 x 10 <sup>-8</sup>	39890590	5	20	26752600	.26207300	11956600
- 1 1	03950000	59850000 × 10 <sup>-5</sup>	.51750000 x 10 <sup>-1</sup>	6 2	02\190700	.24995600	12285600	-		1.5559000	.6090000 × 10 <sup>-3</sup>	.2461.0000 × 10-1
- 1 1	50920000 × 10 <sup>-2</sup>	14 <b>73000</b> 0	.4 <u>e69000</u> 0	1 .	012705000	.64250000 x 10 <sup>-5</sup>	.17950000 × 10 <sup>-1</sup>			22110000 × 10-2	10570000	39540000
10 5				ء امدا	52750000 × 10 <sup>-2</sup>	66500000 × 10 <sup>-ly</sup>	-36070000	и	5			
	ĺ			12 5					1			
-1-1	<del></del>	·······	<del></del>	خلتا	——————————————————————————————————————	λ = 6.0	<u> </u>	ш		<del></del>		
٦٦	0.65045480	-0.017477262	0.17/\$4210 × 10 <sup>-3</sup>	П		<u> </u>		T,	مام	5306756	-0.017295431	0.18616880 x 10 <sup>-3</sup>
- 1 1	-,12385890	.74956600 × 10 <sup>-2</sup>	.,	ا ا	0.61586676	-0.017105023	0.19459510 × 10 <sup>-3</sup>		ı	1649960	.72116900 x 10 <sup>-2</sup>	
- 1 1	-,026715000	.12461000 × 10-5	.74915000 × 10 <sup>-1</sup>		10942850	.69517100 × 10 <sup>-0</sup>	27790610			26554000	196-9000 x 10 <sup>-5</sup>	,69097000 x 1.0 <sup>-1</sup>
6 5	.66650000 × 10-2	720k0000	.40600000	1 I	026526000	.26966000 × 10 <sup>-5</sup>	.65457000 × 10 <sup>-1</sup>			9570000 × 10 <sup>-2</sup>	- 68040000	.40120000
8		-,		813		64160000	.59570000	Ġ	il i			
ر ا	<u></u>			10 6		-10410000	177710000		3			
71				122 5				-	1			
Щ.							L				<u> </u>	Ļ <del></del>

## THERE I.- COMPUTED VALUES OF $G_n$ , $3\frac{\partial G_n}{\partial s}$ , AND $\frac{\partial G_n}{\partial s^2}$ FOR n=0 TO 5 AND DEFENDER

### VALUES OF P FOR VARIOUS VALUES OF L AND $\lambda$ = Contained

(e) L = 0.1

P n	G <sub>n</sub> (P)	2 <u>91</u> 90 <sup>2</sup>	9 <del>4</del> 5	P n	a <sub>n</sub> (P)	1 <u>24</u> 90 <sup>2</sup>	95. 96 <sup>7</sup>	P		G <sub>n</sub> (P)	1 gd <sup>r</sup>	90 <sup>2</sup> 5 90 <sup>34</sup>
					·-	λ = 0.02						[
21	0.70968000 × 10 <sup>-2</sup>	-0.099290518	0.88215301	20					0	o(10-21)	o(10-53)	0(10-27)
┝┸╴	L			لبلب	<u> </u>	λ ~ 0.06	·	ш_	<u>.                                    </u>	L <u>-</u> -	ł <del></del>	
00	0.021054700 0(10-15)	-0.097894552 0(10 <sup>-14</sup> )	0.28756456 0(10-12)	20 41	o(10 <sup>-15</sup> )	a (10-14)	o(10 <sub>-75</sub> )	ш	0	0.12564700 × 10 <sup>-5</sup> 0 (10 <sup>-30</sup> )	-0.19270524 × 10 <sup>-14</sup> 0(10-29)	0.28471514 × 10 <sup>-3</sup> 0(10 <sup>-27</sup> )
Γ.	<del></del>					λ = 0.10			_			
0 0 2 1 4 2		-0.096329409 75338930 × 10 <sup>-6</sup> 0(10 <sup>-1.9</sup> )	0.16875947 .78710965 × 10 <sup>-5</sup> 0(10 <sup>-18</sup> )	2 0 4 1	0.70516600 × 10 <sup>-7</sup> 0(10 <sup>-20</sup> )	-0.76736864 × 10 <sup>-6</sup> o(10 <sup>-19</sup> )	0.80251722 × 10 <sup>-5</sup> o(10 <sup>-18</sup> )			0.78869800 × 10 <sup>-7</sup> 0(10 <sup>-12</sup> )	0(10-71) -0.84938245 × 10-5	0.01 <del>2595399</del> 0(10 <sup>-10</sup> )
						λ = 0.20	·					
0 0 2 1 4 2 6 3	.15022740 x 10 <sup>-6</sup>	-0.095245220 25090265 × 10 <sup>-2</sup> 70644990 × 10 <sup>-6</sup> 0(10 <sup>-11</sup> )	0.075881688 .55999759 × 10 <sup>-2</sup> .56806285 × 10 <sup>-5</sup> o(10 <sup>-10</sup> )	20 41 62	0.76655400 × 10 <sup>-3</sup> .13495370 × 10 <sup>-6</sup> 0(10 <sup>-12</sup> )	-0.24980686 × 10 <sup>-2</sup> 73296610 × 10 <sup>-6</sup> 0(10 <sup>-11</sup> )	0.70766832 × 10 <sup>-2</sup> .38245700 × 10 <sup>-5</sup> o(10 <sup>-20</sup> )		1 0 5 1 7 3	.31844700 × 10 <sup>-9</sup>	-0.025215550 14261200 × 10 <sup>-14</sup> 21054736 × 10 <sup>-8</sup> 0(10 <sup>-15</sup> )	0.045227054 .25875874 × 10 <sup>-3</sup> .13525554 × 10 <sup>-7</sup> 0(10 <sup>-14</sup> )
						λ = 0.40				-		
0 0 2 1 4 2 6 3 8 4	.27157500 × 10 <sup>-1</sup> .20671500 × 10 <sup>-6</sup>	-0.087186659 020089475 18523037 × 10 <sup>-2</sup> 57585150 × 10 <sup>-3</sup> 57531400 × 10 <sup>-6</sup> 16251200 × 10 <sup>-8</sup>	0.035884458 .017033541 .25781936 × 10 <sup>-2</sup> .11545883 × 10 <sup>-3</sup> .14327048 × 10 <sup>-8</sup> .51851410 × 10 <sup>-8</sup>	20 41 62 85 104	0.022960600 .15891260 × 10 <sup>-2</sup> .2969430 × 10 <sup>-4</sup> .2220000 × 10 <sup>-6</sup> .52977000 × 10 <sup>-9</sup> o(10 <sup>-12</sup> )	-0.024159181 21039280 × 10 <sup>-8</sup> 63019350 × 10 <sup>-8</sup> 59838300 × 10 <sup>-6</sup> 0(10 <sup>-11</sup> )	0.0621/58405 .25757769 × 10 <sup>-2</sup> .12548459 × 10 <sup>-3</sup> .35480546 × 10 <sup>-3</sup> .75185760 × 10 <sup>-8</sup> 0(10 <sup>-13</sup> )		3 1 3 2 7 3	.12105800 x 10 <sup>-5</sup>	-0.051722226674391410 × 10 <sup>-2</sup> 59689070 × 10 <sup>-5</sup> 6825656 × 10 <sup>-5</sup> 76131600 × 10 <sup>-7</sup> 0 (10 <sup>-10</sup> )	0.0589/6831 .8406050 × 10-2 .67058040 × 10-3 .15572987 × 10-4 .10430800 × 10-6 .20071240 × 10-9

### Then I.- confused values of $c_n$ , $1\frac{2c_n}{6t}$ , and $\frac{2c_n}{6n^2}$ for n=0 30.5 are estimated

#### VALUES OF . P -POR VARIOUS WATERS OF $\ L$ AND $\ \lambda$ = Continued

#### (a) L = 0,1 - Continued

PR	O <sub>n</sub> (P)	۱ <u>وت</u> چې	90	P a	a <sub>n</sub> (r)	1 <u>25</u>	90 80	ŀ	n	a <sub>n</sub> (₽)	1 <u>क्र</u> म	82
						λ = 0.60						
0 0 0 R 1 L B B 6 3 L B B 4 L D 5	0.18669190 .049690480 .94609480 × 10 <sup>-8</sup> .18041480 .11368400 × 10 <sup>-5</sup> .63047000 × 10 <sup>-5</sup>	-0.051754813 085313695 74113690 × 10 <sup>-8</sup> 18967490 149685000 × 10 <sup>-3</sup> 94685000 × 10 <sup>-3</sup>	0.02151920 .0122306 .0712 0 CT.12170 × 10 <sup>-2</sup> .1200501 .1600501 × 10 <sup>-3</sup> .13426200 × 10 <sup>-4</sup>	8 0 6 2 6 3 10 4 19: 5		-0.039344267 -93658610 × 10 <sup>-2</sup> -13796340 -16697590 × 10 <sup>-3</sup> -10717190 × 10 <sup>-4</sup> -11969800 × 10 <sup>-6</sup>	0.018789108 .64028980 × 10-8 .14368471 .19444890 × 10-5 .15426880 × 10-4 ,41319890 × 10-6	3	5 E	.40408700 x 30 <sup>-8</sup> .43861400 x 10 <sup>-3</sup>	-0.059785453 01750556 36658570 × 10 <sup>-2</sup> 89915600 × 10 <sup>-5</sup> 821598100 × 10 <sup>-5</sup>	0.082,75771 .95908470 × 10 <sup>-2</sup> .85387575 .911,88880 × 10 <sup>-5</sup> .542,74880 × 10 <sup>-5</sup> .535,41250 × 10 <sup>-5</sup>
L.,						λ = 0,80			_	•		
00 21 42 63 84	0.85366450 .075304790 .083207670 .98706800 × 10 <sup>-2</sup> .3053700 .17608000 × 10 <sup>-5</sup>	-0.07681,7330 068673403 000130638 31230970 × 10 <sup>-3</sup> 15269300	0.00460036 .68561990 × 10 <sup>-2</sup> .54875460 .19585990 .47644000 × 10 <sup>-5</sup> .116611900	2 0 4 1 6 2 8 3 10 4	0.1057076 .08570340 .70649000 × 10 <sup>-8</sup> .3377800 .8067700 × 10 <sup>-5</sup> .27468000 × 10 <sup>-8</sup>	-0.04075455 0581545 4536110 × 10 <sup>-2</sup> 1000500 19071100 × 10 <sup>-3</sup> 87617700 × 10 <sup>-4</sup>	0.00k597783 .99688200 × 10 <sup>-2</sup> .88065090 .69949090 × 10 <sup>-3</sup> .19134990 .86041800 × 10 <sup>-4</sup>	1	1 2 2 3 4	.01.9505760 .95075500 x 10 <sup>-Q</sup>	-0.05275120 -0.0167475 -0.0257410 -0.0257410 -0.000000 -0.0000000 -0.00000000000	0.03875025 .6975860 x 30 <sup>-2</sup> .89597040 .10407500 .88581250 x 30 <sup>-5</sup> .57954200 x 30 <sup>-5</sup>
						λ = 1.0					•	
00 21 42 63 84 205	0,2764230 .001200750 .089969950 .94877700 × 10 <sup>-8</sup> .27985000 × 10 <sup>-3</sup>	-0.072357648 -082252578 -092486400 × 10 <sup>-2</sup> -09260100 -138422000 × 10 <sup>-2</sup>	0.010607476 .75676960 x 20 <sup>-8</sup> .16090060 .69317100 x 10 <sup>-5</sup> .40788900 .16906000	8 0 4 1 6 2 8 5 10 4	.01/416760 ,40374800 x 10 <sup>-8</sup> .10177300	-0.050092557 017547757 55084550 × 10 <sup>-2</sup> 155927000 × 10 <sup>-5</sup> 14654500	0.011134186 .42906470 x 10 <sup>-2</sup> .17646160 .72119600 x 10 <sup>-3</sup> .86143300 .81337000 x 10 <sup>-4</sup>	3 3	5 1 5 2 7 3 9 4		-0.06339331k -0.02548770 77696900 × 10 <sup>-8</sup> 87173000 87173000 × 10 <sup>-5</sup> 84769000	.1255000
						λ = 1.2						
0 0 2 1 4 8 6 3 8 4 10 5	0.31698090 .10189999 .039788680 .011458800 .38868000 × 10 <sup>-2</sup>	-0.068311968 081334890 78468000 × 10 <sup>-8</sup> 89664300 10906200 41066000 × 10 <sup>-5</sup>	0.80565050 x 10 <sup>-2</sup> .11-510750 .86405700 x 10 <sup>-5</sup> .11000500 .98560000 x 10 <sup>-1</sup> .66560000	2 0 4 1 6 3 10 4 12 7	.0004/59150 .65†85600 x 10 <sup>-2</sup> .82556000	-0.053228459 -036957577 -3575500 × 10 <sup>-3</sup> -38965800 -3445000 × 10 <sup>-3</sup> -36099000	.¥07796800	3	5 2 7 3 9 4	.0 <b>007</b> 63540	-0.07999/7668 0194333191 67533500 × 10 <sup>-8</sup> 94647600 94686000 × 10 <sup>-5</sup> 33607000	0.85170410 × 10 <sup>-2</sup> .82230620 .71,746700 × 10 <sup>-5</sup> .51284600 .16603600 × 10 <sup>-4</sup>
<u> </u>		<del>,</del>	<del></del>			) = 1.4			_			· · · · · · · · · · · · · · · · · · ·
00 21 42 65 84	0.7557000 ,1058604 ,058605830 ,010636300 ,56863000 × 10 <sup>-2</sup> ,12586000	-0.054627979 016515480 4495200 × 10 <sup>-8</sup> 12743400 43132000 × 10 <sup>-3</sup> 17380000	0.68609470 × 10 <sup>-2</sup> .19408000 × 10 <sup>-3</sup> 54850700 56917000 36908000 58850000 × 10 <sup>-4</sup>	# 0 # 1 6 # 8 3 10 #	0.25760575 .07250500 .023421300 .16712000 × 10 <sup>-2</sup> .25650000 × 10 <sup>-3</sup>	-0.031171077 015081725 66798500 × 10 <sup>-8</sup> 13608400 77999000 × 10 <sup>-7</sup> 21664000	.5\109000 x 10-1		5 <u>1</u> 5 <u>2</u> 7 5		-0.00071995 016293990 47964700 × 10 <sup>-8</sup> 19167900 94015000 × 10 <sup>-9</sup> 21220000	0.67744680 × 10-2 .9000900 × 10-3 95959000 × 10-3 15300000 × 10-3 25300000 × 10-3

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THERE I. - Consumes tollies of  $\sigma_n$  , j  $\frac{\partial \sigma_n}{\partial z}$  , and  $\frac{\partial \sigma_n}{\partial z}$  for n=0 to 5 and insides

#### VALUES OF P FOR VARIOUS VALUES OF L AND $\lambda$ - Continued

#### (e) L = 0.1 = Continued

•	G <sub>n</sub> (P)	7 gr <sup>i</sup>	9 80	Р	о <sub>в</sub> (Р)	1 94 92"	89	P	θ <sub>p</sub> (P)	1 <u>91</u> 50 <sup>2</sup>	30 <u>.</u>
						λ = 1.6					· · · · · ·
이이	0.39753490	-0.06126906	0.50043240 x 30 <sup>-2</sup>	П					0.32867929	-0.076017484	0.54406650 x 30
2 1	.10456520	012465120	61122500 x 10 <sup>-5</sup>	20	0.27542917	-0-050142555	0.56795420 x 10 <sup>-2</sup>	∥ <b>Я</b> ⊒	.091701500	01.2763530	73990000 × 10-
4 2	.0281/1250	17996500 x 10 <sup>-2</sup>	948688 <b>0</b> 0	4 2	.0790021000	012535989	,48e87100 x 10-5	5 2	-025929410	256583400 × 10 <sup>-2</sup>	~.58762200 × 10°
6 3	-P± 000640TP.	.90280000 × 10 <sup>-4</sup>	57095000	6 2	.025126500	29928600 x 20 <sup>-2</sup>	28067IDQ :	7 3	-15/129000 × 10-8	~ 56749000 x 10 <sup>-3</sup>	38896000
6 4	.82124000	-85490000 × 10 <sup>-3</sup>	27909000	B 3	.69899000 × 10 <sup>-2</sup>	69525000 x 10 <sup>-3</sup>	- 23205000	94	<b>.23158000</b>	]	1924600o
05	.71790000 x 10 <sup>-5</sup>	-12970000	-*172T96000	10 4	*8580E000	16420000	31841000	ᄤᇰ	-77720000 x 10 <sup>-5</sup>		82560000 x 10-
Щ				12/2	-75970000 × 10 <sup>-5</sup>	1/7200000 × 10 <sup>-1</sup>	50430000 × 10 <sup>-4</sup>	Ш	<u>.</u>		
						λ = 1.8					
Q O	0.41814260	-0.05838 <del>575</del> 9	0.40958866 x 10 <sup>-2</sup>	П	] <del></del>			10	0.36206679	-0.053906954	0.44449800 x 10
2 1	.098365200	84567600 × 10 <sup>-2</sup>	13088990	원	0. 71042601.	~0.0 <del>19537588</del> 4	0.46769657 x 10 <sup>-2</sup>	ᆝᅯ	,069 <del>11</del> 3000	95041300 x 10 <sup>-9</sup>	~.60229800 x 10
4 8	021070600	.\1502000 x 10 <sup>-5</sup>	10945926	4 1	.07991,3800	96852600 × 10 <sup>-9</sup>	16770 <b>6</b> 00 × 10 <sup>-3</sup>	5 2	.090983500	54499000 x 10 <sup>-5</sup>	828113700 x 10
6 5	.36638000 × 10 <sup>-2</sup>	.13276700 × 10 <sup>-12</sup>	59564000 x 10 <sup>-3</sup>	6 8	-0E0061 <del>2</del> 000	1.2 <del>h   755</del> 00	581AA400	7 3	.45151000 x 10 <sup>-2</sup>	.59113000	47650000
8 4	.2 <del>7780000</del> × 10−3	•69990000 × 10-ე	27546000	8 3	.48907000 x 10 <sup>-2</sup>	71228000 × 70-2	36178000	94	.85900000 x 10 <sup>-3</sup>	.43950000	29634000
이키	12400000	-54590000	-, <u>,11801000</u>	10 4	-11744000	.85 <b>8</b> 50000	17521000	111 5	-3A8000000	.23180000	97640000 x 10T
Ш		L		12 2	.70700000 × 10 <sup>-5</sup>	-12870000	76760000 × 10 <sup>-1</sup>	Ш	<u> </u>		·
						λ = 2.0					
ఠ이	0.44659580		0.55645587 × 10 <sup>-2</sup>		-			140	0.39277888	-0.051.8 <b>8008</b> 4	0.56830330 × 10 <sup>-</sup>
2 1	.088гүт/880.	48613100 x 10 <sup>-2</sup>			0.5128592	-0.048022414	0.38981289 x 10 <sup>-2</sup>	31	.089984700	60449800 x 10 <sup>-2</sup>	- 98230000 × 10"
4 2	.012720900	.21150100	- 10855900	4 1	-076812100	683586600 x 10 <sup>-12</sup>	61127100 x 20 <sup>-5</sup>	] <b>3</b>  2	.01k32k600	.13225600	903.00000
6 3	57680000 x 1073	~71221 <b>€</b> 000	51268000 x 10 <sup>-3</sup>	6	-015098200	.51282000 × 10-3	71974500	T >	-95680000 x 10−3	.12754000	45206000
하누	-12620000 × 10-6	-89950000 x 10 <sup>-3</sup>	20799000	8 3	*80005000 × 70-5	.85780000	58370000	9 +		, <del></del> -	19203000
이키	r————	Ji180000.	i	10		.51890000	16927000	ᄤᄼ	<del></del>		<del></del>
Ш			L	12/5		.85920000		Щ	<u> </u>		<u> </u>
٠,						λ = 2.5					
이이	0.50761900		0.22126896 × 10 <sup>-2</sup>	1 1		)		140	0.45952945	-0.046920151	0.84159588 x 10 <sup>-1</sup>
역시	.077813700	-25%59400 x 10 <sup>-2</sup>	_	20	0.43383888	-0.0H14156T2	0.258355+2 × 10 <sup>-2</sup>	1 7-1	.0775797000	-84333000 × 10-5	13859840
누입	83702000 x 10 <sup>−2</sup>	-46940000°	75560000 x 10 <sup>-5</sup>	4 1	.0777811200	42704000 x 10 <sup>-3</sup>		커e	-,44509000 × 10 <sup>-12</sup>	-35497400 x 10 <sup>-2</sup>	12105000 × 10-
위기	65712000	.189\6000	18922000	6 2		.28565600 x 10 <sup>-2</sup>	1 1	J ¶3]	65680000	.16957000	~,8069 <b>8</b> 000
역制	577720000	-611120000 × 10−3		B 3	49720000	.aA859000	\$1M06000	94	31560000	.59760000 x 1.0 <sup>-3</sup>	05200000 x 20 <sup>-1</sup>
이기	11660000			10 4	25750000	.76720000 x 10 <sup>-3</sup>		쁘기	<del></del>		
Ш				12/2		<u></u>	<u> </u>	Ш			
						እ = 3.0					
이이	0.55797850	-0.044202170	0.15268650 × 10 <sup>-2</sup>	11		\	1	10	0.53456405	-0.0\te600.995	0.16705815 × 10
위기	-97599000 × 3.0™	•135000000 × 20−6	35553940	40	0.47983503	-0.040867834	0.17945857 × 10 <sup>-2</sup>	3 1	.016596900	.99067500 x 10 <sup>-2</sup>	1A150090
시티	025856000	A9A15000	31 × 000(56) c3	4 1	.021621500	.35649600 x 10-2	12706170	5 E	03706100	39323000	59679000 × 10°3
43	9 <b>51/&gt;00</b> 000 x 30 <del>-1</del> 2	.9753.0000 x 10 <sup>-3</sup>		6 2	015949900	, <del>35300010</del> 0	\0255000 × 10 <sup>-3</sup>	7 3	86470000 x 10 <sup>-6</sup>	.10070000	.16990000 × 10 <sup>-1</sup>
	82620000		i	8 3	78740000 x 30 <sup>-9</sup>	.30095000	31900000 × 30-4	9 4	221,70000		
리시											
하				ו   מנ	#11/k0000	7¥y00000 × 10−3	-57100000	ոլջ			

## THE LT. COMPOSED VALUES OF $a_n$ , $a \frac{\partial a_n}{\partial a_n}$ , and $\frac{\partial a_n^2}{\partial a_n^2}$ for n=0.20.5 and integer

#### VALUES OF P FOR VARIOUS VALUES OF L AND A .. Continued

(e) L = 0.1 ~ Concluded

P n	<sub>ከ</sub> (ዮ)	1 90 U	ुम्बू श्रुव	P	a a <sub>n</sub> (P)	ე <u>ეგი</u>	98 188	P	1	a <sub>n</sub> (P)	1 9c <sup>p</sup>	85 A
						λ = 3.5				· · · · · · · · · · · · · · · · · · ·		
2 1		.01.080.1640	0.10957348 × 10-2 13841330 78760000 × 10-4 .15866000 × 10-5	6	J	-0.097508261 .8£115000 × 10-2 .90075000 .19010000 × 10-3	14139000 × 10 <sup>-3</sup>		3 1 3 2 7 3 9 4	0.56048459 027878500 027687100 61640000 x 10 <sup>-2</sup>	-0.03857450. .94711100 × 10 <sup>-2</sup> .51379000 .74800000 × 10 <sup>-1</sup>	0.12013560 × 10 <sup>-5</sup> 13023500 11061000 × 10 <sup>-5</sup> .12755000
2 1		-0.076473223 .015077650 .1604000 × 10 <sup>-2</sup>	0.81298790 × 10 <sup>-3</sup> 11988400 × 10 <sup>-2</sup> 13878000 × 10 <sup>-3</sup> .16150000	] 4 :	·	J	0.95324570 × 10-5 10997510 × 10-2 .60280000 × 10-3 .13400000 × 10-3		5 2 5 2	0:559821486 075858600 087544000 81700000 × 10 <sup>-5</sup>	-0.0956005T0 .011903000 .17213000 × 10-2 65660000 × 10-5	0.89130580 × 10 <sup>-3</sup> 11505420 × 10 <sup>-4</sup> .97250000 × 10 <sup>-3</sup> .14790000 × 10 <sup>-3</sup>
						λ = 6.0					·	
		-0.026601767 .016019450 -145871000 x 10 <sup>-2</sup>	0.30536340 × 10 <sup>-3</sup> 63307300 .38920000	, ,		-0.086001559 04将4330 38580000 × 10 <sup>-2</sup>	0.36413690 × 10 <sup>-3</sup> 68931200 .34975000	:	5 A 7 5 4	0.70667777 24446100 .031360000	-0.026963399 -0.02584640 42130000 × 30 <sup>-22</sup>	0.35554000 x 10 <sup>-5</sup> ~.65324000 .36628000

#### VALUES OF P FOR VARIOUS VALUES OF L AND $\lambda$ - Continued

(f) L = 0.2

Pn	G <sub>II</sub> (P)	9 <u>9¢</u>	<u>3a₁</u> 3æ²	Pn	G <sub>n</sub> (₽)	1 gt	90 <sub>2</sub>	P	G <sub>n</sub> (P)	1 36 n	900 g
				L- J-L		λ = 0.02		<del></del> -			
007	0.00003400	-0.19799733	2.48377770	원 0 부 1				31			
			<u></u>			λ = 0.06		IJ. <b>.</b> .L			
21	0.0897721.00 0(10 <sup>-27</sup> )	-0.19408558 0(10 <sup>-25</sup> )	o.80222707 o(10 <sup>-24</sup> )	2 0 4 1	0(10-27)	o(10-25)	o(10 <sup>24</sup> )	31	0.91536000 × 10-9	-0.27055542 × 10 <sup>-7</sup>	0-17613572 × 10 <sup>-6</sup>
•		<del></del>	,	4 — i — i		λ = 0.10					!
0021	0.0489281.00 0(10 <sup>-11</sup> )	-0.19089438 0(10 <sup>-10</sup> )	0.46656763 .10101161 × 10 <sup>-8</sup> o(10 <sup>-35</sup> )	20	0(11-17)	o(10-10)	0.20500503 × 10-8 0(10-33)	1 0 5 1 5 2	0.26703400 × 10 <sup>-1</sup>	-0.30171974 × 10 <sup>-5</sup>	0.53585902 × 10 <sup>-4</sup> 0(10 <sup>-19</sup> )
						λ = 0.20		. i_		1	:
00 21 42	0.093435100 .48879100 × 10 <sup>-4</sup> 0(10-11)	-0.18131378 28247604 x 10 <sup>-3</sup> 	0.21607057 .13227274 × 10-2 .47169882 × 10-9	20 41 62	0.72171300 × 10-3. 0(10-11)	-0.30264614 × 10-3 0(10-10)	0.16957439 × 10 <sup>-2</sup> .59052641 × 10-9 (10 <sup>-80</sup> )	1 0 3 2 5 2	0.55627900 × 10 <sup>-2</sup> .48550500 × 10 <sup>-7</sup> o(10-16)	-0.002596700 39094313 × 10-6 0(10-15)	0.067969610 .30397637 × 10-2 o(10-14)
				-		λ = 0.40					
0 0 2 1 4 2 6 3 8 4	0.17569490 .92062300 × 10 <sup>-2</sup> .77761600 × 10 <sup>-2</sup> .74267000 × 10 <sup>-7</sup> o(10 <sup>-11</sup> )	0.16326108 016446141 22177050 x 10 <sup>-5</sup> 29770570 x 10 <sup>-6</sup> 0(10 <sup>-10</sup> )	0.09510A430 .084649980 .58669290 × 10 <sup>-5</sup> .11449697 × 10 <sup>-5</sup> .18480150 × 10 <sup>-9</sup>	20 41 62 83	0.012804690 .80757000 × 10 <sup>-3</sup> .817700 × 10 <sup>-7</sup> o(10 <sup>-11</sup> )	-0.020528322 25487430 × 10 <sup>-5</sup> 32829660 × 10 <sup>-6</sup> 0(10 <sup>-10</sup> )		1 ( 5 1 5 2 7 3	·10059300 × 10-8	-0.074893096 27482920 × 10-2 11972990 × 10-3 46271500 × 10-3 0(10-12)	0.077331.548 -5781.8882 × 10 <sup>-2</sup> -57652059 × 10 <sup>-4</sup> -80697543 × 10 <sup>-7</sup> 0(10 <sup>-1,2</sup> )

### THE E I.- CONFUSED VALUES OF $a_{\rm pt}$ , $1\frac{\partial a_{\rm pt}}{\partial t}$ , and $\frac{\partial a_{\rm pt}}{\partial m^2}$ for n=0 to 7 and defining

#### VALUES OF P FOR VARIOUS VALUES OF L AND $\lambda$ - Constitued

(f) L = 0.R - Continued

P a	Gm(P)	1 gar	94 <sub>6</sub> 92 <sup>8</sup>	P	G <sub>R</sub> (P)	े <u>श्र</u>	9m <sub>6</sub> 90 <sup>m</sup>	,	ŀ	O <sub>p</sub> (P)	) <u>20</u> 90°	A S
						λ = 0.60						
0 0 0 2 1 4 2 6 5 8 4	0.94308100 .95439300 × 10 <sup>-8</sup> .80938000 × 10 <sup>-4</sup> .9937000 × 10 <sup>-8</sup>	-0,1513550 -,05073470 -,34717070 × 10 <sup>-2</sup> -,15007300 × 10 <sup>-3</sup> -,2593500 × 10 <sup>-7</sup> -,12947200 × 10 <sup>-7</sup>	0.05584763 .088584763 .10059400 × 10-2 .55696000 × 10-3 .55695000 × 10-7	2 0 4 1 6 2 3 3 10 4		-0.046699886 -,46590060 × 10 <sup>-2</sup> -,18666170 × 10 <sup>-3</sup> -,27675900 × 10 <sup>-3</sup> -,14775800 × 10 <sup>-3</sup> 0(10 <sup>-10</sup> )	0.058721259 .57860860 × 10 <sup>-2</sup> .52800960 × 10 <sup>-3</sup> .6235670 × 10 <sup>-3</sup> .0(10 <sup>-10</sup> )	1 2 7 9	1 2 3 4	0.115/1827 .015/405/0 .569/6800 × 10 <sup>-5</sup> .11109100 × 10 <sup>-1</sup> .81782000 × 10 <sup>-9</sup>	-0.095 <b>TISOB</b> 4 -,019940123 -,98418800 × 10 <sup>-3</sup> -,82434500 × 10 <sup>-4</sup> -,82434500 × 10 <sup>-6</sup> -,67698000 × 10 <sup>-9</sup>	0.074052196 .012486711 .13586419 × 10 <sup>-4</sup> .46918300 × 10 <sup>-4</sup> .94397100 × 10 <sup>-4</sup> .80885600 × 10 <sup>-4</sup>
			·······	-	· · · · · ·	λ ≈ 0,80	· · · · · ·		-			
6 3 8 4 10 5	0.30542770 .058466670 .90563700 × 10 <sup>-8</sup> .96496000 × 10 <sup>-5</sup> .64614000 × 10 <sup>-5</sup> .25860000 × 10 <sup>-5</sup>	-0.13951446 -,034578360 -,72372400 x 10 <sup>-0</sup> -,10800510 -,86570000 x 10 <sup>-3</sup>	0.035m54m .012811299 .44445260 × 10 <sup>-2</sup> .98061700 × 10 <sup>-3</sup> .1059600 .64414000 × 10 <sup>-3</sup>	2 0 4 1 6 2 3 5 10 4 12 5	0.05818520 .0.37480.0 .13510160 × 10 <sup>-2</sup> .8981800 × 10 <sup>-3</sup> .3946200 × 10 <sup>-5</sup> .78610000 × 10 <sup>-7</sup>	-0.0660957564 011794188 14644250 × 10 <sup>-2</sup> 11674000 × 10 <sup>-3</sup> 57490000 × 10 <sup>-3</sup> 17975000 × 10 <sup>-6</sup>	0,038958009 ,88908040 × 20-8 ,14898410 ,14690850 × 10-5 ,85477000 × 10-5 ,86007000 × 10-6	1 7 9 11	1 2 3 4 5	0,18253486 ,020304260 ,37634600 × 10-8 ,30367300 × 10-5 ,15686000 × 10-6 ,47510000 × 10-6	-0,1000,661 -,081,980,510 -,577,80,300 × 10 <sup>-2</sup> -,5760,0000 × 10 <sup>-3</sup> -,2940,5900 × 10 <sup>-4</sup> -,585,800000 × 10 <sup>-6</sup>	0.037955965 ,021818766 _26557520 × 10 <sup>-4</sup> _2685600 × 10 <sup>-4</sup> _18151700 × 10 <sup>-4</sup>
						λ = 1.0				·		
0 0 0 2 1 4 2 6 3 8 4 10 5	0,7561190 .073109170 .015042740 .86771900 × 10-4 .75627000 × 10-5 .41010000 × 10-4	-0,18675782 -,089838590 -,12741760 -,21486000 × 10 <sup>-2</sup>	0.084711127 -53543980 × 10-2 -21565900 -86009000 × 10-3 -21525000 -37348000 × 10-4	2 0 4 1 6 2 3 3 10 4 12 5	.56533000 × 10 <sup>-5</sup>	-0.077036074 01606000 × 10-8 50841000 × 10-8 50841000 × 10-5 78060000 × 10-5 λ = 1.2	0.086908111. ,68886630 × 10 <sup>-2</sup> .18081.660 .37590300 × 10 <sup>-3</sup> .55703000 × 10 <sup>-5</sup>	1 7 9	N	0.48049595 .041976980 .86686400 × 10 <sup>-2</sup> .131933400 .15641000 × 10 <sup>-5</sup> .14890000 × 10 <sup>-5</sup>	-0,1082/607 -,08553.61/60 -,56686700 × 10 <sup>-26</sup> -,10071100 -,18646000 × 10 <sup>-3</sup> -01 × 00076761	0.027545792 .78436090 × 10 <sup>-6</sup> .83004000 .63271300 × 10 <sup>-5</sup> .12144800 .16658000 × 10 <sup>-5</sup>
ada	0.40265100	-0.11947581	0.018157947	Т		l		1	اما	0.29274654	-0.099880174	0.0906\1097
2 1 4 2 6 3 8 4 10 5	.015991400 .017085790 .77505000 × 10 <sup>-2</sup> .76650000 × 10 <sup>-3</sup>	022310940 51555500 × 10-8 34653500 57460000 × 10-5 65500000 × 10-4	.54859000 × 10⁻5	2 0 4 1 6 2 8 3 10 4 12 5	.78084800 x 10-8 .12790400 .87578000 x 10-7	-0.0769707180 0169971800 97109000 × 10 <sup>-2</sup> 01507000 × 10 <sup>-3</sup> 160990000 × 10 <sup>-1</sup>	0.0mm804950 .4m546910 × 10-8 .11456020 .34004000 × 10-5 .88870000 × 10-4 .18540000	3 7 9 11	1 9 3 4	.036448580 .018068470 .24175000 × 10-8 .44510000 × 10-5 .69800000 × 10-4	080546600 47999900 × 10-8 11841100 86901000 × 10 <sup>-3</sup> 50640000 × 10 <sup>-3</sup>	.31216640 × 10 <sup>-2</sup> .82765000 × 10 <sup>-5</sup> .32459000 .11345000 .29900000 × 10 <sup>-1</sup>
				<del></del>	<del></del>	A = 1.4			-1		<del></del>	
0 0 0 9 1 4 2 6 3 8 4 10 5	0.443661.0 .014175800 .51975000 × 10-2 .66750000 × 10-3 .14670000	-,01/1940200 -,18184000 × 10 <sup>-2</sup>	0.013/9119h 269/2650 × 10 <sup>-8</sup> 15982700 47259000 × 10 <sup>-5</sup> 11569000 × 10 <sup>-1</sup>	2 0 4 1 6 8 6 5 10 4 12 5	.94953000 x 10 <sup>-9</sup> .19486000 .40750000 x 10 <sup>-5</sup>	-0.079995770 014254050 01695600 x 10-8 60697000 x 10-5 16040000 40100000 x 10 <sup>-1</sup>	0.016949472 .17150100 × 10 <sup>-2</sup> .17590000 × 10 <sup>-3</sup> .54760000 × 10 <sup>-3</sup> .58410000 .13890000	1 7 7 9	2 3	0.35969668 .06535200 .01276600 .86479000 × 10-8 .56760000 × 10-5	-0.096380578 015251300 87685100 × 10 <sup>-2</sup> 64970000 × 10 <sup>-3</sup> 138500000 × 10 <sup>-3</sup>	0.00,5078597 .1369300 × 10 <sup>-3</sup> 17293000 13239000 × 10 <sup>-3</sup> .19200000 × 10 <sup>-3</sup>

# TABLE I.- CONTINUO WALRIS OF $G_k$ , $3\frac{\partial G_k}{\partial x}$ , And $\frac{\partial G_k}{\partial x^2}$ For n=0 to 5 AND interest. Values of P for Various Galles of L and $\lambda$ - Continued

(f) L = 0.2 - Continued

Pn	O <sub>p</sub> (P)	<u>يم</u> ر	\$		Ф <sub>2</sub> (P)	3 gd <sup>2</sup>	97. 87	ŀ	٦	0 <sub>0</sub> (P)	1 <u>96</u>	¥ <b>1</b> 22
						1 = 1.6				•		
63 63 63 105	0.48010700 .057107700 .98050000 × 10 <sup>-2</sup> .13808000 .15100000 × 10 <sup>-5</sup>	-0.1097941 66138200 × 10 <sup>-2</sup> .12989600 .79900000 × 10 <sup>-3</sup> .18160000	0.010 pt 5e7k 58501850 x 10 <sup>-2</sup> 28705000 71578600 x 10 <sup>-3</sup> 58580000	2 0 4 1 6 2 8 3 10 4	0.85596867 .04544400 .87455000 × 10 <sup>-2</sup> .16659000 .36480000 × 10 <sup>-3</sup>	-0.079340934 010452750 12735000 × 10 <sup>-2</sup> 18130000 × 10 <sup>-3</sup> 29500000 × 10 <sup>-4</sup>		3 3 1 9	3	0.98181865 .099710400 .96348000 × 10 <sup>-2</sup> .17843000 .12700000 × 30 <sup>-3</sup>	-0.083301876 95377600 × 10 <sup>-2</sup> 55494000 × 10 <sup>-3</sup> .15760000 41500000 × 20 <sup>-4</sup>	0.012468579 18296270 x 10* 12595290 44043000 x 10*
						λ = 3.B	· · · · · ·					
0 0 2 1 4 8 6 5 8 4	0.51961770 .052905700 .80175000 × 10 <sup>-2</sup> .10759000 × 10 <sup>-5</sup>	.1753000 x 10 <sup>-3</sup> .36374000 x 10 <sup>-2</sup> .13566000		4 1 6 2 8 3 10 4	.6127000 × 10 <sup>-2</sup>	-0.077755134 55004500 x 10 <sup>-2</sup> -59975000 x 10-5 -59995000 -15810000	0.010809967 16630950 × 10 <sup>-8</sup> 105620000 × 10 <sup>-5</sup> 10750000	) ) 1	2 3	0.k1967510 .051017600 . J6950000 × 10 <sup>-2</sup> .9660000 × 10 <sup>-3</sup>	-0.083174174 -36747900 × 10 <sup>-2</sup> -15118000 .57650000 × 10 <sup>-3</sup> -18660000	0.99706630 × 10° 30975330 15986600 51660000 × 10° 19460000
			لـــــــا	12/2	<u> </u>	λ = 2.0		Ц.	L		L	
2 1 4 2	0.54175710 .054282500 54425000 × 10 <sup>-2</sup> 56070000	.60294600 × 10 <sup>-6</sup> .50665000 .16896000	0.6911\(\begin{align*}750 \times 10^-2\)505149000180579001\(\begin{align*}240000 \times 10^-5\)12060000	2 0 4 1 6 2 8 3 10 4 10 5	.182300000 × 10 <sup>-2</sup>	-0.07559661\(\lambda\) -0.07559661\(\lambda\) -0.07559661\(\lambda\) -2.07506000 \(\times\) 1075	11956100	3 2 7	2	0.47376935 .035020200 ~13575000 × 10 <sup>-2</sup> ~13570000 ~11360000	-0.084119408 .16609700 × 10 <sup>-2</sup> .33997000 .12964000 ,18900000 × 10 <sup>-3</sup>	0.809401A0 × 10 57201900 15189600 Ash00000 × 10 16610000
			·		<del></del>	λ = 2.5		_	_			
8 1	0.60267740 022076200 013257400 47420000 × 30-2	60000000 x 0000000000000000000000000000	0.4897540 × 10 <sup>-2</sup> 48775000 67666000 × 10 <sup>-3</sup> .1250000	2 0 4 1 6 2 8 3 10 4 12 5	0105/Jeco ·	-0.069994396 .89691400 × 10 <sup>-0</sup> .97648000 .753180000 × 10 <sup>-5</sup>	75357000 × 10 <sup>-3</sup>	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	ŀ	0.5894702 7589000 × 10 <sup>-0</sup> 04584400 4650000 × 10 <sup>-0</sup>	-0.0147/92/0 .0129/0000 × 10 <sup>-2</sup> .0129/0000 × 10 <sup>-3</sup>	0,5065710 × 10° 41465300 76498000 × 10° .1A700000 × 10°
	0,69045480 =.055575400 081428000 15550000 × 20 <sup>-2</sup> 45600000	-0.06990908 ,025446320 ,2565300 × 10 <sup>74</sup> 7500000 × 10 <sup>73</sup> 19130000 × 10 <sup>73</sup>	0.98590770 × 10 <sup>-2</sup> A1A45000SEESOOO × 10 <sup>-5</sup> SESOOOO	8 0 4 1 6 1 10 4	006056000 29950000 × 10 <sup>-2</sup>	-0.05260302 .01769350 .27658000 × 10 <sup>-5</sup>		7	2 3	0.5805667 068470000 018760000 × 10 <sup>-2</sup>	-0.066750050 .019453500 .019453500 .019530000 × 10 <sup>-2</sup>	0.336[9620 × 10 37525100 -77550000 × 10 -81750000 × 10

## APPIER I'm considered and mer cal, of $a^{2n}$ ' and $\frac{2^n}{2a^n}$ ' and $\frac{2^n}{2a^n}$ . Los n=0 so 2 yield decisions

### VALUES OF P FOR VARIOUS VALUES OF L AND \(\lambda\) - Continued

(f) L = 0.2 - Concluded

P	G <sub>n</sub> (P)	1 <u>98</u> 90 <sup>27</sup>	945 96	P	a a <sub>n</sub> (P)	1 <u>2f</u> 9g <sup>2</sup>	98. 30.	₽		G <sub>n</sub> (₽)	1 <u>9ľ</u> 90 <sup>D</sup>	90 <sup>1</sup>
						λ = 3-5						
2 1		-0.062844728 .027152070 -11287000 x 10 <sup>-2</sup> -20030000	0.19689940 × 10 <sup>-2</sup> 34156700 × 10 <sup>-2</sup> .86640000 × 10 <sup>-3</sup>	4		-0.057576648 .080669730 .15470000 x 10 <sup>-2</sup>	0.66691/100 × 10 <sup>-8</sup> 5011/200 .46820000 × 10 <sup>-5</sup> .22660000		위그	03.2406000	-0.060085784 .025817500 38770000 × 10 <sup>-3</sup> 10920000 × 10 <sup>-2</sup>	0.83480150 × 10 <sup>-2</sup> 38446100 .65580000 × 10 <sup>-3</sup> .85640000
		·	<del></del>			λ = 4.0	· · · · · · · · · · · · · · · · · · ·					
0 0 2 1 4 2 6 5 8 4 10 5	0.72005290 -,20890750 .01610000 × 10 <sup>-2</sup>	-0.075995430 .025041490 47550000 x 10 <sup>-2</sup> 11780000	0.14169770 x 10 <sup>-2</sup> 87888000 .11753000		5	-0.052645446 .025651090 .025651090 × 10 <sup>-2</sup>	0.19538640 × 10 <sup>-2</sup> -,26057600 ,04720000 × 10 <sup>-3</sup>	:	3 2		-0.094456802 .02623330 -35721000 × 10-2 -31010000	0.1685410 × 10 <sup>-2</sup> 27084600 .10054000
						λ = 6.0		ì				
0 0 2 1 4 2 6 3 8 4	.15180000	-0.035999540 .026749600 034060000	0.49173380 x 10 <sup>-3</sup> 12740900 x 10 <sup>-2</sup> .11405000			-0.058419746 .026205800 -,011966000	0.67989790 × 10 <sup>-5</sup> 12687500 × 10 <sup>-2</sup> .10544000	1		0. 76869689 - 37598670 - 11805000	-0.039034066 .027484100 002950000	0.58795660 × 10 <sup>-3</sup> 18756000 × 10-8 .10872000

TABLE I.- CONFUSED VALUES OF  $G_n$ ,  $1 \frac{\partial G_n}{\partial t}$ , AND  $\frac{\partial G_n}{\partial x^2}$  FOR n=0 to 5 AND DIFFERENCE VALUES OF L. AND  $\lambda$  - Continued.

(R)	L	Q.	3

P a	O <sub>n</sub> (P)	1 gr	90°	Pn	G <sub>n</sub> (P)	1 94 J	90°8 90°		P	G <sub>II</sub> (P)	) <u>91</u>	<u>∂o</u> _
						λ = 0.02				·	· · · · · · · · · · · · · · · · · · ·	
00	0.012241900	-0.296327k2	4.5463923	2 0 4 1					1 ( 3 )			
						λ = 0.06				·	<del></del>	<del></del>
0 0 2 1	0.036028300 . 0 (110 <sup>-39</sup> )	-0.289150 <sup>3</sup> 5 0(10 <sup>-57</sup> )	1,4585594 0(10~36)	2 O	0(10-39)	o(10 <sup>-3-7</sup> )	0(10-36)		1 0	0(10 <sup>-12</sup> )	o(10-10)	0,13743829 × 10 <sup>-8</sup>
					<u> </u>	λ = 0.10	·	***				<del></del>
0 0 2 1	0.078923400 0 (10 <sup>-16</sup> )	-0.26252299 0(10 <sup>-14</sup> )	0.84276119 0(10 <sup>-15</sup> )	20	o(10 <sup>-16</sup> )	0(10-14)	o(10 <sup>-13</sup> )	ш	1 0 3 1	0.18968600 × 10 <sup>-5</sup> 0(16 <sup>-52</sup> )	-0.31684296 × 10 <sup>-4</sup> 0(10 <sup>-31</sup> )	0.50525608 × 10 <sup>-3</sup> 0(10 <sup>-29</sup> )
			· · · · · · · · · · · · · · · · · · ·			λ = 0.20	<u>,                                    </u>			<del></del>		·
0 0 2 1 4 2	0.11252910 .34823300 × 10 <sup>-5</sup> 0(10 <sup>-15</sup> )	-0.26624126 28970133 × 10 <sup>-1</sup> 0(10 <sup>-14</sup> )	0.38565667 .228599919 × 10 <sup>-3</sup> 0(10 <sup>-13</sup> )	20 41	0.57508700 × 10 <sup>-5</sup> 2 0(10 <sup>-15</sup> )	-0.51154095 × 10 <sup>-1</sup> 0(10 <sup>-14</sup> )	0.24703046 x 10 <sup>-3</sup> 0(10 <sup>-13</sup> )	1	1 0 3 1	1	-0.014955749 17431589 × 10 <sup>-8</sup> 0(10 <sup>-22</sup> )	0.066 <del>797174</del> .20121778 × 10-7 0(10-20)
		<del> </del>		٠	<b>:</b>	λ = 0.40						
0 0 2 1 4 2 6 3 8 4	0.20610960 ,47190060 × 10 <sup>-8</sup> ,54719600 × 10 <sup>-5</sup> .22424000 × 10 <sup>-9</sup> o(10 <sup>-15</sup> )	-0,27816711 011117326 22706760 × 10 <sup>-8</sup> 15189640 × 10 <sup>-8</sup> 0(10 <sup>-14</sup> )	0.16031440 .023714510 .87760290 × 10 <sup>-4</sup> .757566900 × 10 <sup>-8</sup> 0(10 <sup>-13</sup> )	20 41 62 83	0.76203770 × 10 <sup>-2</sup> .66831700 × 10 <sup>-5</sup> .24767200 × 10 <sup>-9</sup> o(10 <sup>-3.5</sup> )	-0.014177919 -0.26074600 × 10 <sup>-1</sup> 14607260 × 10 <sup>-8</sup> 0(10 <sup>-14</sup> )	0.051295464 .10636265 × 10 <sup>-5</sup> .85904970 × 10 <sup>-8</sup> 0(10 <sup>-15</sup> )		1 0 3 1 5 2 7 3	-7-01 × 00275575-	-0.093492183 84297830 × 10 <sup>-5</sup> 28737830 × 10 <sup>-6</sup>	0.11958690 .25511841 × 10 <sup>-2</sup> .15864866 × 10 <sup>-5</sup> .0(10-10)

### Table 1.— co-pures values of $a_n$ , 0, $\frac{\partial a_n}{\partial t}$ , and $\frac{\partial a_n}{\partial t^2}$ for n=0 to 5 are linearized

#### VALUES OF P FOR VARIOUS VALUES OF L AND $\lambda$ - Continued

g) L = 0.7 - Continued

Pa	G <sub>m</sub> (1°)	<u> غد</u> غ <del>د</del>	হু খ	7 2	e <sub>t</sub> (P)	1 <u>95</u> 900	<u> </u>	,	n G <sub>n</sub> (P)	1 <u>90</u> 7	75
						λ = 0.60					
0 0 1 4 9 6 5 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	0.28466460 .004054720 .72196600 × 10 <sup>-3</sup> .7740000 × 10 <sup>-8</sup> 0(10 <sup>-11</sup> )	-0.4146061 050137140 13930420 × 10 <sup>-2</sup> 130278000 × 10 <sup>-2</sup> 0(10 <sup>-10</sup> )	0.090195500 .089195100 .58175500 × 10 <sup>-8</sup> .113580.00 × 10 <sup>-6</sup> .113580.00 × 10 <sup>-6</sup>	2 0 4 1 6 2 8 3	0.056076570 .95875000 × 10 <sup>-5</sup> .69051300 × 10 <sup>-5</sup> .11470000 × 10 <sup>-7</sup> 0(10 <sup>-11</sup> )	-0.045180606 15998515 × 10 <sup>-2</sup> 16775350 × 10 <sup>-3</sup> 40090600 × 10 <sup>-7</sup> o(10 <sup>-10</sup> )	0.03869887 .3408010 × 10 <sup>-8</sup> .1851986 × 10 <sup>-8</sup> .15566870 × 10 <sup>-6</sup> 0(10 <sup>-10</sup> )	1 7 9 11	2 .57970600 × 10 <sup>-3</sup> 3 .31084000 × 10 <sup>-6</sup> 4 .24547000 × 10 <sup>-9</sup>	-0,12040496 -,98896150 × 10 <sup>-2</sup> -,19977620 × 10 <sup>-5</sup> -,99796000 × 10 <sup>-6</sup> -,94612000 × 10 <sup>-9</sup> 0(10 <sup>-12</sup> )	
				12 5					3		· · · · · ·
			· · · · · · · · · · · · · · · · · · ·	<del>, , .</del>		λ = 0.80	<del> </del>			<u>.                                    </u>	r
0 0 0 2 1 4 2 6 5 8 4 10 5	0.3511866 .04301690 .40965600 × 10 <sup>-3</sup> .19544000 × 10 <sup>-5</sup> .43750000 × 10 <sup>-7</sup> .43660000 × 10 <sup>-7</sup>	-0,19464401 -,095186040 -,49518000 × 10 <sup>-2</sup> -,29795400 × 10 <sup>-3</sup> -,39109000 × 10 <sup>-3</sup> -,10094000 × 10 <sup>-6</sup>	0.071489060 .017249260 .40569230 × 10 <sup>-2</sup> .40567400 × 10 <sup>-3</sup> .17681900 × 10 <sup>-4</sup> .87797000 × 10 <sup>-6</sup>	8 0 6 2 8 3 10 4 12 5	0.08-976970 .69366800 × 10 <sup>-2</sup> .80093100 × 10 <sup>-3</sup> .58811000 × 10 <sup>-3</sup> .94160000 × 10 <sup>-7</sup> .81350000 × 10 <sup>-9</sup>	-0.074387513 77418740 × 10 <sup>-2</sup> 246014600 × 10 <sup>-3</sup> 11570000 × 10 <sup>-4</sup> 13650000 × 10 <sup>-6</sup> 66670000 × 10 <sup>-9</sup>	0.020808821 .71850440 × 10 <sup>-8</sup> .68658540 × 10 <sup>-5</sup> .81706800 × 10 <sup>-6</sup> .50385800 × 10 <sup>-6</sup> .17059000 × 10 <sup>-0</sup>	<b>  </b>   3	2 .120022800 x 10 <sup>-2</sup> 3 .37994000 x 10 <sup>-3</sup> 4 .55110000 x 10 <sup>-6</sup>	-0.15858584 -0.015787470 -1.6126170 × 10 <sup>-8</sup> 66289000 × 10 <sup>-3</sup> 11910000 × 10 <sup>-5</sup> 08880000 × 10 <sup>-8</sup>	0.069570860 .014218980 .11879850 × 10 <sup>-2</sup> .10850070 × 10 <sup>-3</sup> .25007400 × 10 <sup>-5</sup> .22808000 × 10 <sup>-7</sup>
`						λ = 1.0					
00 21 42 63 84	-29490000 × 10 <sup>-2</sup> -29490000 × 10 <sup>-2</sup> -29490000 × 10 <sup>-3</sup> -29490000 × 10 <sup>-3</sup>	"20160000 × 10.25 "138340000 × 10.25 "13834000 × 10.26 "1383638120 "1083638120	0.055404165 .60517000 × 10 <sup>-8</sup> .25140000 .98518000 × 10 <sup>-3</sup> .76860000 × 10 <sup>-3</sup>	2 0 4 1 6 2 8 5 10 4 12 5	0,1601138 ,01525300 .15054500 × 10 <sup>-12</sup> .960000 × 10 <sup>-13</sup> .3992000 × 10 <sup>-13</sup> .1050000 × 10 <sup>-14</sup>	-0.089330996 012535300 13090600 × 10 <sup>-2</sup> 12108300 × 10 <sup>-3</sup> 59590000 × 10 <sup>-3</sup> 17090000 × 10 <sup>-6</sup>	0.041818070 .76290090 × 10 <sup>-8</sup> .12616750 .15753300 × 10 <sup>-5</sup> .85599000 × 10 <sup>-5</sup> .50750000 × 10 <sup>-6</sup>	,	0 0.25150545 1 .05542540 2 .77675900 × 10 <sup>-2</sup> 3 .51840000 × 10 <sup>-3</sup> 4 .16760000 × 10 <sup>-4</sup> 5 .61800000 × 10 <sup>-6</sup>	-0.13407768 -0.021581970 -38108700 × 10 <sup>-2</sup> -55343000 × 10 <sup>-3</sup> -85096000 × 10 <sup>-4</sup> -87900000 × 10 <sup>-6</sup>	0.045763657 .91674700 × 10-8 .20567100 .36541600 × 10 <sup>-5</sup> .20559000 × 10 <sup>-1</sup> .11558000 × 10 <sup>-5</sup>
						λ = 1.2			· · · · · · · · · · · · · · · · · · ·		
0 0 2 1 4 2 6 3 8 4 10 5	0.4968430 .066067600 .95117000 × 10 <sup>-2</sup> .1449000 .18700000 × 10 <sup>-3</sup>	-0.16294670 019657450 77782100 × 10 <sup>-2</sup> 76760000 × 10 <sup>-3</sup> 15700000 15800000 × 10 <sup>-4</sup>	0.08970831 ~11697900 × 10 <sup>-8</sup> ~29994000 × 10 <sup>-3</sup> ~19190000 ~70500000 × 10 <sup>-1</sup> ~1110000	2 0 1 1 6 2 5 5 10 1 12 5	0.1951868 .0658680 .5515940 × 10 <sup>-2</sup> .5686900 × 10 <sup>-5</sup> .5659000 × 10 <sup>-5</sup>	-0,097045619 -,014186090 -,21548900 x 10 <sup>-8</sup> -,30558000 x 10 <sup>-5</sup> -,38500000 x 10 <sup>-5</sup>	0.053618531 .50515030 × 10 <sup>-28</sup> .10400200 .80575000 × 10 <sup>-5</sup> .80590000 × 10 <sup>-5</sup>	3 7 9 11	5 .75560000 x 10 <sup>-3</sup> 4 .85500000 x 10 <sup>-4</sup>	-0.15108780 01664610 51866400 × 10 <sup>-2</sup> 5406000 × 10 <sup>-3</sup> 75410000 × 10 <sup>-3</sup>	0.0339*7977 .33903000 × 10 <sup>-2</sup> .84630000 × 10 <sup>-3</sup> .23765000 .23050000 × 10 <sup>-1</sup>
-1-1	-1			_		) = 1-}	<del>-  </del>		1		
2 1 4 2 6 5 6 4	0.49518380 .095860100 .79870000 × 10-2 .11188000 .81540000 × 10-3	-0.15064485 50458000 × 10 <sup>-20</sup> 55550000 × 10 <sup>-20</sup> 15750000	0.081144979 -,58466000 x 10 <sup>-8</sup> -,20536700 -,41430000 x 10 <sup>-3</sup>	20 41 68 33 30 4	0.34716166 .051585610 .45656000 × 10 <sup>-2</sup> .68680000 × 10 <sup>-3</sup> .88600000 × 10 <sup>-3</sup>	.0.099872719 (URURLISO 12005600 × 10 <sup>-2</sup> 51190000 × 10 <sup>-3</sup> 57500000 × 10 <sup>-3</sup>	0.08693840 .16004900 × 10 <sup>-5</sup> .17906000 × 10 <sup>-5</sup> .69980000 × 10 <sup>-5</sup> .88770000	3	17/2/10000	-0,129487799 -,012487950 -,16278500 × 10 <sup>-2</sup> -,72460000 × 10 <sup>-3</sup>	0.009486160 -,11100500 × 10 <sup>-2</sup> 60339000 × 10 <sup>-3</sup>

# TRAILS I.- CONTRIBES OF $G_{n}$ , $g = \frac{\partial G_{n}}{\partial g}$ , and $\frac{\partial G_{n}}{\partial x^{n}}$ for x = 0 to 5 and instance. Values of P for values waters of I. And $\lambda$ - Continued.

(g) L = 0.3 - Continued

-   -	G <sub>n</sub> (P)	) <u>96</u>	90° 90°	P	G <sub>m</sub> (₽)	1 <u>श</u> व्र	84 84	7	*	ā <sub>n</sub> (x)	<del>ار</del> و د ت <u>و</u> و	%4 2⊒≷
						λ = 1.6						
2 1 4 2 6 3 6 4 10 7	0.79611610 .040979800 .24069000 × 10-8 17500006 × 10-4	-0.1791/0516 -0.465000 × 10 <sup>-76</sup> -0.9579000 × 10 <sup>-76</sup> -0.12944007 -0.12944007	66140000 x 20-5 12730000 0.012671211	6 2 8 3 10 4 12 5	-580k2000 x 10 <sup>-2</sup>	-0.09991/fore -76706400 x 10-2 -757540000 x 10-3  \[ \lambda = 1.6 \] -0.099729898		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 2 3 4 5	0.40577148 .08553900 .7955000 × 10 <sup>-2</sup> .90680000 × 10 <sup>-3</sup>	-0.1909055 51090000 x 10 <sup>-2</sup> .5100000 x 10 <sup>-3</sup> .1950000 -0.11508905 .22761700 x 10 <sup>-3</sup>	0.020001765 1150700 x 10 15564400 54630000 x 10 0.003798001 55071760 x 10
* 2 6 5 8 4 0 5	- 35/20000 × 30 <sup>-2</sup>	.9652000 .0007,000 .0007,000 .707,0000	~.50072000 × 10 <sup>-3</sup>	6 8 6 8 10 4	.06729400 .1602000 × 10 <sup>-2</sup>	-, 82495400 x 10 <sup>-2</sup> -,98090000 x 10 <sup>-3</sup> -,89330000	384322600 × 30 <sup>-8</sup>	Ŋ,	4	52900000 × 10 <sup>-3</sup>	.25040000 × 10 <sup>-5</sup>	- 184.98600
익시	0.59715570 55599000 × 30 <sup>-2</sup> 52224000	-0.19059128 .017175080 .95975000 × 30°*	0.010095592 99865900 × 10 <sup>-2</sup> 1995000 9987000 × 10 <sup>-3</sup>	2 0 4 1 6 8 8 5 10 4	65600000 × 10 <sup>-5</sup>	-0.092839797 .5978800 × 10 <sup>-8</sup> .28396000 .5\480000 × 10 <sup>-5</sup>	~13040000	]	2 3	0,45361554 .010564000 -10565000 × 30 <sup>-2</sup> -15676000	-0.10939048 .9094300 x 10 <sup>-0</sup> .91949000 .83460000 x 10 <sup>-3</sup>	0,019674742 68614800 × 10 16748000 29980000 × 10
-4-3			<del></del>		<u> </u>	À = 2.5		ш	ч			
	0.65565240 065523800 06522000 J8550000 x 20 <sup>-8</sup>	.0.10350420 .9308470 .97594000 x 10 <sup>-©</sup>	0.65300690 × 10 <sup>-2</sup> 89054900	4 1 6 2	0,46341066 08438900 90040000 x 10 <sup>-12</sup> 14840000	-0.05%85065 .015867000 .51058000 x 10 <sup>-0</sup>	0.8995000 × 10-2 ,5786000 × 30-3	1 5 7 9	1 2 3 4	0.2776535 043541900 012703000 16750000 × 10 <sup>-2</sup>	-0.096360447 .082994130 .34989000 x 10 <sup>-4</sup>	0.77566300 × 107 72663000 58740000 × 107
0 0 2 1 4 2 6 3 8 4	0.70057120 17585980 86500000 × 10 <sup>-12</sup> 88200000	-0.099006311 .097886300 -21593000 x 30 <sup>-22</sup>	0.39959480 × 10 <sup>-2</sup> 69699000 -14432000 -40800000 × 10 <sup>-3</sup>		-	-0.079900968 .084129270 .72000000 x 10 <sup>-3</sup>	0.5902560 × 10 <sup>-2</sup> 5685560 -5490000 × 10 <sup>-5</sup>	) z	2	2.6186,000 2.10556560 2.10556560 2.105656000 × 30−€	-0-002998039 -09068400 -24900000 × 20 <sup>-3</sup>	0.508(8750 x 10 -,65045000 ,94140000 x 30

# TABLE 1.- COMPUTED VALUES OF $G_n$ , $j\frac{\partial G_n}{\partial z}$ , AND $\frac{\partial G_n}{\partial z^2}$ FOR z=0.20.5 AND DEFINISHE VALUES OF F FOR VARIOUS VALUES OF L AND $\lambda$ - Continued

(g) L = 0.3 - 0opoluded

P	G <sub>3</sub> (P)	i <u>90</u>	94 <sub>5</sub>	P	n G <sub>n</sub> (P)	1 9t	900 900	,	,  ,	G <sub>n</sub> (P)	1 9t yr.	97.5 90 <sup>7</sup>
		<del></del>				λ = 3.5	· · · · · · · · · · · · · · · · · · ·			•	<del></del>	<u> </u>
2 7		-0.079367277 .040709900 66780000 x 10 <sup>-2</sup>	0.26771910 × 10 <sup>-2</sup> 54590500 .21796000		<u> </u>	-0.072530940 .050887400 31710000 × 10 <sup>-2</sup>	0.40875040 × 10 <sup>-2</sup> 49050500 .13587000			· · · · · · · · · · · · · · · · · · ·	-0.076305770 .095558500 47210000 x 10 <sup>-2</sup>	0.34345720 × 10 <sup>-5</sup> 52259700 .17446000
					•	X = 4.0	· · · · · ·					
- 1		-0.070989585 .041906700 011595000	0.18975550 × 10 <sup>-2</sup> *5185800 .8**15000	£	3	-0.06606528 .033440700 73580000 x 10 <sup>-2</sup>	0.29259850 × 10-2 A1122000 .15016000				-0.068755680 .037626800 95360000 x 10 <sup>-2</sup>	0.24432590 x 10 <sup>-2</sup> -,42490600 .22140000
						λ = 6.0					_	
		-0.049593037 .038404700 023903000 .031680000	0.65565700 × 10 <sup>-5</sup> 18087800 × 10 <sup>-2</sup> .19090000	4	¥	-0.047754861 .034659900 018343000	0.996a9700 × 10 <sup>-3</sup> 19194500 × 10 <sup>-2</sup> .17660000			.16810000	-0.0\8663695 .036560000 00005000 .010\70000	0.61970500 × 10 <sup>-5</sup> 18750400 × 10 <sup>-2</sup> .18440000

## TRABLE I... COMPUTED VALUES OF $G_{n_2}$ , $J \frac{\partial G_{n_1}}{\partial g}$ , and $\frac{\partial G_{n_2}}{\partial g^2}$ for g=0 to 5 and intermed

#### VALUES OF P FOR VARIOUS VALUES OF L. AND \(\lambda\) - Continued

(h) L = 0.4

Pn	G <sub>22</sub> (P)	1 <u>9</u> ¢ 90 <sup>0</sup>	dang dang	Pn	O <sub>zz</sub> (P)	ე <del>9€</del> gg <sup>20</sup>	ბი <u>ო</u> 2		Pn	a <sub>n</sub> (P)	i ge <sup>u</sup>	90 <sup>2</sup>
				:		λ = 0.02	··				·	
0 0 2 1	0.014114500	-0.39\35\20 	6.9 <del>1817</del> 549	20- 41-				Ш	1 0 3 1			
			-			λ = 0.06						
0021	0.041419300	-0.585A3250	2.2254592	20-					3 1	0(10-15)	0(10-13)	α(τυ-11)
				<u> </u>	· · · · · · · · · · · · · · · · · · ·	λ = 0.10	<del>'</del>			l. <u></u>		<u></u>
0 0 2 1	0.067547800 0 (10 <sup>-20</sup> )	-0.37296066 o(10 <sup>-16</sup> )	1.2781070 0(10 <sup>-17</sup> )	20	o(10- <del>2</del> 0)	o(10 <sup>-18</sup> )	0(10-17)		3 1	0.13980440 × 10 <sup>-6</sup> 0(10 <sup>-12</sup> )	-0.30417595 × 10 <sup>-5</sup> 0(10 <sup>-40</sup> )	0.65582570 × 10 <sup>-1</sup> 0(10 <sup>-56</sup> )
						λ = 0.20		_		· · · · · · · · · · · · · · · · · · ·	<del></del>	<del> </del>
0 0 2 1 4 2	0,1281,5560 •25597700 × 10 <sup>-6</sup> 0(10 <sup>-20</sup> )	-0.34874636 27754388 × 10 <sup>-5</sup> 0(10 <sup>-1,6</sup> )	0.57415104 .288599258 × 10 <sup>-1</sup> 0(10 <sup>-1</sup> 7)	200 41	0.27481410 × 10-6 0(10 <sup>-20</sup> )	0(70- <sub>78</sub> ) -0°88 <u>81122</u> 4 × 70- <sub>2</sub>	0.3120 <b>4</b> 535 × 10 <sup>-4</sup> 0(10 <sup>-17</sup> )	: 11	3 1	0.14914160 × 10 <sup>-2</sup>	-0.95483836 × 10-2	0.054765007 0(10 <sup>-9</sup> )
						λ = 0.40					•	<del></del>
0 0 2 1 4 2 6 3	0.25186450 .22404120 × 10 <sup>-2</sup> .39957500 × 10 <sup>-6</sup> 0(10 <sup>-12</sup> )	-0.50725420 69801720 × 10 <sup>-2</sup> 21441900 × 10 <sup>-2</sup> 0(10 <sup>-11</sup> )	0.2559851k .019291809 .11043450 × 10 <sup>-k</sup> 0(10 <sup>-10</sup> )	200 11 62	0(10 <sup>-12</sup> )	-0.90076160 x 10 <sup>-2</sup> 8488610 x 10 <sup>-5</sup> o(10 <sup>-11</sup> )	0.025686925 .12896410 × 10 <sup>-1</sup> 0(10 <sup>-10</sup> )		1051	.10216700 x 10 <sup>-8</sup>	-0.089081380 -28129210 × 10 <sup>-5</sup> 67092800 × 10 <sup>-8</sup> 0(10 <sup>-13</sup> )	0.15557004 .95757140 × 10 <sup>-5</sup> .42654720 × 10 <sup>-7</sup> 0(10 <sup>-15</sup> )

## TABLE I.- COMPUTED VALUES OF $d_{\rm D}$ , $d_{\rm T} = \frac{\partial d_{\rm D}}{\partial z}$ , AND $\frac{\partial d_{\rm D}}{\partial z^2}$ FOR n=0 TO 5 AND DITEMPER

VALUES OF P FOR VARIOUS VALUES OF L AND \(\lambda\) - Continued

(h) L = 0.4 - Continued

Pn	a <sub>n</sub> (P)	j <u>90</u> 2	90°5	Pa	G <sub>n</sub> (P)	1 <u>90</u> ₽	98 87	P	n G <sub>R</sub> (P)	i gra	90°5
<u>L</u>	<u> </u>					λ = 0.60					
2 1 4 2	0.51688050 .017059550 .21195400 × 10 <sup>-5</sup>	-0.27324787 026413770 52835500 x 10 <sup>-5</sup>	0.12698406 .052686180 .12047620 × 10 <sup>-2</sup>	2 O	0.026\81560 .28550100 × 10 <sup>-3</sup>	-0.043022228 72751600 × 10 <sup>-5</sup>	0.060760575 .17070210 × 10 <sup>-2</sup>	3	0 0.111 <i>75778</i> 1 .28300660 × 10 1	. 1	0.12510047 .010393557 .11573500 × 10 <sup>-5</sup>
6 3 8 4 10 5	.40599000 × 10 <sup>-5</sup> 0(10 <sup>-10</sup> )	14198900 × 10 <sup>-9</sup> 45677000 × 10 <sup>-9</sup>	.47896800 × 10 <sup>-5</sup> .20436800 × 10 <sup>-8</sup> o(10 <sup>-13</sup> )	6 2 8 3 10 4 12 5	o(10-174) •174,000 × 10-6	17820750 x 10 <sup>-9</sup> 54578000 x 10 <sup>-9</sup>	.60704540 × 10 <sup>-5</sup> .24458550 × 10 <sup>-8</sup> o(10 <sup>-12</sup> )		95 .90550000 x 10° 0 (10-12)	0 (10-11)	.14479090 x 10 <sup>-6</sup> 0(10 <sup>-10</sup> )
├┴┴		<u> </u>	L. , ,,_		<u> </u>	λ = 0.80		Ш	<u> </u>	<u> </u>	<u>L</u>
00	0.38735490	-0.2450580g	0.080389900	<u> </u>	<del></del>	<u>, , - 5155</u>		Π,	0 0.18996484	-0.15606601	
£ 1	.036145300 .13279300 × 10 <sup>-2</sup>	053561680 27325400 x 10 <sup>-2</sup>	.020696340 .9261,9900 × 10 <sup>-2</sup>	2 O	0.0717711640 .31727170 × 10 <sup>-2</sup>	-0.076720768 47726500 × 10 <sup>-0</sup>	0.064809339 .62636730 × 10 <sup>-8</sup>	<b> </b>    3	2 .39919500 × 10	0150\1920	0.090177800 .014745292 .10717930 × 10 <sup>-2</sup>
6 3 8 4 30 5	.\$1692000 × 10 <sup>-6</sup> .\$1550000 × 10 <sup>-6</sup> .7\$200000 × 10 <sup>-9</sup>	82591000 x 10 <sup>-1</sup> 75490000 x 10 <sup>-6</sup> 85450000 x 10 <sup>-8</sup>	.19677000 x 10 <sup>-5</sup>	6 2 8 3	.60635000 × 10 <sup>-4</sup> .41617000 × 10 <sup>-6</sup>	12552520 x 10 <sup>-5</sup> 10861500 x 10 <sup>-5</sup>	.27207400 x 10 <sup>-5</sup>	9		757730000 × 30-7	.24320400 × 10 <sup>-4</sup> .16154000 × 10 <sup>-6</sup>
֓֟֟֓֟֟֟֓֟֟֓֟֟֓֟֓֟֓֟֓֟֓֟֓֟֓֟֓֓֟֓֓֟֓֓֟֓֓֟	· isamment Tra	KA-20000 X 10	.72570000 × 10 <sup>-8</sup>	10 4 12 5		301/3000 × 10 <sup>-8</sup> 0(10 <sup>-11</sup> ) λ = 1.0	0(10-11)	11.	5 0(10-10)	o(10-30)	.50960000 × 10 <sup>-9</sup>
اماه	0.44639380	-0.221kh2k7	0.054152940	ГТ	-	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		1	0 0.2547653.0	-0.15998511	0.065154140
21	.047781900	088039770	.622278900 × 10 <sup>-2</sup>	20	0.12660600	-0.097794956	0.056556767		1 .025946950	018972720	.01.0265970
4 2	.46002500 x 10 <sup>-2</sup>	39408900 × 10 <sup>-2</sup>	,22535300	4 1	.90242700 × 10 <sup>-2</sup>	97106700 × 10 <sup>-2</sup>	.76941470 × 10 <sup>-2</sup>	5	2 17470600 × 10"	_	.1666e400 × 10 <sup>-2</sup>
6 3	.29548000 x 10 <sup>-5</sup>	55814000 × 10 <sup>-3</sup>	.36374000 x 10 <sup>-3</sup>	6 2	.55089000 × 10 <sup>-5</sup>	68869800 × 10 <sup>-5</sup>	.78e46600 x 10 <sup>-3</sup>	7	5 .78960000 x 10-	-,112 <b>59000</b> x 10 <sup>-3</sup>	.14558200 × 10 <sup>-3</sup>
[8 4	·10690000 × 10-4	19610000 × 10	.24550000 × 10 <sup>-4</sup>	8 3	.16757000 × 10 <sup>-1</sup>	27589000 x 10 <sup>-4</sup>	.42207000 × 10 <sup>-1</sup>	9	4 .19910000 × 10-	5 - 35840000 x 10 <sup>-5</sup>	.59080000 x 10 <sup>-5</sup>
<sup>10</sup> 기			.78350000 x 10 <sup>-6</sup>	10 4	.28520000 × 10 <sup>-6</sup>	~.55410000 × 10 <sup>-6</sup>	.10867000 × 10-7	ը	5		7-10850000 × 10 <sub>-6</sub>
				12 5	.25400000 × 10 <sup>-15</sup>	- 5+100000 x 10 <sup>-6</sup>	.1261.000 x 10-7	Ш		<u> </u>	<u> </u>
	0.49653600	o emilénée		1 1		λ = 1.2	<del></del>	П.	0 0 00 00 000	T	
21	.045441800	-0.20146560 016618720	0.058555570 59205500 x 10 <sup>-2</sup>		0.18505590	-0.10920900	0.046410558	H 1	0 0.31614532	-0.15729712	0.048045820
42	.56162000 × 10 <sup>-2</sup>	25812000 × 10 <sup>-2</sup>	~.3k008000 x 10 <sup>-5</sup>	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.017186350	01.621.60	.73252400 × 10 <sup>-2</sup>	11 1	1 .051346150 2 .38008400 × 10 <sup>-1</sup>	016754790	.80910000 × 10 <sup>-2</sup>
6 5	.61600000 x 10 <sup>-5</sup>	12770000 x 10 <sup>-3</sup>	.14956000	6 2	.14920100 × 10 <sup>-2</sup>	12709000 × 10 <sup>-2</sup>	.82896000 x 10 <sup>-3</sup>	7	11 -		17345000
8 4	55500000 × 10-4	47430000 × 10 <sup>-1</sup>	-4005000 × 10 <sup>-1</sup>	8 3	.10238000 × 10 <sup>-3</sup>	~.10984000 × 10 <sup>-3</sup>	.10299000	او اا	l I	1 .	.20820000 × 10 <sup>-1</sup>
10 5			,	10 4	.55100000 x 10 <sup>-5</sup>	61200000 × 10 <sup>-5</sup>	.81.620000 × 10 <sup>-5</sup>	ļц	1 1 '	.93600000 × 10 <sup>-5</sup>	.80\60000 x 10 <sup>-5</sup>
Ш				12 5			. <sup>:</sup> 	$\  \ $		<u> </u>	<u> </u>
<del>,</del> ,						λ = 1.4		<del></del>	<del></del>		
000	0.55896No	-0.18441426	0.026184270					4	0 0.37025975	ì	0.036217534
2 1	.059023100	57976400 × 30 <sup>-2</sup>	98167 <del>7</del> 00 x 10 <sup>-2</sup>		0.25719289	_1	0.057415955	3	1 1.051688700	96374900 x 10 <sup>-Q</sup>	24329100 × 10 <sup>-2</sup>
12	.37690000 x 10 <sup>-2</sup>	-53740000 × 10 <sup>-5</sup>	22558000	4 1	.021.624090	96197800 x 10 <sup>-2</sup>	.15577000 x 10 <sup>-2</sup>	5	2 .55186000 x 10 <sup>-4</sup>		58\55000 x 10 <sup>-3</sup>
93	.51870000 x 10 <sup>-3</sup>	43700000 × 10 <sup>-4</sup>	~.8813000 × 10 <sup>-5</sup>	6 2	.21,920000 × 10 <sup>-8</sup>	11279000	.18744000 × 10 <sup>-3</sup>	7		17540000	-,21800000 × 10 <sup>-1</sup>
8 4			<del></del>	8 3	.22040000 x 10 <sup>-3</sup>	14670000 × 10 <sup>-3</sup>	.58200000 × 30 <sup>-1</sup>	9	4		
ᄳ키	<del></del>	·		10 4	<del></del>	15110000 x 10 <sup>-4</sup>	.119e000 × 10 <sup>-4</sup>	삗	5	· · · · · · · · · · · · · · · · · · ·	
Ш		<u>_</u>		12 5	*			<u>II_I</u>		<u> </u>	

# SHEET I.- CONTRIBE VALUES OF $G_{n}$ , $j\frac{\partial G_{n}}{\partial g}$ , and $\frac{\partial G_{n}}{\partial w^{2}}$ for n=0 to 5 and different values of k. And k — Continued

(h) L = 0.4 - Continued

,	a <sub>n</sub> (P)	1 <u>96</u> €	95 95	Pa	G <sub>n</sub> (F)	2 <u>94</u> .	8 B	P	a G <sub>h</sub> (P)	7 <u>9</u> 4	30 <sub>3</sub> 3≠2
						λ = 1.6					
0 0 0 2 1 4 2 6 5 8 4	0.97969990 .021790600 	-0.169(386e .82516300 × 10 <sup>-2</sup> .50566000 .48800000 × 10 <sup>-5</sup>	0.021310758 012760670 29129000 × 10 <sup>-2</sup> 50060000 × 10 <sup>-5</sup>	8 0 4 1 6 2 8 3 10 4 18 5		-0.11545428 52812200 x 10 <sup>-2</sup> 90480000 x 20 <sup>-5</sup>	0.030120386 20251700 × 10 <sup>-2</sup> 61451000 × 10 <sup>-5</sup>	5 5 7	0.A178530E 1.084759200 1.16647000 × 10 <sup>-2</sup> 5.17560000 × 10 <sup>-2</sup>		0.027865308 64485900 × 10 19708000 24340000 × 10
	<del></del>					X = 1.8					•
0 0 2 1 4 2 6 3 8 4	0.60747590 11082000 × 10 <sup>-2</sup> 50571000 92100000 × 10 <sup>-5</sup>	-0.15701046 .016695870 .14275000 × 10 <sup>-2</sup> .78900000 × 10 <sup>-3</sup>	0.016490881 017070660 25840000 x 10 <sup>-2</sup> 40660000 x 10 <sup>-3</sup>	2 0 4 1 6 2 8 5 10 4 12 5	.29520000 × 10 <sup>-5</sup>	-0.11\28798 .6772000 × 10 <sup>-5</sup> .30548000 × 10 <sup>-6</sup>		7	0 0.15970782 51 .011505900 52 -11220000 × 10 <sup>-1</sup> 75 -38400000 × 10 <sup>-1</sup>	.	0.021832107 88425400 x 10 18650000 30710000 x 10
ш			L	LL		λ = 2.0		ш.	<del>-1-1</del>	<u></u>	<del>!</del>
2 1 2	0.65546780 027622800 92056000 × 10 <sup>-4</sup> 14550000	-0.1\699299 .02[513500 .508\1000 × 10 <sup>-2</sup>	0.015007609 017911150 17138000 × 10 <sup>-2</sup>	20 41 62 83 154	59800000 x 10 <sup>-3</sup>	-0.1117689k .70601800 × 10 <sup>-2</sup> .20712000 .3890000 × 10 <sup>-3</sup>	0.015868762 69715900 × 10 <sup>-2</sup> 12907000 17850000 × 10 <sup>-5</sup>	3	1 o 0.49697582 5 16685000 x 10 <sup>-4</sup> 5 247618000 7 5 ~.8220000 x 10 <sup>-3</sup> 9 4	.54933000 × 10 <sup>-8</sup>	
						λ = 2-5					
8	0.69260790 10118510 010639600	-0.12501702 .041868300 .37982000 × 10 <sup>-2</sup>	0.7651500 × 10 <sup>-2</sup> 02845610 .97690000 × 10 <sup>-3</sup>			-0.1025219 .021478000 .21505000 × 10 <sup>-2</sup>	0.002779882 86511300 × 10 <sup>-5</sup> 87420000 × 10 <sup>-5</sup>	3	1.0 0.57801711 5 1065065500 5 286560000 x 10 <sup>-7</sup> 7 5	-0.11\hb\n36 .050699700 .21694000 x 10 <sup>-4</sup>	0.010424098 01027780 .28960000 x 10
	··- · · · · · · · · · · · · · · · · · ·			ш.	<del></del>	λ = 5.0	·		. <u>.                                   </u>	······································	<del> </del>
	0, 13518830 1752130 .51180000 × 10 <sup>-2</sup>	-0.10ft2[0] .04920000 51070000 x 10 <sup>-2</sup>	0.48658150 × 10 <sup>-2</sup> 55585800 -87655000	4 3	0.55150300 094970800 86700000 x 10 <sup>-2</sup>	0.095\7666\ .052657600 13970000 × 10 <sup>-0</sup>	0.601717990 × 10-2 76261300		5 113069090 5 274300000 x 10 <sup>-1</sup> 7 3	-0.10050208 .095978000 87690000 x 10 <sup>-4</sup>	0.66866670 x 1 88181500 .19853000
כ מנ		<del></del>		20 h				1	1 5		

## Table I.- Computed values of $a_n$ , $a = \frac{\partial a_n}{\partial z}$ , and $\frac{\partial a_n}{\partial z^n}$ for n = 0 to 5. And intergrant

#### VALUES OF E FOR VARIOUS VALUES OF L AND $\lambda$ - Continued

### (h) L = 0.4 - Concluded

P	n	a <sub>n</sub> (P)	1 <u>9;</u> 90 <sup>2</sup>	क्ष <sub>र</sub> इत्म	P	o <sub>n</sub> (P)	ا <del>و</del> د م	<u>સ્ત્રુ</u> એક્ <sup>2</sup>	P	Ħ	o <sub>n</sub> (P)	1 <u>96</u>	9°5 90°5
Γ							λ = 3.5				-		<u>.</u>
]    - 			-0.099740696 .059175900 011367000	0.58877250 x 10 <sup>-2</sup> 74725900 .56030000	6	5	-0.084767812 .037341200 -:61490000 x 10 <sup>-2</sup>	0.55667650 × 10 <sup>-2</sup> 67476400 .22649000	:	1 2 3	0.67376218 19553020 .019413000	-0.069825820 .044827300 87300000 × 10 <sup>-2</sup>	0.45281200 × 10 <sup>-2</sup> 71984500 -28940000
			<u> </u>			· · · · · · · · · · · · · · · · · · ·	λ = 4.0	·			<u></u>	<u> </u>	
1 1 1		0.79138890 30576970 .064877000	-0.083444460 .098690200 017655000	0.25046980 × 10 <sup>-2</sup> 56133500 .36190000	6 8	0.65027929 121194980 2 .035015000	-0.077113656 .041191400 011913000	0.39960280 × 10 <sup>-2</sup> 56034700 .27720000				-0.080692956 .046885800 014909000	0.51829980 × 10 <sup>-2</sup> 57737600 -32710000
							እ = 6.0						
1 1 1		0.85602580 48809060 .82520000	-0.09/590496 .046359700 020/56000	0.75212500 × 10 <sup>-3</sup> 2550000 × 10 <sup>-2</sup> .26140000		5	-0.075703520 .043450000 027660000	0.13640520 x 10 <sup>-2</sup> 25448000 .24660000				-0.056690128 .045957500 026050000	0.10469690 × 10 <sup>-2</sup> 24561000 .25380000

# TABLES I.— COMPUTED VALUES OF $G_n$ , $5\frac{\partial G_n}{\partial \xi}$ AND $\frac{\partial G_n}{\partial n^2}$ FOR n=0 TO 5 AND INTEGER VALUES OF F FOR VARIOUS VALUES OF L AND $\lambda$ — Continued

### (i) L = 0.5

P n	G <sub>n</sub> (F)	1 30 <u>n</u>	90°5	Pn	a <sub>n</sub> (P)	1 gr <sup>2</sup>	હેલું. જેવ <sup>2</sup>	P	n G <sub>n</sub> (P)	1 <u>94</u>	9 <sup>20</sup> 5 93 <sup>17</sup>
						λ = 0.02					
0 0 2 2 1	0:015759900	-0.49212006	9.TE <b>[49</b> ]2	20		Marian (1997)		ı ı	1		
			· · · · · · · · · · · · · · · · · · ·			λ = 0.06	· · · · · · · · · · · · · · · · · · ·				
00	0.046129200	-0.47699545	3.0860513	20-				3	o o(10~18)	0(10-16)	0(10-14)
	<del></del>		<del> </del>	<del></del>		y = 0°T0			····		
0 0 2 1	0.07504e600 0(20-24)	-0.46647869 0 (10 <sup>-623</sup> )	1.7654721 0(10- <sup>21</sup> )	20 1-	o(10- <b>34</b> )	0 (10-25)	0(10-51)	61 .	0 0.10508080 × 10 <sup>-7</sup>	7 -0.28139968 × 10 <sup>-6</sup>	0.72968974 × 10 <sup>-5</sup>
	<del>, , , , , , , , , , , , , , , , , , , </del>	<del></del> -				λ = 0.20					
0 0 2 1 4 8	0.14152040 .19196400 x 10 <sup>-7</sup> 0(10 <sup>-84</sup> )	-0.48983983 25641568 × 10 <sup>-6</sup> o(10 <sup>-25</sup> )	0.78275781 .53122586 × 10 <sup>-5</sup> 0(10 <sup>-21</sup> )	200 41	0 (10 <sup>-24</sup> )	-0.27633889 × 10 <sup>-6</sup> 0(10 <sup>-83</sup> )	0.35786526 × 10 <sup>-5</sup> 0(10 <sup>-21</sup> )	3	0 0.7761.0200 × 10 <sup>-1</sup> 1	-0.58316270 × 10 <sup>-6</sup> 0(10 <sup>-13</sup> )	0.040904925 0(10 <sup>-12</sup> )
						λ = 0.40					· · · · · · · · · · · · · · · · · · ·
0 0 2 1 4 2 6 3	.29797800 × 10 <sup>-7</sup>	-0.37327717 42181690 × 10 <sup>-1</sup> 19735240 × 10 <sup>-1</sup> 0(10 <sup>-1</sup> )		2 0 0 4 1 6 2	1.14309200 × 10 <sup>-2</sup> .54481900 × 10 <sup>-7</sup> 0(10 <sup>-14</sup> )	-0.5%9%2180 × 10 <sup>-6</sup> 229552%0 × 10 <sup>-6</sup> o(10 <sup>-1,5</sup> )	0.015153660 .14765211 × 10 <sup>-5</sup> 0(10 <sup>-1,2</sup> )	]] 3	0 0.034585840 1 .128555840 × 10 2 0(10-10)	-0.0683377980 66980330 × 10 <sup>-2</sup> 15189870 × 10 <sup>-2</sup>	

# THE E I. - CONCRISION VALUES OF $G_{\rm R}$ , $J = \frac{\partial G_{\rm R}}{\partial L}$ , and $\frac{\partial G_{\rm R}}{\partial m^2}$ for m=0 20 5. And increment values of P. Mor various values of L. and $\lambda$ - Concissoed

(1) L = 0.5 - Continued

4 1 1

2 =	a <sub>n</sub> (₽)	1 <u>96</u>	80 <sub>m</sub>	7 .	а <sub>р</sub> (Р)	) <u>80,</u>	8 <b>4</b> 8√2	,		G <sub>n</sub> (P)	1 <u>95</u> 90 <sup>2</sup>	97 <sub>6</sub>
						λ = 0.60						
9 4 4 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.34551890 ,018187510 .65744800 × 10 <sup>-4</sup> .29904000 × 10 <sup>-7</sup> 0(10 <sup>-13</sup> )	-0.32534073 026733-510 15555-510 × 10 <sup>-5</sup> 15008200 × 10 <sup>-6</sup> 0(10 <sup>-11</sup> )	0.162m0165 .055637050 .53657050 × 10 <sup>-5</sup> .54695500 × 10 <sup>-6</sup> .0(10 <sup>-10</sup> )	# 0 # 1 6 # 5 5	o(10 <sup>-11</sup> )	-9.098099891 86883160 × 10 <sup>-5</sup> 16967790 × 10 <sup>-6</sup> o(10 <sup>-11</sup> )	0,065850970 ,78086560 × 10 <sup>-3</sup> .69781300 × 10 <sup>-6</sup> q(10 <sup>-10</sup> )	ıu	10127794 1012794	0.1009366 .14093500 × 10 <sup>-8</sup> .21531700 × 10 <sup>-9</sup> .27344000 × 10 <sup>-9</sup> 0(10 <sup>-14</sup> )	-0.14978049 34710050 × 10 <sup>-8</sup> 80058800 × 10 <sup>-5</sup> 13681500 × 10 <sup>-6</sup> o(10 <sup>-13</sup> )	.26557110 × 10"
						λ = 0.80						
00 21 42 63 64 105	0.41649630 .cm8666140 .gm854000 × 10 <sup>-5</sup> .gm890000 × 10 <sup>-5</sup> .sm870000 × 10 <sup>-7</sup> 0(10 <sup>-10</sup> )	-0.53175197 -031116660 16012500 × 10 <sup>-3</sup> 88348000 × 10 <sup>-3</sup> 72590000 × 10 <sup>-7</sup> 0(10 <sup>-10</sup> )	0.10346838 .085049089 .82583100 × 10 <sup>-8</sup> .51159000 × 10 <sup>-8</sup> .28445000 × 10 <sup>-6</sup> .80550000 × 10 <sup>-9</sup>	20 41 68 83	.50700000 × 10 <sup>-7</sup>	-0.075550005 9545500 × 10 <sup>-8</sup> 5545500 × 10 <sup>-8</sup> 99455000 × 10 <sup>-8</sup> 0(10 <sup>-10</sup> )	.79120800 × 10 <sup>-1</sup>	<b>   </b>     .	10 51 59 75 94	0.18197678 .80*80000 × 10 <sup>-2</sup> .18973900 × 10 <sup>-3</sup> .6480000 × 10 <sup>-6</sup> .75900000 × 10 <sup>-9</sup>	-0.1700705 011703110 02765200 × 10 <sup>-5</sup> 02765000 × 10 <sup>-6</sup>	0.11799708 .014077667 .55670500 × 10 <sup>-1</sup> .9600000 × 10 <sup>-1</sup>
				LI	······································	λ = 1.0	r	ш.			L	· · · · · · · · · · · · · · · · · · ·
0 0 2 2 4 2 6 3 5 4 30 5	0.47694750 .076980100 .6696400 × 10 <sup>-8</sup> .10660000 × 10 <sup>-5</sup>	-0.26157628 -0.2652100 -27797000 × 10 <sup>-2</sup> -1.2650000 × 10 <sup>-3</sup> 25970000 × 10 <sup>-3</sup>	0.06668m00 61006100 × 10 <sup>-8</sup> 2066600 80636000 × 10 <sup>-5</sup> .6982000 × 10 <sup>-5</sup>	20 41 62 83 104 105	0.11359311 .60124590 × 10-8 .19514700 × 10 <sup>-5</sup> .50380000 × 10 <sup>-5</sup> .80540000 × 10 <sup>-7</sup>	-0.100.95675 71335900 × 10 <sup>-6</sup> 90676100 × 10 <sup>-7</sup> 61266000 × 10 <sup>-7</sup> 50640000 × 10 <sup>-7</sup>			10 32 13 13 15	0.9357386 .017396580 .8ep16000 x 10 <sup>-3</sup> .8037000 x 10 <sup>-4</sup> .83870000 x 10 <sup>-4</sup>	-0,18160091 -,016666600 -,10966900 × 10 <sup>-9</sup> -,9698000 × 10 <sup>-8</sup> -,49560000 × 10 <sup>-6</sup>	0.05553400 .010741690 .12501200 × 10* .55045000 × 10*
						λ = 2.2						
00 21 4 2 6 5 6 5 4 10 5	0.52719590 .052060000 .54766000 × 10 <sup>-2</sup> .27700000 × 10 <sup>-3</sup> .16100000 × 10 <sup>-4</sup>	-0.856-0307 03286390 18087000 × 10 <sup>-8</sup> 9608000 × 10 <sup>-5</sup> 16310000 × 10 <sup>-1</sup>	0.04009410 45198900 × 10 <sup>-12</sup> 45094000 × 10 <sup>-5</sup> .1861000 .19620000 × 10 <sup>-14</sup>	20 41. 62 53 104	0.17000124 .011640600 .69658000 × 10 <sup>-7</sup> .89680000 × 10 <sup>-6</sup>	-0.11738725 -0.59608900 × 10 <sup>-3</sup> -0.78789000 × 10 <sup>-3</sup> -0.78789000 × 10 <sup>-3</sup> -0.11790000 × 10 <sup>-3</sup>	,61057000 × 10 <sup>-5</sup>		1 0 5 2 7 3 9 4	0.53604690 .0695571460 .17686500 × 10 <sup>-2</sup> .3M90000 × 10 <sup>-3</sup>	-0.17943678 034134090 14599900 x 10 <sup>-2</sup> ,11651000 x 10 <sup>-3</sup>	0.05956580 .39205000 × 10 <sup>-1</sup> .72464000 × 10 <sup>-1</sup> .30505000
L.,						λ = 1. <sup>1</sup>						, <u></u>
00 21 32 63 84	0.56965450 .086948500 .80304000 × 10 <sup>-2</sup> .84360000 × 10 <sup>-3</sup>	-0.91517875 .11696900 × 10 <sup>-2</sup> .65660000 × 10 <sup>-3</sup> 64800000 × 10 <sup>-1</sup>	0.0548950m0 -,403911040 -,an669000 × 10 <sup>-8</sup> -,18890000 × 10 <sup>-3</sup>	2 0 4 1 6 8 8 3 10 4 18 5	0.2238275 .02535550 .1149000 × 10 <sup>-2</sup> .88600000 × 10 <sup>-3</sup>	-0.12990398 75012700 × 10 <sup>-1</sup> 72059000 × 10 <sup>-1</sup> 59430000 × 10 <sup>-1</sup>	.) -		10 31 52 73 94	0.57443077 .085099700 .18818000 x 10 <sup>-2</sup> .16940000 x 10 <sup>-3</sup>	-0.1798718 -71658000 x 10 <sup>-2</sup> 6#540000 x 10 <sup>-3</sup>	0.047056500 56757500 × 10 <sup>-3</sup> 50665000 × 10 <sup>-3</sup>

# THE I.- COMPUTED VALUES OF $G_{\rm p}$ , $J = \frac{3G_{\rm p}}{3g}$ , and $\frac{3G_{\rm p}}{3g}$ for s=0.20.5 And defined the second of L and $\lambda$ - Continued.

(1) L = 0.5 - Continued

P	a	1 gr <sup>u</sup>	<u>a</u>	P	€ <sub>n</sub> (P)	1 <u>94</u>	8 3	P		€ <sub>n</sub> (P)	1 <u>91</u> 90 <sup>27</sup>	alga Sign
			•			λ = 1.6	•					
0 2 4 6 8	212302000 312800000 × 10 <sup>-3</sup>	-0.19709331 ,014867600 ,30631000 × 10 <sup>-2</sup> ,34040000 × 10 <sup>-3</sup>	о.себлени олужую еди38000 × 10 <sup>-2</sup> уу810000 × 10 <sup>-3</sup>	2 0 4 1 6 2 8 3 10 4	.94190000 × 10 <sup>-5</sup>	-0.127\\$9573 5\496100 × 10 <sup>-2</sup> 68600000 × 10 <sup>-1</sup>	0.058803550 27905400 × 10 <sup>-2</sup> 51440000 × 10 <sup>-3</sup>		5 2 7 3 4	.61470000 × 10 <sup>-5</sup>	-0.1654846 .19946200 × 10 <sup>-2</sup> .88500000 × 10 <sup>-3</sup> .77100000 × 10 <sup>-4</sup>	0.035983080 86498000 × 10 <sup>-8</sup> 14835000 16660000 × 10 <sup>-3</sup>
Т	<del></del>				<u> </u>	λ = 1.8			_			<del></del>
2	0 0.6568220 1087125700 245625000 x 20 <sup>-2</sup> 3	-0.15155868 .086528300 .44019000 × 20-8	0.02097(860 -,0087(467)0 -,084217000 × 10-2	4 1 6 5 8 1 10 4		-0.12702111 ,26967400 × 10 <sup>-2</sup> ,90750000 × 10 <sup>-2</sup>			912	16776000 × 10 <sup>-3</sup>	-0.13716966 .011927900 .22648000 × 10 <sup>-2</sup> .26500000 × 10 <sup>-5</sup>	0.026040730 011667140 17590000 × 10 <sup>-2</sup> 88070000 × 10 <sup>-3</sup>
М	·	L				λ = 2.0	<u> </u>	ш	_	•		
0 2 4 6 8 10	2 ~.76040000 × 30 <sup>-2</sup>	-0.16810118 .096289000 .19687000 × 10 <sup>-6</sup>	0.0156545y2 018563950 18596000 × 10 <sup>-2</sup>	• -	-0	-0.12872575 .9756700 x 10 <sup>-2</sup> .17899000	0.0256555558 85508000 × 10 <sup>-2</sup> 10686000		<b>,</b>  1	0.50\73983 08\715000 \126\7000 x 10-2	-0.1\delta\end{a}	0.022804990 015157120 15810000 x 10 <sup>-2</sup>
<del> -</del>		T- 11				r		m^	តក	0.5812524	-0.13009909	0.013159000
2	255670000 x 10 <sup>-2</sup>	-0.18135066 .05218500 61500000 x 10 <sup>-5</sup>	0.9125660 × 10 <sup>-2</sup> 03713700 .20493000 × 10 <sup>-2</sup>		· <del></del>	-0.11545572 .085717900 .18680000 x 10 <sup>-5</sup>	0.017957184 010908800 5560000 × 10 <sup>-3</sup>		1	078500400 55990000 × 10 <sup>-2</sup>	.07760E300 .19700000 x 10 <sup>-5</sup>	03555070
L						λ = 5.0	_					
2	Ñ <b></b>	-0.1215139\$ -0.95560000 07500000 x 10 <sup>-2</sup>	0.71334100 × 10 <sup>-2</sup> 012510400 .41970000 × 10 <sup>-2</sup>		0 0.52690761 1 - 1.0699770 2 .17900000 × 10 <sup>-6</sup>	-0.10490759 .057046400 27220000 × 10 <sup>-5</sup>	0.010405k12 95599000 × 10 <sup>-2</sup> -15600000		7 3 4 5	.55540000 × 30 <sup>-Q</sup>	-0.1144488 .047705100 52100000 × 10 <sup>-12</sup>	0.83611510 × 10-0 011317100 .85180000 × 10 <sup>-2</sup>

# TABLE 1.— COMPUSED VALUES OF $G_{n_i}$ , $J = \frac{\partial G_{n_i}}{\partial \xi}$ , AND $\frac{\partial G_{n_i}}{\partial x^2}$ FOR $n_i = 0$ TO 5 AND INCREASER VALUES OF P FOR VARIOUS VALUES OF L AND $\lambda$ — Concluded

(1) L = 0.5 - Concluded

Pn	G <sub>m</sub> (P)	1 <u>96</u>	90°5 90 <sup>10</sup>	P	G <sub>n</sub> (P)	1 gr 3	90 <sup>2</sup>	P		G <sub>n</sub> (P)	<u>n</u> 26 t	<u>∂0,</u> ∂ω²
						አ = 5.5						-
	0.78730970 -,26993650 .043237000	-0.10634515 .062112400 016605000	0,38191760 × 10 <sup>-2</sup> 94603000 -50880000		.019553000	.0.095228910 .04;2699900 85570000 × 10-2	0.70979590 × 10 <sup>-Q</sup> -85596000 .51450000			0.68318291 21255550 28754000	-0.10161006 -0.10171700 -0.1012121000	0.56681350 × 10 <sup>-2</sup> 91565000 .Achtecoo
					<u> </u>	λ = 4.0		•				
	0.8117950 55215900 .011710000	-0.09\\\10250 .06199\\200 025012000	0,8666600 x 10 <sup>-2</sup> -,72795000 -,51610000			-0.066610020 .047494500 014150000	0.50895050 × 10 <sup>-2</sup> 70832000 .37960000	21 27	1   -   2		-0.090103715 .094694300 018209000	0.39278710 x 10 <sup>-2</sup> 78862000 .44840000
<u> </u>		·				λ = 6.0						
0 0 2 1 4 2 6 3 8 4	.24894000	-0.05k773eB0 .07521k300 03k250000	0.87575000 × 10 <sup>-5</sup> 88471000 × 10 <sup>-2</sup> .32770000	20	1 '	-0.062240835 .047159100 -027550000	0.16662280 × 10 <sup>-2</sup> 51724000 .50750000	7	1 1 1 1 1 1	2.60616026 - 1.46048540 - 21626000	-0.065723050 .050668100 031040000	0.12734310 × 10 <sup>-2</sup> 50551000 -51550000

Table II.- values of  $\frac{T_1}{T_e}$ ,  $\frac{\lambda_{\frac{T_1}{T_e}}^{T_1}}{\lambda_{\frac{\epsilon}{2}}}$ , and  $\frac{\lambda_{\frac{T_1}{T_e}}^{T_1}}{\lambda_{\frac{t_0}{2}}}$  at  $\epsilon = 0$  and 1.0 for perfectly

Insulated plate at various values of  $\ L$  and  $\ \lambda$ 

		<u> </u>			£ = 1.0	
λ	T <sub>1</sub>	$\frac{\partial^{T_1}_{T_e}}{\partial t}$	∂ <sup>π</sup> 1/ <sub>πe</sub> ∂ω²	$\frac{\mathtt{T_1}}{\mathtt{T_e}}$	ST CO	
			L = 0.001			
0.1	0.01026	-9.8974 × 10 <sup>-14</sup>	9.8938 × 10 <sup>-h</sup>	0.00978	9.8986 x 10 <sup>-1</sup>	
.2	.03950	-9.6050	9.6014	.03902	9.6062	
.4	.14808	-8.5192	8,5160	.14766	8.5202	
.6	.30244	-6.9756	6.9730	.30210	6.9764	
.8	.47274	-5.2726	5.2706	.47248	5.2732	
1.0	.63210	-3.6790	3.6776	.63192	3.6794	
1.2	.76302	-2.3698	2.3690	.76290	2.3702	
1.4	.85906	-1.4092	1.4086	.85901	1.4093	
1.6	.92265	-7.7350 × 10 <sup>-5</sup>	7.7322 × 10 <sup>-5</sup>	.92261	7.7360 × 10 <sup>-5</sup>	
1.8	.96080	-3.9198	3.9184	.96078	3.9204	
2.0	.98166	-1.8337	1.8330	.9816 <del>5</del>	1.8340	
2.5	.99807	-1.9343 × 10 <sup>-6</sup>	1.9336 x 10 <sup>-6</sup>	.99806	1.9345 × 10 <sup>-6</sup>	
3.0	.99988	-1.2378 × 10-7	1.2374 × 10~7	.99876	1.2380 × 10-7	
3.5	1.0	-4.8076 × 10 <sup>-9</sup>	4.8058 × 10 <sup>-9</sup>	1.0	4.8082 × 10 <sup>-9</sup>	
4.0	1.0	-1.1317 × 10 <sup>-10</sup>	1.1313 × 10 <sup>-10</sup>	1.0	1.1319 × 10 <sup>-10</sup>	
			L = 0.005	<del></del>		
0.1	0.01164	-4.9418 × 10 <sup>-3</sup>	4.9337 × 10 <sup>-3</sup>	0.00919	4.9459 × 10 <sup>-3</sup>	
.2	.04076	-4.7962	4.7883	.03838	4.8002	
.4	.14907	-4.2546	4.2477	.14696	4.2582	
.6	.30308	-3.4846	3.4789	.30135	3.4875	
.8	.47304	-2.6348	2.6305	.47173	2.6370	
1.0	.63214	-1.8393	1.8363	.63123	1.8408	
1.2	.76290	-1.1855	1.1836	.76231	1.1865	
1.4	.85893	-7.0535 × 10 <sup>-4</sup>	7.0419 × 10-4	.85858	7.0594 × 10 <sup>-4</sup>	
1.6	.92250	-3.8750	3.8750	.92231	3.8782	
1.8	.96069	-1.9653	1.9621	.96060	1.9669	
2.0	.981.59	-9.2030 × 10 <sup>-5</sup>	9.1879 × 10 <sup>-5</sup>	.981.55	9.2109 × 10 <sup>-5</sup>	
2.5	99805	-9.7345 × 10 <sup>-6</sup>	9.7185 × 10 <sup>-6</sup>	.99805	9.7430 × 10 <sup>-6</sup>	
3.0	.99987	-6.2520 × 10-7	6.2417 × 10-7	.99987	6.2572 x 10-7	
3.5	1.0	-2.4368 × 10 <sup>-8</sup>	2.4328 × 10 <sup>-8</sup>	1.0	2.4388 × 10 <sup>-8</sup>	
4.0	1.0	-5.7665 × 10 <sup>-10</sup>	5.7570 × 10 <sup>-10</sup>	1.0	5.7710 × 10 <sup>-10</sup>	

Table II.- values of  $\frac{T_1}{T_e}$ ,  $\frac{\partial \frac{T_1}{T_e}}{\partial \xi}$ , and  $\frac{\partial \frac{T_1}{T_e}}{\partial \omega^2}$  at  $\xi = 0$  and 1.0 for perfectly

INSULATED PLATE AT VARIOUS VALUES OF L AND  $\lambda$  - Continued

		ξ = O			ξ = 1.0
λ	$rac{ extstyle T_1}{ extstyle T_e}$	∂ <u>Te</u> ∂ <u>\$</u>	$\frac{\partial^{\frac{1}{1}}_{\frac{1}{2}}}{\partial^{\frac{2}{1}}}$	T <sub>1</sub> T <sub>e</sub>	$\frac{g_{\overline{L}^{\overline{6}}}}{g_{\overline{L}^{\overline{1}}}}$
			L = 0.1		
0.1	0.03472	-9.6528 x 10 <sup>-2</sup>	0.16877	0.00078	2.1252 × 10 <sup>-2</sup>
2	.06906	-9.3094	9.3568 × 10 <sup>-2</sup>	.02286	9.1054
.4	.17142	-8.2858	8.0172	.12964	8.4214
.6	.31720	-6.8280	6.6066	.28278	6.9396
.8	.47924	-5.2076	5.0388	.45300	5.2926
1.0	.63242	-3.6758	3.5566	.61388	3.7360
1.2	.75986	-2.4014	2.3236	.74776	2.4406
1.4	.85481	-1.4519	1.4048	.84750	1.4756
1.6	.91875	-8.1250 × 10 <sup>-3</sup>	7.8616 × 10 <sup>-3</sup>	.91465	8.2580 × 10 <sup>-3</sup>
1.8	-95792	-4.2078	4.0714	.95580	4.2768
2.0	.97983	-2.0170	1.9516	.97881	2.0502
2.5	.9977⊥	-2.2868 × 10 <sup>-1</sup>	2.2126 × 10 <sup>-4</sup>	.99760	2.3242 × 10 <sup>-1</sup>
3.0	.99984	-1.5983 × 10 <sup>-5</sup>	1.5465 × 10 <sup>-5</sup>	.99983	1.6244 × 10 <sup>-5</sup>
3.5	.99999	-6.8846 × 10 <sup>-7</sup>	6.6614 × 10 <sup>-7</sup>	•99999	6.9972 × 10 <sup>-7</sup>
4.0	1.0	-1.8286 × 10 <sup>-8</sup>	1.7693 × 10 <sup>-8</sup>	1.0	1.8585 × 10 <sup>-8</sup>
			L = 0.2		
0.1	0.04852	-0.19030	0.46656	0.00004	0.00667
.2	.09356	18129	.21921	.01172	.13594
.4	.19428	16114	.15106	.11244	.16607
.6	.33192	13362	.12516	.26408	.13788
.8	.48608	10278	9.6284 × 10 <sup>-2</sup>	.43384	.10607
1.0	.63412	-7.3176 × 10 <sup>-2</sup>	6.8548	-59592	7.5704 × 10 <sup>-2</sup>
1.2	.75708	-4.8584	4.5512	.73240	5.0136
1.4	.85076	-2.9849	2.7961	. 83560	3.0801
1.6	.91493	-1.7014	1.5938	.90628	1.7558
1.8	.95501	-8.9984 × 10 <sup>-3</sup>	8.4292 × 10 <sup>-3</sup>	.95044	9.2860 × 10 <sup>-3</sup>
2.0	-97792	4.4156	4.1364	.97568	4.5564
2.5	-99732	-5.3660 × 10 <sup>-1</sup> 4	5.0269 × 10 <sup>-1</sup>	.99704	5.5372 × 10 <sup>-4</sup>
3.0	.99980	-4.0820 × 10 <sup>-5</sup>	3.8237 × 10 <sup>-5</sup>	.99978	4.2120 × 10 <sup>-5</sup>
3.5	.99999	-1.9445 × 10 <sup>-6</sup>	1.8215 × 10 <sup>-6</sup>	•99999	2.0065 × 10 <sup>-6</sup>
4.0	1.0	-5.7956 × 10 <sup>-8</sup>	5.4292 x 10 <sup>-8</sup>	1.0	5.9808 × 10 <sup>-8</sup>

Table II.- values of  $\frac{T_1}{T_e}$ ,  $\frac{\partial \frac{T_1}{T_e}}{\partial \xi}$ , and  $\frac{\partial \frac{T_1}{T_e}}{\partial \omega^2}$  at  $\xi = 0$  and 1.0 for perfectly

INSULATED PLATE AT VARIOUS VALUES OF L AND  $\lambda$  - Continued

		ξ = O			ξ = 1.0
λ	T <sub>1</sub> T <sub>e</sub>	$\frac{\partial_{\frac{\mathbf{T_l}}{\partial \mathbf{g}}}^{\mathbf{T_l}}}{\partial \mathbf{g}}$	$\frac{g_{\mathrm{L}^{\mathbf{G}}}}{g_{\mathrm{L}^{\mathbf{G}}}}$	$rac{ extstyle  au_1}{ extstyle  au_{f e}}$	$\frac{g_{\overline{L}^{\underline{G}}}}{g_{\underline{L}^{\underline{I}}}}$
			L = 0.01	h	
0.1	0.01326	-9.8674 × 10 <sup>-3</sup>	9.8358 × 10 <sup>-3</sup>	0.00834	9.8848 x 10 <sup>-3</sup>
.2	.04234	-9.5766	9.5460	.03756	9.5936
.4	.15030	-8.4970	8.4698	.14606	8.5120
.6	.30388	-6.9612	6.9390	.30040	6.9736
.8	.47864	-5.2136	5.1970	.47604	5.2228
1.0	.63218	-3.6782	3.6664	.63034	3.6848
1.2	.76278	-2.3722	2.3664	.76160	2.3764
1.4	.85873	-1.4127	1.4082	.85802	1.4152
1.6	.92232	-7.7678 × 10 <sup>-4</sup>	7.7430 × 10 <sup>-4</sup>	.92193	7.7816 × 10 <sup>-4</sup>
1.8	.96056	-3.9402	3.9314	.96036	3.9510
2.0	.98154	-1.8459	1.8400	.98142	1.8522
2.5	.99804	-1.9628 × 10 <sup>-5</sup>	1.9566 × 10 <sup>-5</sup>	.99803	1,9633 × 10 <sup>-5</sup>
3.0	.99987	-1.2659 × 10 <sup>-6</sup>	1.2618 × 10 <sup>-6</sup>	.99987	1.2682 x 10 <sup>-6</sup>
3.5.	1.0	-4.9586 × 10 <sup>-8</sup>	4.9428 × 10 <sup>-8</sup>	1.0	4.9674 × 10 <sup>-8</sup>
4.0	1.0	-1.1805 × 10 <sup>-9</sup>	1.1767 × 10 <sup>-9</sup>	1.0	1.1826 × 10 <sup>-9</sup>
			L = 0.05		
0.1	0.02484	-4.8758 × 10 <sup>-2</sup>	6.1436 × 10 <sup>-2</sup>	0.00308	3.5584 × 10 <sup>-2</sup>
.2	.05446	-4.7277	4.6533	.03070	4.7633
.4	.15972	-4.2014	4.1322	.13860	4.2361
.6	.30976	-3.4512	3.3944	.29241	3.4794
.8	.47593	-2.6204	2.5772	.46276	2.6420
1.0	.63219	-1.8390	1.8088	.62294	1.8543
1.2	.76140	-1.1930	1.1734	.75540	1.2029
1.4	.85692	-7.1540 × 10 <sup>-3</sup>	7.0362 × 10 <sup>-3</sup>	.85333	7.2128 × 10 <sup>-3</sup>
1.6	.92070	-3.9648	3.8996	.91871	3-9975
1.8	-95937	-2.0513	1.9979	.95835	5.0487
2.0	.98076	-9.6190 × 10 <sup>-1</sup> 4	9.4607 × 10 <sup>-4</sup>	.98028	9.6982 × 10 <sup>-4</sup>
2.5	-99790	-1.0522	1.0349	.99784	1.0608
3.0	.99986	-7.0375 × 10 <sup>-6</sup>	6.9217 × 10-6	.99986	7.0953 × 10-6
3.5	-99999	-2.8798 × 10 <sup>-7</sup>	2.8324 × 10-7	•99999	2.9036 × 10-7
4.0	1.0	-7.2015 × 10 <sup>-9</sup>	7.0830 × 10 <sup>-9</sup>	1.0	7.2610 × 10 <sup>-9</sup>

Table II.- values of  $\frac{T_1}{T_e}$ ,  $\frac{\partial \frac{T_1}{T_e}}{\partial \xi}$ , and  $\frac{\partial \frac{T_1}{T_e}}{\partial \omega^2}$  at  $\xi = 0$  and 1.0 for perfectly

INSULATED PLATE AT VARIOUS VALUES OF L AND  $\lambda$  - Continued

		£ = 0	<del></del>		ξ = 1.0
λ	$\frac{\mathtt{T_1}}{\mathtt{T_e}}$	$\frac{\partial_{\overline{\mathbf{T}_{\mathbf{e}}}}^{\mathbf{T}_{\mathbf{e}}}}{\partial_{\mathbf{f}}}$	de die die die die die die die die die d	$rac{ extstyle  au_{ extstyle  extstyle  au_{ extstyle  extstyle  au_{ extstyle  extstyle  extstyle  au_{ extstyle  au_$	922 25
			L = 0.3	_	
0.1	0.05890	-0.28233	0.84238	0	0.00103
.2	.11248	26626	.38414	.00586	.13318
.4	.21628	23512	.21551	.09634	.24388
.6	.34654	19604	.17791	.24622	.20522
.8	.49315	15205	.13799	.41534	.15918
1.0	.63441	10968	9.9534 x 10 <sup>-2</sup>	.57829	.11482
1.2	.75476	-7.3572 × 10 <sup>-2</sup>	6.6768	.71712	7.7016 × 10 <sup>-2</sup>
1.4	.84703	-4.5891	4.1648	.82355	4.8041
1.6	.91126	-2.6622	2.4160	89763	2.7870
1.8	.95212	-1.4363	1.3035	.94477	1.5036
2.0	.97598	-7.2066 × 10 <sup>-3</sup>	6.5400 × 10 <sup>-3</sup>	.97229	7.5444 × 10 <sup>-3</sup>
2.5	.99688	-9.3516 × 10 <sup>-1</sup>	8.4870 × 10 <sup>-4</sup>	.99640	9.7896 × 10 <sup>-4</sup>
3.0	-99974	-7-7094 × 10 <sup>-5</sup>	6.9966 × 10 <sup>-5</sup>	.99970	8.0706 x 10 <sup>-5</sup>
3.5	•99999	-4.0385 × 10−6	3.6650 × 10 <sup>-6</sup>	.99998	4.2277 × 10-6
4.0	1.0	-1.3423 × 10-7	1.2182 × 10-7	1.0	1.4052 x 10-7
			L = 0.4		
0.1	0.06752	-0.37299	1.2780	0	0.00017
.2	.12808	34877	-57422	.00288	.10955
-4	.23690	30524	.27893	.08192	:31266
.6	.36087	25565	.22498	.22917	.27124
.8	.50043	19982	.17582	.39748	.21205
1.0	.63605	14558	.12809	.56105	·15448
1.2	.75287	-9.8848 × 10 <sup>-2</sup>	8.6968 x 10 <sup>-2</sup>	.70194	-10490
1.4	.84362	-6.2554	5.5036	.81138	6.6380 × 10 <sup>-2</sup>
1.6	•90775 <sup>.</sup>	-3.6899	3.2465	.88874	3.9154
1.8	•94929	-2.0286	1.7848	.93883	2.1527
2.0	.97402	-1.0394	9.1448 × 10 <sup>-3</sup>	.96866	1.1030
2.5	.99641	-1.4357 × 10 <sup>-3</sup>	1.2631	.99567	1.5235 × 10 <sup>-3</sup>
3.0	.99968	-1.2773 × 10 <sup>-4</sup>	1.1238 × 10 <sup>-4</sup>	.99961	1.3554 × 10 <sup>-4</sup>
3.5	.99998	-7.3174 × 10 <sup>-6</sup>	6.4381 × 10 <sup>-6</sup>	•99998	7.7650 × 10 <sup>-6</sup>
0.4	1.0	-2.7017 × 10 <sup>-7</sup>	2.3770 × 10 <sup>-7</sup>	1.0	2.8670 × 10 <sup>-7</sup>

TABLE II.- VALUES OF  $\frac{T_1}{T_e}$ ,  $\frac{\partial \frac{T_1}{T_e}}{\partial \xi}$ , AND  $\frac{\partial \frac{T_1}{T_e}}{\partial \omega^2}$  AT  $\xi$  = 0 AND 1.0 FOR PERFECTLY

INSULATED PLATE AT VARIOUS VALUES OF  $\ L$  AND  $\ \lambda$  - Concluded

		<b>£</b> = 0			ξ = 1.0
λ	T <u>l</u> Te	$\frac{\partial^{\overline{T}_{\underline{1}}}}{\partial \underline{\mathfrak{t}}}$	$\frac{3^{\frac{T}{1}}}{2\omega^2}$	T <u>l</u> Te	orthograms of the state of the
			L = 0.5		
0.1	0.07504	-0.46248	1.7633	0.00003	0
.2	.14151	42924	.78278	.00152	.08179
•4	.25600	37200	·3455i	.06922	.36890
.6	•37499	31250	.26710	.21303	·335 <sup>4</sup> 7
.8	.50787	24606	.21002	.38028	.26447
1.0	.63796	18102	.15450	.54409	.19456
1.2	.75139	12430	.10610	.68693	.13361
1.4	.84049	-7.9755 × 10 <sup>-2</sup>	6.8072 × 10 <sup>-2</sup>	.79914	8.5719 × 10 <sup>-2</sup>
1.6	.90442	-4.7792	4.0791	.87964	5.1365
1.8	.94650	<b>-</b> 2.6748	2.2830	.93264	2.8748
2.0	.97204	-1.3982	1.1933	.96479	1.5027
2.5	.99510	-2.0490 × 10 <sup>-3</sup>	1.7488 × 10 <sup>-3</sup>	.99484	2.2022 × 10 <sup>-3</sup>
3.0	.99961	-1.9596 × 10 <sup>-4</sup>	1.6725 × 10 <sup>-4</sup>	•99951	2.1061 × 10 <sup>-4</sup>
3.5	.99998	-1.2226 × 10 <sup>-5</sup>	1.0436 × 10 <sup>-5</sup>	•99997	1.3141 × 10 <sup>-5</sup>
4.0	1.0	-4.9836 × 10 <sup>-7</sup>	4.2536 × 10 <sup>-7</sup>	1.0	5.3563 × 10 <sup>-7</sup>

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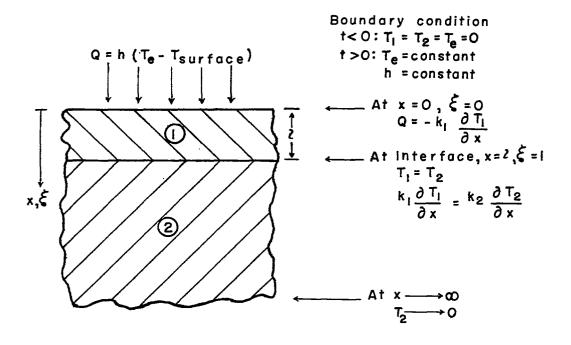


Figure 1.- Sketch of the composite slab showing pertinent boundary conditions.

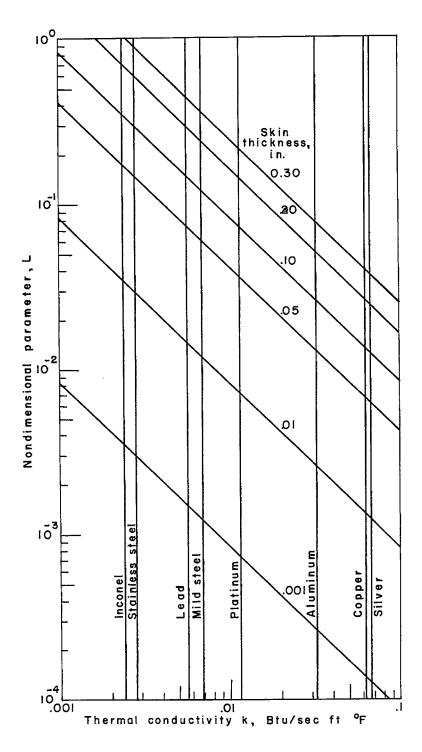


Figure 2.- Plot of the nondimensional parameter  $\,L\,$  as a function of skin material and thickness for  $\,h=0.1\,$  Btu/sq ft- $^{\circ}F$ -sec.

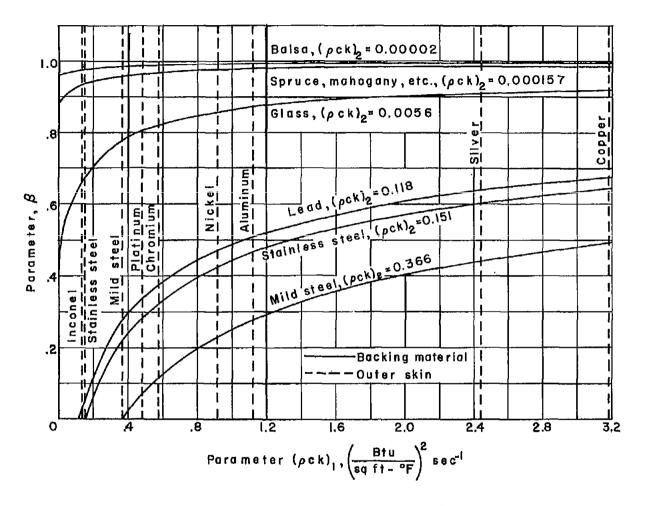
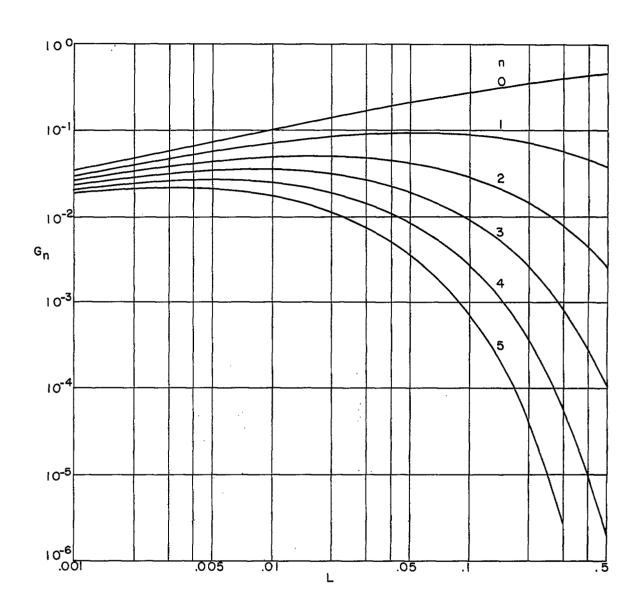


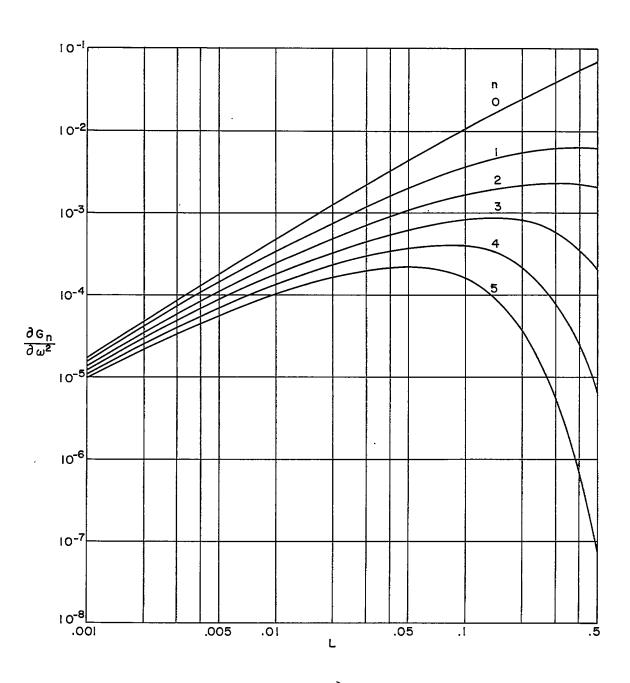
Figure 3.- Variation of the parameter  $\beta$  with the parameter  $(\rho ck)_1$  for various outer skins and backing materials. The appropriate value of  $\beta$  is determined by the intersection of the backing-material curve with the abscissa for the outer skin. If the outer skin and backing material are interchanged, the sign of  $\beta$  is reversed.



(a) G<sub>n</sub>.

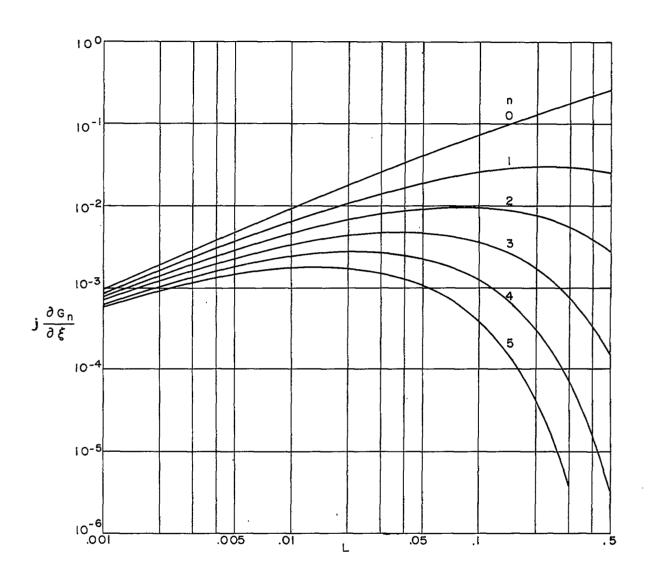
Figure 4.- Values of  $G_n$ ,  $\frac{\partial G_n}{\partial \omega^2}$ , and  $j \frac{\partial G_n}{\partial \xi}$  applicable at  $\xi = 0$  plotted against L for  $\lambda = 1.0$ . P = 2n.

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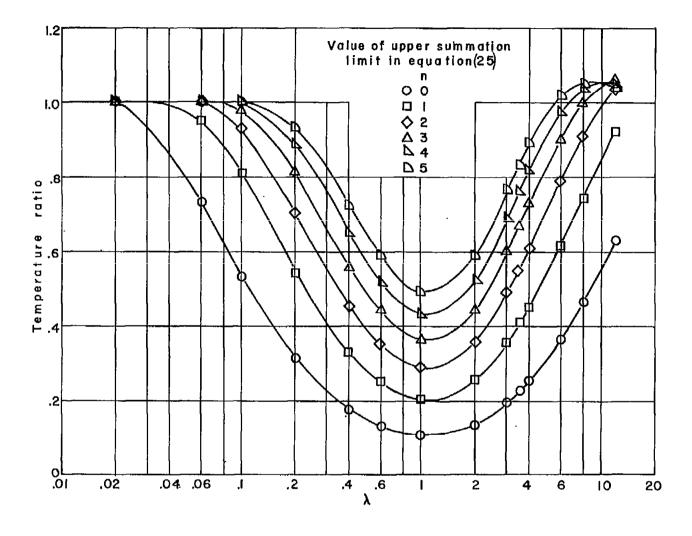
(b)  $\frac{\partial G_n}{\partial G_n}$ .

Figure 4.- Continued.



(c)  $j \frac{\partial G_n}{\partial \xi}$ .

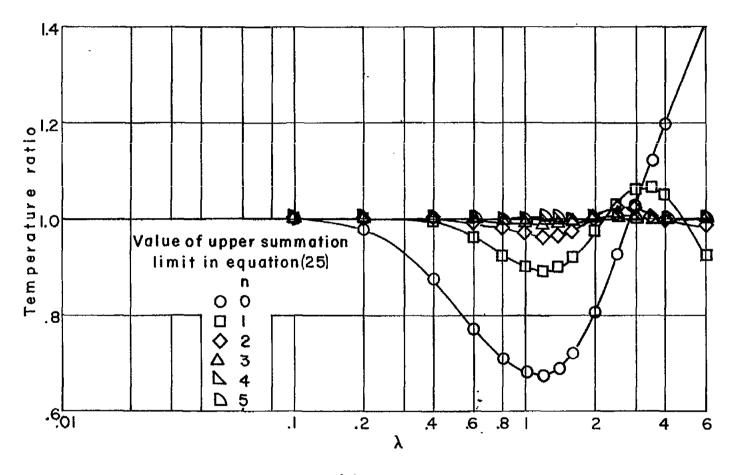
Figure 4.- Concluded.



(a) L = 0.001.

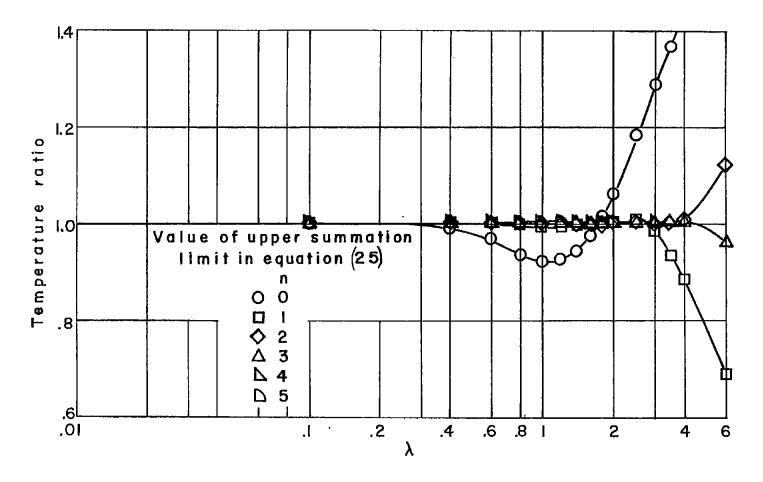
Figure 5.- Ratio of  $T_1/T_e$  at  $\xi=0$  for a finite number of terms in equation (25) to  $T_1/T_e$  from equation (15) plotted against the parameter  $\lambda$ .  $\beta=1$ .

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(b) L = 0.1.

Figure 5.- Continued.



(c) L = 0.5.

Figure 5.- Concluded.

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Figure 6.- Temperature distribution at the outer face plotted against time for composite slabs having stainless-steel skins suddenly exposed to aerodynamic heating at t=0. The skin thicknesses are 0.060 and 0.030 inch and the insulating backing materials are mahogany, balsa, and a perfect insulator. h=0.056 Btu/sq ft- $^{\circ}$ F-sec.

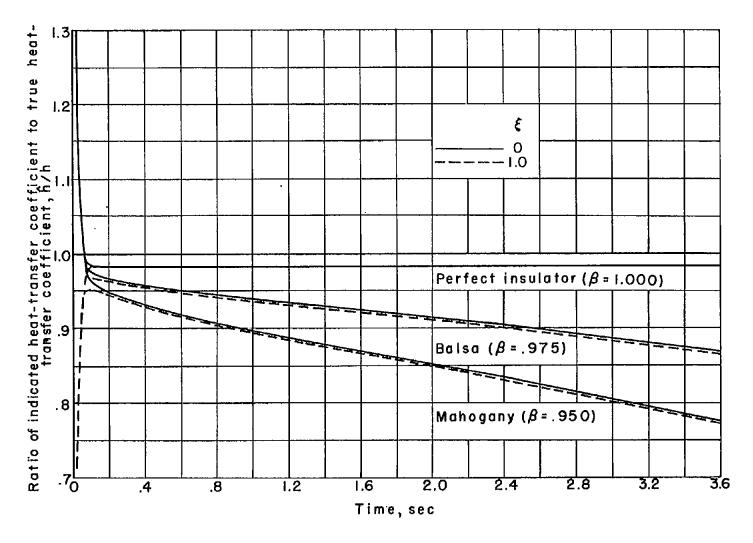


Figure 7.- Ratio of indicated heat-transfer coefficient to true heat-transfer coefficient plotted against time for a composite slab having a 0.030-inch-thick stainless-steel skin and various insulating backing materials. h = 0.056 Btu/sq ft- $^{\circ}$ F-sec.

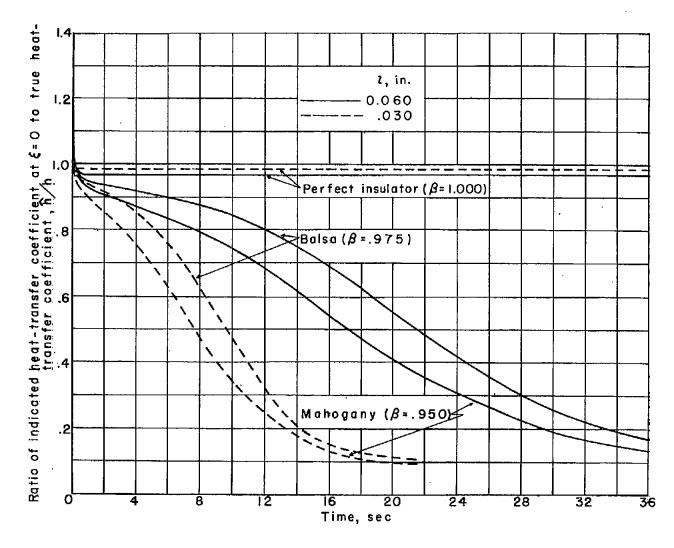


Figure 8.- Ratio of indicated heat-transfer coefficient at  $\xi=0$  to true heat-transfer coefficient plotted against time for composite slabs having stainless-steel skins of thickness l and various insulating backing materials. h=0.056 Btu/sq ft- $^{0}F$ -sec.

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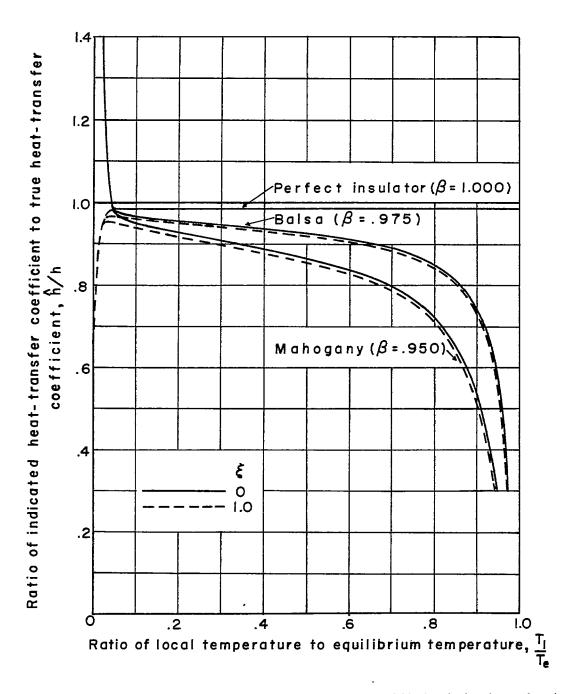


Figure 9.- Ratio of indicated heat-transfer coefficient to true heat-transfer coefficient plotted against ratio of local temperature to equilibrium temperature for composite slab having a 0.030-inch-thick stainless-steel outer skin and various insulating backing materials. h = 0.056 Btu/sq ft- $^{0}$ F-sec.